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# Ultralightweight x-ray telescope missions: ORBIS and GEO-X

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**Abstract.** Toward an era of x-ray astronomy, next-generation x-ray optics are indispensable. To meet a demand for telescopes lighter than the foil optics but with a better angular resolution  $<1$  arcmin, we are developing micropore x-ray optics based on micromachining technologies. Using sidewalls of micropores through a thin silicon wafer, this type can be the lightest x-ray telescope ever achieved. Two Japanese missions, ORBIS and GEO-X, will carry this telescope. ORBIS is a small x-ray astronomy mission to monitor supermassive blackholes, while GEO-X is a small exploration mission of the Earth's magnetosphere. Both missions need an ultralightweight ( $<1$  kg) telescope with moderately good angular resolution ( $<10$  arcmin) at an extremely short focal length ( $<30$  cm). We plan to demonstrate this type of telescope in these two missions around 2020. © The Authors. Published by SPIE under a Creative Commons Attribution 3.0 Unported License. Distribution or reproduction of this work in whole or in part requires full attribution of the original publication, including its DOI. [DOI: [10.1117/1.JATIS.4.4.046001](https://doi.org/10.1117/1.JATIS.4.4.046001)]

Keywords: x-ray telescope; small satellite; ORBIS; GEO-X.

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## 1 Introduction

X-ray telescopes are essential for future x-ray astronomy. Toward a new era of x-ray astronomy, next-generation x-ray optics are needed. Three different methods have been established in past x-ray missions: direct polishing of glass, replication of thin shells from an accurately shaped mandrel, and thin foils bent to a conical approximation of a Wolter type-I geometry. As shown in Fig. 1, there is a well-known trade-off relation between the angular resolution and the mass normalized by the effective area among these three methods.<sup>1</sup> In order to break this relation, new mirror fabrication methods are demanded.

There is an obvious need for telescopes as light as the foil optics but with  $<10$  arcsec angular resolution, which is  $\times 10$  better than the foil optics. Silicon pore optics, precision polishing of single-crystal silicon, slumping of glass sheets, and adjustable optics with piezo stress are being developed for this purpose (e.g., Refs. 2–4). Such technologies are especially important for large x-ray observatories such as Athena and Lynx.

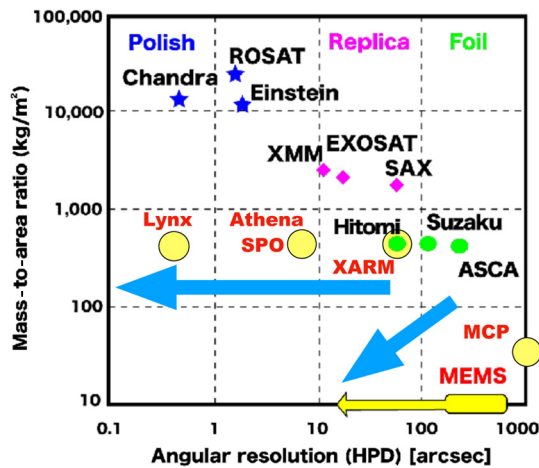
There is another demand for different telescopes that are lighter than the foil optics but have a comparable or better angular resolution of  $<1$  arcmin. Potential applications are an all-sky monitor to cover a large fraction of the sky with focusing x-ray telescopes, small/medium class astronomy satellites, and solar system exploration missions.

For these two purposes, micropore x-ray optics are now considered as good candidates. Sidewalls of micropores through a thin substrate are utilized for x-ray mirrors. If we shrink the size of the mirrors by a factor of  $C$ , the mirror weight decreases by  $C^3$ . To keep the same effective area, we have to increase the mirror number by  $C^2$ . Consequently, the telescope weight will decrease by  $C^{3-2} = C^1$ . Therefore, using micropores with a width of the order of  $10 \sim 100 \mu\text{m}$  for x-ray mirrors, the micropore optics can be light in weight.<sup>5</sup>

Three types of micropore optics have been proposed and are being developed. The first type is microchannel plate optics (MCP) made of glass fibers.<sup>6,7</sup> Sidewalls of square pores are utilized for x-ray mirrors. A spherically bent glass plate with numerous micropores works as lobster-eye optics. By stacking two plates, a Wolter type-I optic is also fabricated for the ESA's BepiColombo mission.<sup>8</sup> The second type is the silicon pore optics, called SPO.<sup>1,2,7</sup> A thin silicon wafer diced into rectangles is wedged and stacked onto another wafer so that the surface of the wafer is utilized for x-ray mirrors. This type is employed in the ESA's large x-ray observatory, Athena.

As a third type, we have invented and are developing what we call MEMS x-ray optics.<sup>5,9–14</sup> MEMS stands for microelectromechanical systems. We apply micromachining technologies for the micropore x-ray optics. To date, we have demonstrated x-ray reflection and imaging with various MEMS techniques. In this paper, we introduce two new Japanese small mission plans, Orbiting Binary Blackhole Investigation Satellite (ORBIS) and GEO-X, which will carry the MEMS x-ray optics. We then introduce the MEMS x-ray optics.

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**Fig. 1** Performances of past and future x-ray telescopes. A horizontal axis is the angular resolution in half power diameter (HPD), while a vertical axis is a telescope mass normalized by an effective area at 1 keV. Stars, diamonds, and green circles represent x-ray telescopes onboard past space missions. Yellow circles (with outlined circumferences) represent required performances in future missions or expected performances of micropore x-ray optics. Blue arrows indicate the two major demands in future missions. A goal of our MEMS x-ray optics is shown in a yellow arrow.

## 2 Small Missions

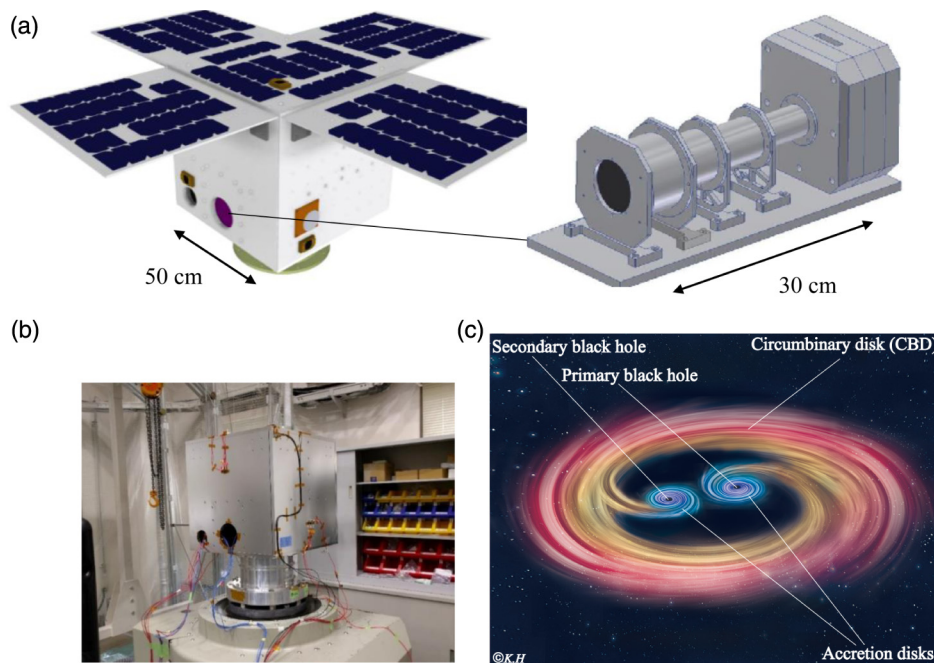
### 2.1 ORBIS

ORBIS is a university-built astronomy satellite led by Tokyo Metropolitan University in collaboration with ISAS/JAXA, Kanto Gakuin University, Kansei Gakuin University, Osaka University, and Meisei University.<sup>15</sup> Its scientific objective is to search for a signature of a binary black hole (BBH) by observing a specific active galactic nucleus (AGN) continuously for a long time ( $\sim 1$  year).

In spite of detections of gravitational waves from intermediate mass BBHs, it is still unclear how a BBH evolves. In evolution of supermassive black holes in galactic nuclei, BBHs may form and influence their host galaxies. In the final stage of a BBH, the gravitational radiation becomes efficient to remove the angular momentum of the BBH. To reach this stage, the angular momentum must be lost while its loss by dynamical friction is expected to slow down due to depletion of stars on orbits intersecting the BBH. As a possible scenario, a mass transfer from a circumbinary disk to each BH is suggested to add the angular momentum loss.<sup>16</sup> Furthermore, by combining the theoretical and observational studies, about 10% of nearby AGNs with  $10^{6.5-7} M_{\odot}$  are estimated to be BBHs.<sup>17</sup> If so, there is a good chance to detect a binary signature. In fact, the optical observation of the blazer OJ287 over 100 years has revealed periodic bursts every  $\sim 12$  years and it is believed to be a BBH.<sup>18</sup>

The ORBIS mission is a special satellite dedicated to this science theme. It will observe only one or two specific AGNs in order to find out a binary motion. Such an observation focused on a limited target is unrealistic in large x-ray astronomy satellites. Even with all-sky x-ray monitors, a nearly continuous observation of one target is not easy, because all-sky x-ray monitors usually scan a part of the sky by narrowing the field of view with slits.<sup>19</sup> Therefore, the ORBIS can be a unique satellite complementary to large x-ray observatories and existing all-sky monitors.

Figure 2 overviews the ORBIS satellite and its science payload. Specifications are summarized in Table 1. It is 50 cm on a side with a mass of 50 kg including the science payload. Science requirements are shown in Table 2. A point source sensitivity comparable to an existing large all-sky x-ray monitor MAXI<sup>19</sup> is required. To achieve this sensitivity under the limited resources (size, weight, and power), focusing the incident x-rays at a low-background detector is essential. Therefore, a compact x-ray imaging spectrometer composed of the MEMS x-ray optic



**Fig. 2** Overview of the ORBIS mission: (a) three-dimensional cad drawings of the spacecraft and the payload, (b) a photo of a structure and thermal model,<sup>15</sup> and (c) artistic impression of a BBH.<sup>17</sup>

**Table 1** Specifications of the ORBIS satellite.

	Unit	Values
Size	mm	500 × 500 × 500
Mass	kg	50
Power	W	144 (max)
Transmitter	kbps	100 (max) @ S-band
Receiver	kbps	1 (max) @ S-band
Altitude		550 km, low Earth orbit

**Table 2** Requirements and specifications of the science payload in ORBIS.

	Unit	Values
Energy	keV	0.3 to 10
Point source sensitivity ( $3\sigma$ )	mCrab	5 in 3 days exposure
MEMS Wolter type-I x-ray optic		
Diameter	mm	100
Focal length	mm	250
Angular resolution	arcmin	<10
Mirror weight <sup>a</sup>	g	5/30
CCD detector		
Pixel size	$\mu\text{m}$	24 × 24
Format	pix	320 × 256
Area	mm	7.680 × 6.114
Energy resolution	eV	180 at 6 keV
Operating temperature	°C	-90

<sup>a</sup>Without/with an Al frame.

and the CCD detector will be onboard. The MEMS x-ray optic can be an ultralightweight telescope enabling a good angular resolution even at the required short focal length (<30 cm). The x-ray CCD is a miniature of the Hitomi SXI.<sup>20</sup>

We have constructed a structure and thermal model of the satellite. Environmental tests for this satellite model are ongoing. In parallel, a vibration test for the MEMS Wolter type-I optic has been conducted and no damage on the optic was observed. We have started an assembly of a part of the flight model of the satellite. The payload will be assembled in the satellite in 2019. An aimed launch year is around 2020. A piggy back launch by a JAXA H-IIA rocket is considered. A candidate for the science observation is a Seyfert 1 galaxy NGC 4151, which is suggested as a BBH candidate from an optical spectroscopy<sup>21</sup> and brightness in x-rays. Other candidates such as a blazar Mrk 421 are under investigation. The line of sight direction is constrained by an observational date and a

solar angle. We will finalize the target when a launch date is fixed.

## 2.2 GEO-X

GEO-X (GEOspace x-ray imager) is a small exploration satellite under concept study by Tokyo Metropolitan University, Nagoya University, University of Tokyo, ISAS/JAXA, Hokkaido University, Kanto Gakuin University, Kobe University, and Tohoku University. Its objective is x-ray imaging of the Earth's magnetosphere using solar wind charge exchange emission from a location outside the magnetosphere. For this purpose, the satellite will be located at the vicinity of the Moon which is about  $60 R_{\text{Earth}}$  from the Earth and will observe this emission from that distant place for the first time.

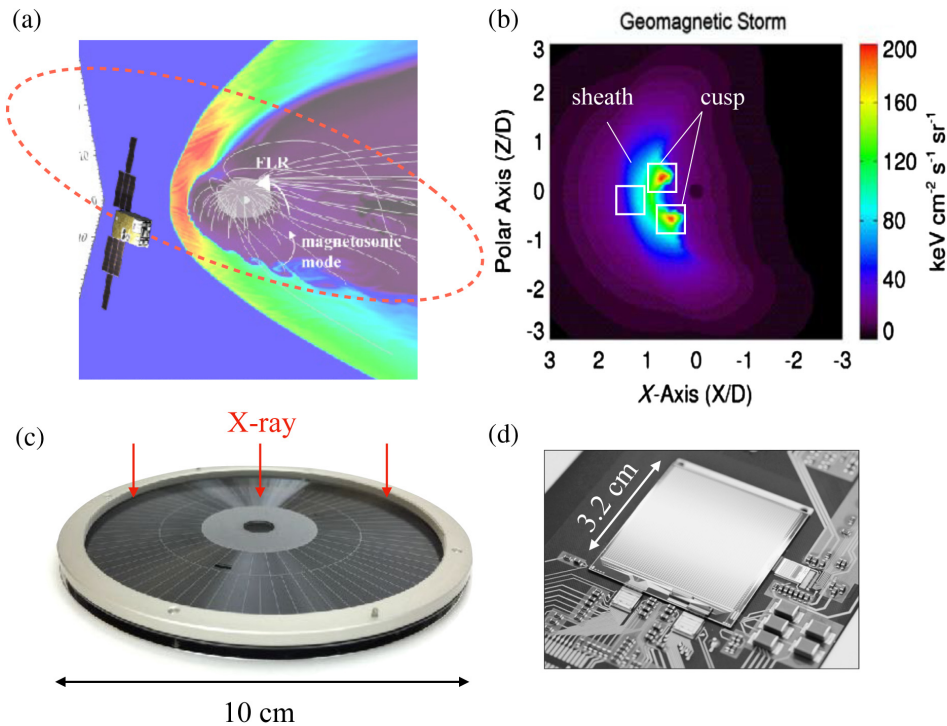
The solar wind charge exchange emission around the Earth was discovered with ROSAT during the all-sky survey.<sup>22</sup> It occurs between solar wind ions and exospheric neutrals near the Earth. The solar wind ion, such as  $\text{O}^{7+}$ , strips an electron from the neutral atom or molecule, such as H. The transferred electron to the ion decays into the ground state emitting photons as emission lines in the UV and x-ray wavelength range. Due to good energy resolution CCDs onboard Chandra, XMM-Newton, and Suzaku, it is now established as a time-variable foreground emission for x-ray astronomy satellites orbiting around the Earth.<sup>23–27</sup>

Because these large x-ray observatories have relatively small FOVs (e.g., 20 arcmin × 20 arcmin) and basically fly within the magnetosphere, fundamental questions such as how this emission is distributed and how this emission becomes bright are still unclear. Understanding of the solar wind charge exchange emission around the Earth is closely related to how the charge exchange emission occurs in other space environments such as supernova remnants and clusters of galaxies. Furthermore, from the viewpoint of planetary and magnetospheric science, this emission can be a new diagnostic tool to image the invisible Earth's magnetosphere.<sup>28</sup>

Many model studies have been conducted on this x-ray emission using magnetohydrodynamics (MHD) simulations of the Earth's magnetosphere. The x-ray emission is predicted to be strong at the dayside sheath region where both solar wind density and exospheric density are high. Magnetosheath, cusps, and bowshock can be visualized via x-rays (e.g., Ref. 29). These dayside regions of the magnetosphere are especially of importance in the context of interactions between solar wind and the magnetosphere. To date, precise measurements of electromagnetic fields and plasmas have been done by *in situ* observations. X-rays can be a new tool to take a global picture of the magnetosphere. Since the emission is expected to be associated with the magnetosphere, we basically need to escape from the magnetosphere.

GEO-X is a small satellite focusing on this special science theme. It will carry a wide FOV X-ray imaging spectrometer to map the emission with high sensitivity in 0.3 to 2 keV where the solar wind charge exchange emission is most strong as emission lines from ionized C, N, O, Fe, Mg, and S. The line of sight direction will be always toward the subsolar side of the Earth, i.e., near the dayside of the Earth. The satellite will be injected into high Earth orbit, outside the Earth's magnetosphere where the emission comes from. Similar to ORBIS, such observations have not been conducted.

Figure 3 shows a concept of the GEO-X satellite. Tables 3 and 4 summarize specifications of the satellite and the payload.



**Fig. 3** Overview of the GEO-X mission: (a) a concept of the spacecraft orbiting around the Earth’s magnetosphere,<sup>30</sup> (b) an MHD-based model for the solar wind charge exchange emission as observed from  $50 R_{\text{Earth}}$ ,<sup>29</sup> (c) an MEMS Wolter type-I optic, and (d) a DepFET detector.<sup>31</sup> Each solid square in the MHD simulation indicates a FOV of the payload.

**Table 3** Specifications of the GEO-X satellite under concept study. Numbers are to be determined.

	Unit	Values
Size	mm	$\sim 200 \times 200 \times 300$
Mass	kg	$\sim 30$
Power	W	$\sim 100$ (max)
Transmitter	kbps	$\sim 50$ @ S-band
Receiver	kbps	$\sim 1$ @ S-band
Altitude		$\sim 40$ to $60 R_{\text{Earth}}$ , high Earth orbit

The satellite will be a  $\sim 12$  U cubesat or a similar size. It will be injected into a near circular high Earth orbit with an altitude of  $40 - 60 R_{\text{Earth}}$ , i.e., near the Moon and a small inclination angle. A propulsion system composed of  $\text{N}_2\text{O}$  and polyethylene can be attached to the satellite. The weight of the satellite will be  $\sim 30$  kg and the propulsion system will add  $\sim 20$  kg. In total, the satellite including the propulsion system will be  $\sim 50$  kg or less. A piggy back launch of the JAXA’s HII-A or HIII rocket is considered. Necessary  $\Delta v$  depends on the rocket and its orbital insertion but it will be at most  $\sim 400 - 500$  m/s when the satellite is first injected into an elliptical orbit by the rocket with an apogee of  $\sim 60,000$  km.

To achieve a good sensitivity to this diffuse x-ray emission, a grasp or a multiple of an effective area and FOV is important. GEO-X will achieve a large grasp comparable to the Suzaku

**Table 4** Requirements and specifications of the science payload in GEO-X.

	Unit	Values
Energy	keV	0.3–2
Grasp	$\text{cm}^2 \text{deg}^2$	10 at 0.6 keV
MEMS Wolter type-I x-ray optic		
Diameter	mm	100
Focal length	mm	250
Angular resolution	arcmin	$< 10$
Mirror weight <sup>a</sup>	g	5/30
DepFET detector		
Pixel size	$\mu\text{m}$	$300 \times 300$
Format	pix	$64 \times 64$
Area	mm	$19.2 \times 19.2$
Energy resolution	eV	80 at 1 keV
Operating temperature	$^{\circ}\text{C}$	$-60$

<sup>a</sup>Without/with an Al frame.

X-ray CCD and telescope system in this small satellite platform. It is in principle possible because of its short focal length and operation in the soft x-ray band, resulting in a large FOV of  $4 \text{ deg} \times 4 \text{ deg}$  at least. The required angular resolution is

moderate because the x-ray emission is expected to be widely extended. The same Wolter type-I design as in ORBIS will be adopted, allowing us swift development. The aimed launch year is around 2022, near the next solar maximum.

We have estimated the number of events that GEO-X will detect using past solar wind data taken with the GOES and ACE satellites during 1998 to 2011. This duration covers one solar cycle. Here, we assumed that signals are proportional to an incoming ion flux, while the background is a combination of soft x-ray sky background and non-x-ray background. For simplicity, we focused on the  $O^{6+}K_{\alpha}$  band (0.5 to 0.6 keV). From Ref. 29, the x-ray flux at a certain solar wind  $O^{7+}$  flux level can be estimated. The soft x-ray background and the instrumental background including a radiation noise mainly due to high energy protons were calculated from the past x-ray observations<sup>32</sup> and our GEANT4 simulations.<sup>33</sup>

Figure 4 shows the results. We counted how many data points can meet the  $S/N$  ratio  $>20$  based on the solar wind data and the past x-ray astronomy observations. The number of the data points can be converted to an estimated observational duration in which the high  $S/N$  ratio is expected. The estimated number of such data points peaks around the solar maximum and decreases toward the solar minimum. At the solar maximum,  $\sim 150$  data points exist. Because each datum is averaged over 2 h, this indicates that we can obtain  $\sim 300$  data sets having  $S/N > 20$  at the 1-h exposure time in a single year with GEO-X. Even at a 10-min exposure, good data points exist. On the other hand, at the solar minimum, the number of the data points is nearly zero. Therefore, the launch year is crucial. The most proper launch year would be the early 2020's in which the solar activity will rise.

For the same purpose, i.e., x-ray imaging of the Earth's magnetosphere, the SMILE and CuPID missions are planned in ESA-China and the USA, respectively.<sup>34,35</sup> The SMILE mission is a medium-class satellite observing the solar wind charge exchange emission from an elliptical orbit with an apogee of  $\sim 20 R_{\text{Earth}}$ . The orbit has a high inclination angle to observe

UV aurora at the same time. Wide FOV Lobster MCP optics and a large format CCD will be onboard. The CuPID mission is a 6U cubesat at low Earth orbit and will carry Lobster MCP optics and an MCP detector. In contrast, GEO-X will observe this emission from the most distant place with a relatively small inclination angle, allowing unique sideview imaging of the Earth's magnetosphere. Also the DepFET detector is not significantly affected for optical light contamination, enabling observations of cusps near the dayside of the Earth. These features will make GEO-X unique and complementary to the other missions.

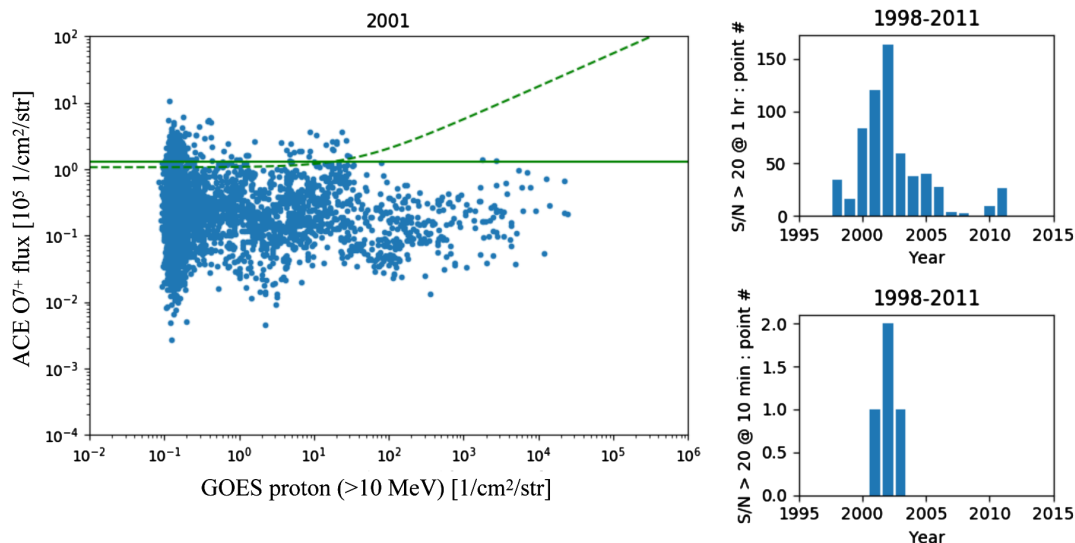
### 3 MEMS X-Ray Optics

#### 3.1 Concept

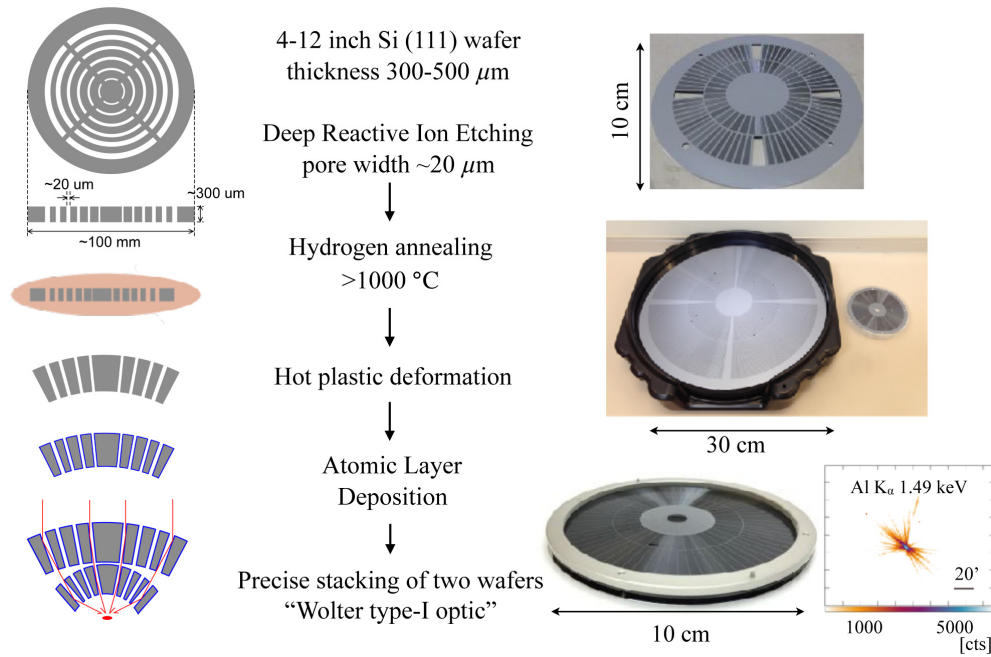
We utilize micromachining techniques for fabrication of the micropore x-ray optics. We have tested various techniques including anisotropic wet etching, deep reactive ion etching (DRIE), x-ray LIGA (Lithographie, Galvanik, und Abformung) and focused ion beam, and succeeded to verify x-ray reflection on sidewalls of micropores.<sup>9,10,14</sup> Now we focus on the DRIE-fabricated optics. The process flow is shown in Fig. 5.

Sidewalls of curvilinear micropores made by DRIE are smoothed by hydrogen annealing at  $>1000^{\circ}\text{C}$ . The wafer is deformed to a spherical shape by hot plastic deformation. Sidewalls can be coated with a high-Z material by atomic layer deposition (ALD). Two wafers deformed to different curvature radii are precisely stacked to form a Wolter type-I optic. Because of the tiny pores and thin wafers, this type of optics can be the lightest x-ray telescope ever achieved. It is also low cost because we basically fabricate the optics by ourselves.

A conical approximation of the Wolter type-I is almost negligible,  $\sim 2$  arcsec, even at a short focal length of 25 cm when the wafer thickness is  $300 \mu\text{m}$  and the reflection angle is 1 deg. A theoretical limit on the angular resolution is an x-ray diffraction within each micropore which is  $\sim 13$  arcsec at 1 keV when the



**Fig. 4** Example of GOES proton ( $>10$  MeV) flux versus ACE  $O^{7+}$  flux in 2001, where each data point is 2 h average. Solid and dashed lines indicate boundaries of the data points having signal-to-noise ratios ( $S/N$ )  $> 20$  when photon statistics or background fluctuation is considered, respectively. GEO-X instrumental parameters and an exposure time of 1 h is assumed. On the right side, histograms of the number of points having  $S/N > 20$  in the 1 h or 10 min exposure are plotted as a function of year from 1998 to 2011.



**Fig. 5** Process flow of the MEMS x-ray optics. From top to bottom, photos show a single-stage 4-in. Si optic, a 12-in. Si optic, and a 4-in. Wolter type-I optic.

micropore width is  $20 \mu\text{m}$ . Therefore, an ultralightweight telescope with an angular resolution better than 1 arcmin would be possible. We have verified x-ray reflection and imaging with this method as shown in Fig. 5.

### 3.2 Design

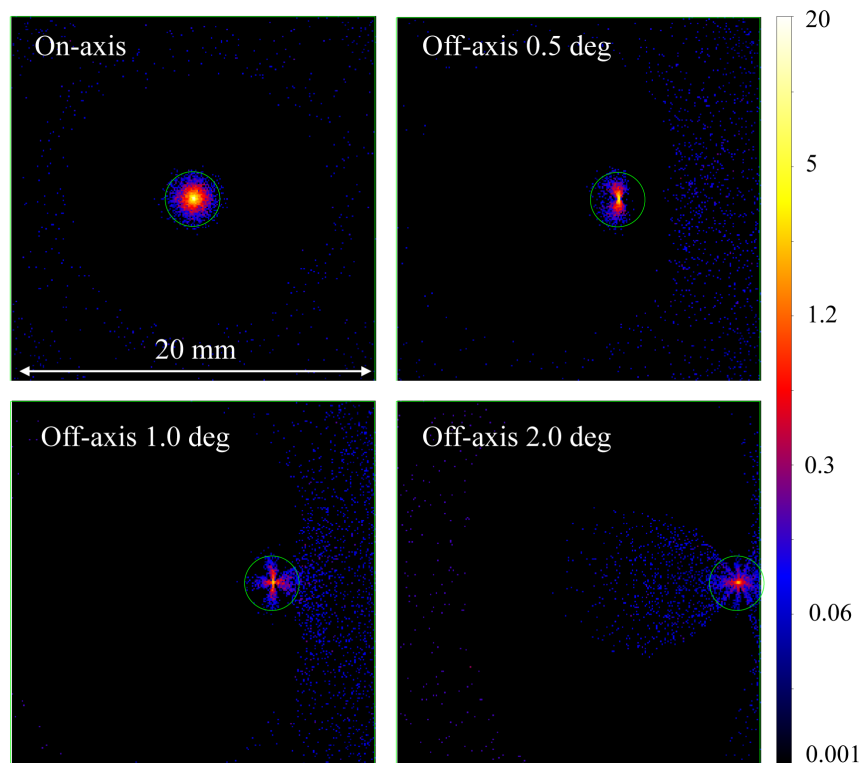
Table 5 summarizes the baseline design of the MEMS Wolter type-I optic for ORBIS and GEO-X. The optic will be made from 4-in. Si wafers. An open area ratio will be  $\sim 20\%$ . Sidewalls will be coated by Pt. A thin  $\text{Al}_2\text{O}_3$  layer will be between Si and Pt for good adhesion. Figure 6 shows raytracing simulations based on these parameters. A photon number for each simulation is 50,000. A detector size of  $20 \text{ mm} \times 20 \text{ mm}$  is used considering the GEO-X configuration. A micro-roughness of each mirror is assumed as 1 nm in rms from the experiments. The focused image changes depending on the incident angle due to vignetting and stray light. We estimate an effective area and a grasp by integrating a circular area around the focus with a radius of 1.5 mm corresponding to 20 arcmin on the detector. Figure 7 shows the obtained results.

In ORBIS, the on-axis effective area is crucial because the target is a point source and the line of sight direction will be always toward the target. A moderate effective area of  $\sim 3 \text{ cm}^2$  is expected at 1 keV. Here, the detector quantum efficiency and the optical blocking filter of the Hitomi SXI are assumed. This value is a factor of  $\sim 100$  smaller than that of Suzaku XIS. However, the sensitivity to the point source is proportional to a square root of the effective area and the exposure time when the photon statistics or the background noise dominates. Therefore, because of the observation strategy whereby only a specific target is observed, the required sensitivity of 5 mCrab in three days exposure time can be achieved as far as the background level is similar to the Suzaku XIS. We expect to achieve such a low background in ORBIS because the orbit and the detector shield will be similar to those in Suzaku.

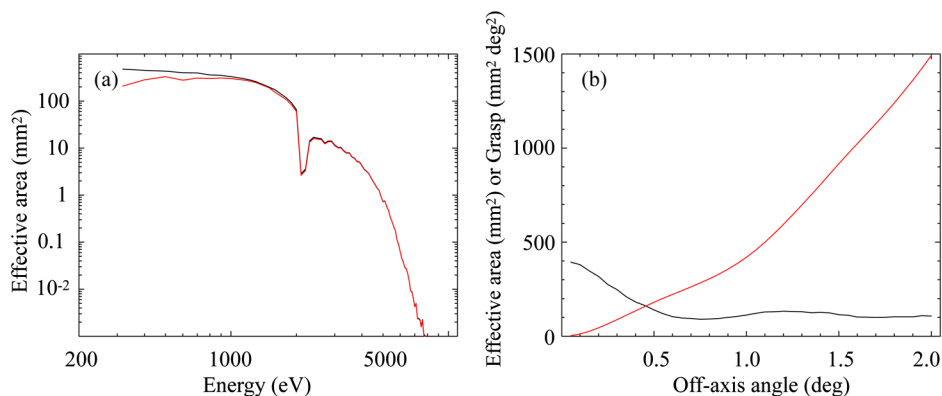
**Table 5** Baseline design of the MEMS Wolter type-I optics for ORBIS and GEO-X.

	Unit	Values
Wafer properties		
Diameter	mm	100
Thickness	$\mu\text{m}$	300
Curvature radius	mm	1000 (first), 333 (second)
Micropore properties		
Micropore width	$\mu\text{m}$	20
Space between micropores	$\mu\text{m}$	20
Innermost radius	mm	15
Outermost radius	mm	45
Sidewall coating		Pt + $\text{Al}_2\text{O}_3$
Required performance		
Angular resolution	arcmin	10
Effective area	$\text{cm}^2$	3 at 1 keV
Grasp	$\text{cm}^2 \text{ deg}^2$	10 at 0.6 keV

In GEO-X, the grasp is more important. Because of the large field of view, the grasp will be comparable to, or even better than, that of the Suzaku XIS. The calculated value is  $1500 \text{ mm}^2 \text{ deg}^2$  or  $15 \text{ cm}^2 \text{ deg}^2$  at 0.6 keV. After considering the detector and optical blocking filter efficiency, which will be similar to ORBIS ( $\sim 70\%$  at 0.6 keV and  $>90\%$  above



**Fig. 6** Raytracing results for the MEMS Wolter type-I optic assuming optics parameters in Table 5 at 0.6 keV. Different incident angles are used. A color scale is in arbitrary unit. A solid circle corresponds to an area with a radius of 1.5 mm used for the effective area and grasp calculations.



**Fig. 7** (a) Effective area of the MEMS Wolter type-I optic estimated from the raytracing simulations. Black and red curves represent an effective area without and with a detector quantum efficiency and an optical blocking filter. (b) Grasp of the MEMS Wolter type-I optic as a function of off-axis angle. Black and red curves are an effective area and a grasp. The detector and optical blocking filter efficiency is not included.

1 keV), the required grasp of  $>10 \text{ cm}^2 \text{ deg}^2$  will be satisfied. Thus, these simulations indicate that the compact and light weight MEMS Wolter type-I optic can meet the required sensitivity in ORBIS and GEO-X under the very limited resources of these small missions.

### 3.3 Recent Development

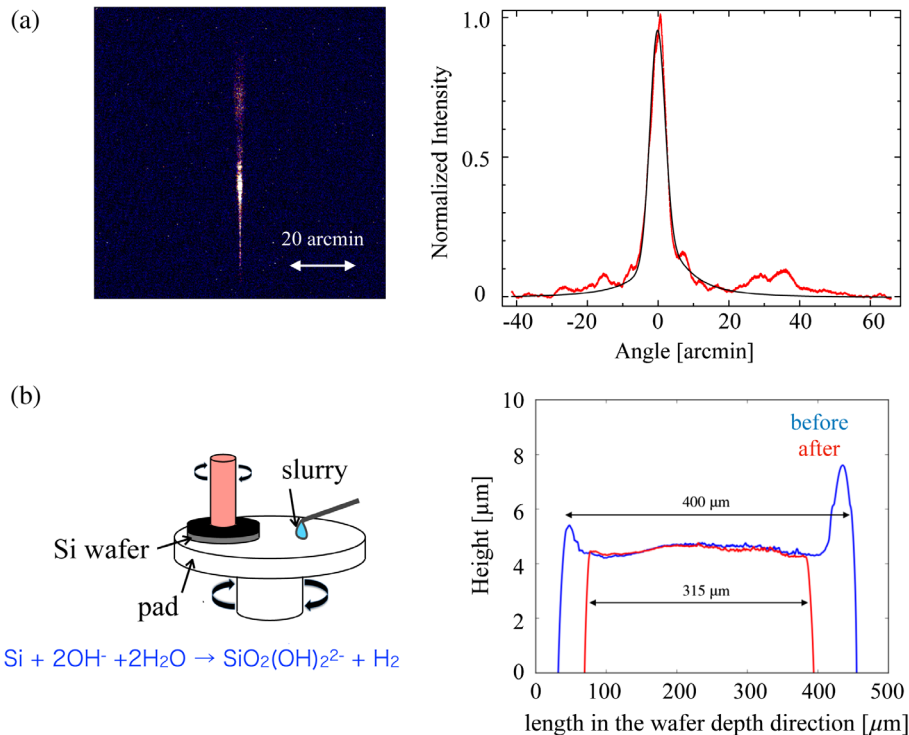
We show our recent development of the MEMS x-ray optics toward ORBIS and GEO-X. As described above, we have demonstrated the Wolter type-I optic. We are now improving the optics performance including the angular resolution and the effective area.

### 3.4 Angular Resolution

From a series of evaluations of mirror qualities and arrangement errors in a step by step manner at individual processes, we now consider that one of the major factors for the angular resolution is mirror quality itself. Figure 8(a) shows our recent x-ray test of a single mirror. It has a relatively sharp peak with a half energy width of  $\sim 5$  arcmin on average within the optic. A typical FWHM is  $\sim 3$  arcmin. The required angular resolution by single reflection is 5 arcmin in both ORBIS and GEO-X. Therefore, this main component meets the requirement.

However, there are two other components that should be eliminated or reduced. One is a broad component represented





**Fig. 8** (a) X-ray response of a single mirror after DRIE and annealing at  $\text{AlK}_\alpha$  1.49 keV and its projected profile fitted with Gaussian and Lorentzian models. (b) Concept of chemical mechanical polishing and an example of sidewall profiles of a sample DRIE-fabricated optic before and after polishing.

by a Lorentzian model. A half energy width of this component is typically  $\sim 15$  arcmin. As a result, the half energy width of the single mirror can become  $\sim 10$  arcmin. The angular distribution of the Lorentzian component is similar to expected x-ray scattering from the mirror surface power spectrum density (PSD). Therefore, we are now trying to suppress the surface roughness by changing DRIE and annealing processes. Because the x-ray scattering intensity is proportional to the PSD and the rms roughness is an integral of the PSD in the frequency domain, we aim at a factor of  $\sim 3$  reduction of the rms roughness which leads to a factor of  $\sim 9$  reduction of the scattering intensity if this is the case.

The other unwanted component is an additional peak located at large reflection angles. It is most likely due to edge structures in the sidewalls generated after DRIE. We thus newly introduced chemical mechanical polishing of the wafer after DRIE from both sides. We filled micropores with photoresist, in order not to break structures, and removed the photoresist after polishing. As shown in Fig. 8(b), we succeeded in removing the edge structures without destruction of the wafer. In addition to removing the edge structure, this process allows us to leave the flat mirror surface. Thus, we can expect not only a large effective area at small reflection angles, but also a better angular resolution.

### 3.5 Effective Area

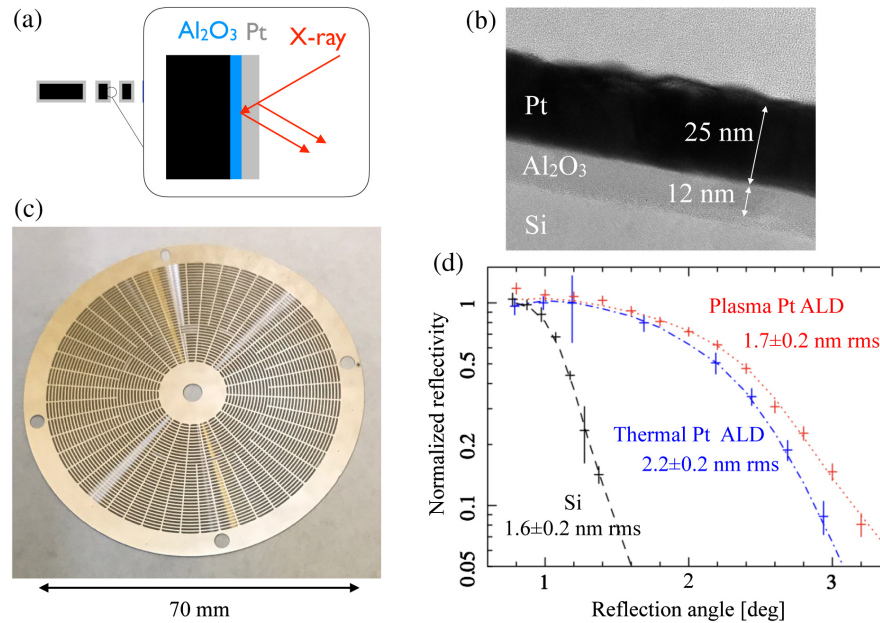
In addition to the angular resolution, we tested a new ALD process to increase the effective area.<sup>36</sup> Coating of the sidewalls with high Z materials is necessary in the MEMS x-ray optics. Since a standard coating process such as sputtering or evaporation do not allow conformal coating of the high aspect sidewalls, we selected the ALD as a new coating method. We tested Ir ALD in the early stage of our development.<sup>37</sup> Although the

coating was successful in terms of x-ray reflectivity, the cost was higher.

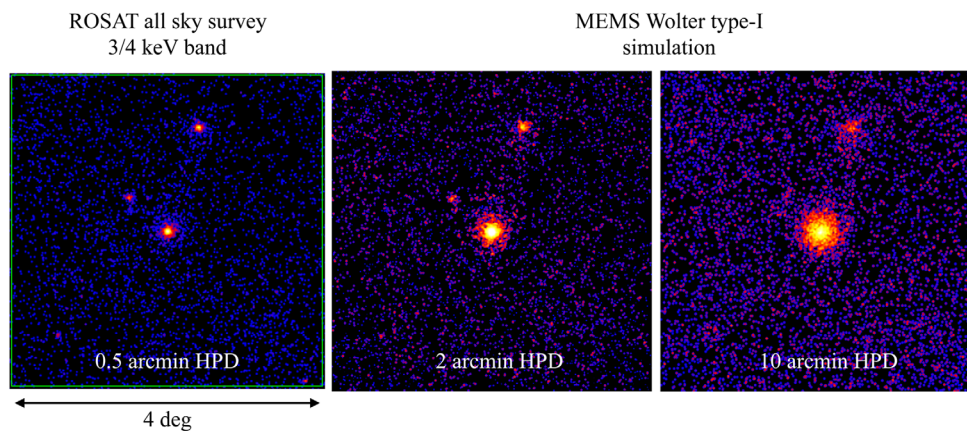
Hence, we recently tried Pt ALD. It consists of two reactions. At first, we introduce a Pt precursor  $2(\text{MeCp})\text{PtMe}_3$ . Then, the precursor attached to the wafer surface is catalytically combusted by  $\text{O}_2$ . By cycling these two reactions, a pure Pt layer can be coated on the Si sidewalls. The reaction temperature and the growth rate are  $\sim 270^\circ\text{C}$  and  $\sim 0.4 \text{ \AA}/\text{cycle}$ , respectively. To strengthen adhesion, we inserted an  $\text{Al}_2\text{O}_3$  layer between Si and Pt.

Figure 9 shows an example of the MEMS x-ray optic after DRIE, annealing, and ALD. Aimed thicknesses of Pt and  $\text{Al}_2\text{O}_3$  layers were 20 and 10 nm, respectively. A transmission electron microscope image of a sidewall indicates that the two layers are coated properly on the sidewall with Pt and  $\text{Al}_2\text{O}_3$  thicknesses of 25 and 12 nm, respectively. At  $\text{Al K}_\alpha$  1.49 keV, an enhanced x-ray reflectivity was confirmed. However, the surface roughness estimated from the curves seemed to increase after coating from 1.6 to 2.2 nm rms. A required microroughness in ORBIS and GEO-X is about  $< 2$  nm in rms.

Therefore, we coated another wafer with a different ALD method. To activate chemical reactions, we introduced O plasma instead of  $\text{O}_2$  gas. This process is called plasma ALD and distinguished from the previous process, thermal ALD. The aimed thicknesses of the two layers are the same as before. Consequently, the plasma ALD-coated sample showed thicknesses similar to those in the thermal ALD but a better reflectivity, while the surface roughness before coating was the same as that before the thermal ALD. No significant change in the microroughness was observed. The required microroughness in ORBIS and GEO-X is below  $\sim 1.5$  nm rms. Therefore, these results support the view that the Pt coating by ALD is usable for ORBIS and GEO-X.



**Fig. 9** (a, c) Concept and photo of Pt-coated MEMS x-ray optics, (b) a transmission electron microscope image of a sidewall, and (d) x-ray reflectivity curves at  $\text{AlK}_{\alpha}$  1.49 keV of the sidewalls. The photo and electron microscope image are for the plasma Pt ALD sample, while the reflectivity curves are for both the thermal and plasma Pt ALD samples. Numbers indicate microroughness estimated from the reflectivity curves.



**Fig. 10** MEMS Wolter type-I simulations compared to an original ROSAT all-sky survey 3/4 keV band image near the Galactic center ( $ra, dec = (266.404996, 28.936172)$  in J2000.<sup>38</sup> The parameters for the MEMS Wolter type-I optic are summarized in Table 5. An x-ray energy of 0.6 keV is assumed. The exposure time of the original ROSAT image is  $\sim 290$  s, while the assumed exposure time for each MEMS Wolter type-I simulation image is set at  $\sim 8$  ks.

We plan to start fabricating the flight model Wolter type-I optics for ORBIS GEO-X soon. New technologies under testing to improve the angular resolution and the effective area are promising. In parallel, shock and thermal tests for a test optic will be conducted. We hope to finish all these development items within the schedule and launch the two optics in the early 2020s.

## 4 Summary

To summarize, future small missions such as ORBIS and GEO-X need new ultralightweight telescopes with a moderate angular resolution at a short focal length and/or a wide field of view. Our MEMS x-ray optics are ideal for these purposes. We have

demonstrated x-ray reflection and imaging with this method. Now we are improving the angular resolution and the effective area by introducing new cutting edge technologies. We hope to verify this new telescope in ORBIS and GEO-X, and then with other small or medium satellite missions as well as solar system explorations to Jupiter or Mars in the late 2020s, Fig. 10 shows simulated images using an ROSAT all-sky survey 3/4 keV band image near the Galactic center. Our final goal is to achieve angular resolution comparable to the ROSAT all-sky survey.

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