

A theoretical study for high-performance inverted p-i-n architecture perovskite solar cells with cuprous iodide as hole transport material

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ABSTRACT

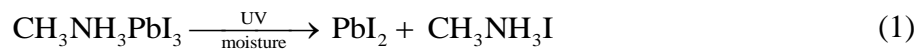
Inverted perovskite solar cells (p-i-n PSCs) have been fascinated due to rapid progress of performance in recent years. PEDOT: PSS is commonly used hole transport material (HTM) in p-i-n PSCs which is hygroscopic and acidic in nature that leads towards poor performance of device thus hinders commercialization of PSCs. Therefore, it is necessary to replace PEDOT: PSS with stable HTM in p-i-n PSCs. In this paper, theoretical study is carried out to investigate various physical parameters that can affect the performance of p-i-n PSCs with copper iodide (CuI) as HTM and phenyl-C61-butyric acid methyl ester (PCBM) as ETM. These parameters include the effect of doping density of ETM, absorber, and HTM as well as defect density and thickness of absorber on the performance of p-i-n PSCs. In addition, hole mobility and thickness of HTM is also investigated. It is found that performance of p-i-n PSC is strongly dependent on defect density and thickness of absorber layer while other physical parameters have minor influence on the performance of device. Upon final optimization, device attains PCE of more than 21 % which is encouraging. These results show that CuI as HTM is a potential choice for p-i-n PSCs.

Keywords: theoretical study, p-i-n PSCs, CuI, PCBM, defect density, PEDOT: PSS

1. Introduction

In 2009, $\text{CH}_3\text{NH}_3\text{PbI}_3$ and $\text{CH}_3\text{NH}_3\text{PbBr}_3$ were utilized as absorber materials by Miyasaka and colleagues in which PCE of more than 3 % was achieved [1]. There had been much research work done to optimize the efficiency of n-i-p type PSCs [2–4]. Various types of PSCs, such as perovskite-sensitized solar cells, mesoporous structured PSCs and Planar heterojunction PSCs had been studied in previous few years [1,5,6]. Mesoporous TiO_2 layers have the disadvantage of high temperature processing, therefore, the simplest design was planar hetero-junction structure [7–9]. In comparison with the mesoporous structured PSCs, planar PSC doesn't contain mesoporous layers, which simplifies production processes. In the meantime, planar PSCs, silicon and CIGS solar cells were also used to create tandem solar cells and device efficiency was further improved [10]. Planar PSCs have, therefore, attracted much attention in the field of photovoltaics [11]. Two types of planar PSCs are available such as normal and inverted structure. Normal PSCs with n-i-p structure are commonly comprised of TiO_2 as ETM, $\text{CH}_3\text{NH}_3\text{PbI}_3$ as absorber, and spiro-MeOTAD as HTM. However, the high manufacturing cost of spiro-MeOTAD and high temperature processing of TiO_2 offer hurdles in the commercialization of PSCs. In order to overcome these drawbacks, inverted PSCs with p-i-n structure have been developed with PEDOT:PSS as HTM and PCBM as ETM, which exhibited the promising efficiencies about 18 % [12]. Inverted PSCs have gained great popularity due to low temperature processing techniques [13,14] and less current hysteresis [15,16]. PEDOT:PSS is a widely used HTM in p-i-n type PSCs due to its high work function, better film deposition, optical transparency and high conductivity[17]. But at the same time, PEDOT:PSS suffers some critical issues such as hygroscopic and acidic nature which causes degradation and reduces the stability of the device. Furthermore, Inverted structure of PSCs is desirable for future roll-to-roll production because of low temperature and simple

manufacturing processes [18,19]. In order to fabricate an efficient device, degradation process in PSCs should be controlled as $\text{CH}_3\text{NH}_3\text{PbI}_3$ is vulnerable to moisture and oxygen and easily degraded [20]. TiO_2 is commonly used ETM in PSCs and has photocatalytic behavior thus sensitive to ultraviolet (UV) light and has the issue of photo-stability[21]. Performance is deteriorated when UV light irradiated on front transparent electrode of PSCs. UV light is absorbed in TiO_2 then photo-generated holes reacts with the adsorbed O_2 which creates the O_2 radical that act like a deep trap [22]. On desorbing the absorbed O_2 , electron is generated which recombines with hole of valence band. When light is absorbed in the absorber, photo induced electrons of absorber layer either move to conduction band of TiO_2 or be surrounded by the deep traps. The remaining electrons due to the desorption of O_2 then recombine with the photo induced holes from absorber layer. Equations (1)-(4) represent the degradation process in absorber layer in the case of $\text{CH}_3\text{NH}_3\text{PbI}_3$ when it comes in contact with moisture and UV light. PbI_2 and $\text{CH}_3\text{NH}_3\text{I}$ are produced as in equation (1). In equation (2), $\text{CH}_3\text{NH}_3\text{I}$ is further decomposed to CH_3NH_2 and HI . HI can be decomposed in two different routes. In the 1st route (equation (3)), I_2 and water is produced when HI comes in contact with oxygen. In the 2nd route (equation (4)), photochemical breakdown occurs and HI is converted into I_2 and H_2 due to UV radiation [23].



Theoretical analysis is as equally important as experimental study to realize working mechanism and performance optimization of device. In terms of inorganic HTMs in Pb-based inverted PSCs, device simulation has not been performed appreciably so far. For example, $\text{CH}_3\text{NH}_3\text{PbI}_{3-x}\text{Cl}_x$

based inverted PSC with NiO as HTM was simulated using SCAPS and PCE was achieved more than 20 % after optimization [24]. Furthermore, other device simulations of inverted PSCs were also performed with NiO as HTM [25–27]. In another device simulation, PSC was investigated with various HTMs including CuI in which only initial simulation was performed without any study of influence of physical parameters on performance of inverted PSC with CuI as HTM [28]. Therefore, it is dire need to further explore inorganic HTMs with hygroscopic as well as thermally and chemically stable nature. In this regard, CuI may be a suitable choice to be used as HTM in p-i-n type PSCs. In this study, inverted PSC has been explored with CuI as HTM because of its photostable and hydrophobic, which provides the shielding to absorber from moisture and UV light [29]. In addition, high transmittance of CuI in the range of visible light (400 nm to 800 nm) allows the absorbance of more incident photon flux and the generation of more charge carriers [30,31]. The structure FTO/CuI/CH₃NH₃PbI₃/PCBM/Al is used for the device modeling of proposed device. The influence of the thickness of absorber and CuI layers, the doping concentrations of CuI, absorber and PCBM layers as well as defect density of absorber and hole mobility of CuI on PSC device performance have been investigated.

2. Simulated device architecture and computational details

The device engineering of p-i-n type PSC is carried out with device architecture FTO / CuI / CH₃NH₃PbI₃ / PCBM / Al as discussed above. The schematic structure of the device is shown in **Figure 1a**. FTO is used as front electrode. CuI is applied as HTM, CH₃NH₃PbI₃ is designated as absorber, PCBM is acted as ETM and Al is used as back metal contact. The band alignment is shown in **Figure 1b**. It is evident that VBO of + 0.3 eV at the interface (CuI/absorber) is very critical for the transport of the holes, and the CBO at absorber/PCBM interface is - 0.2 eV which is also very important for transport of photo-generated electrons. Two defect interfaces are used in

order to analyze carrier recombination. One defect interface is $\text{CH}_3\text{NH}_3\text{PbI}_3 / \text{PCBM}$ and the other one is $\text{CuI} / \text{CH}_3\text{NH}_3\text{PbI}_3$. The defect type is chosen as single with defect density of $1 \times 10^{10} \text{ cm}^{-3}$. Defect parameters of interfaces and material properties of each layer are shown in **Tables 1** and **2** respectively.

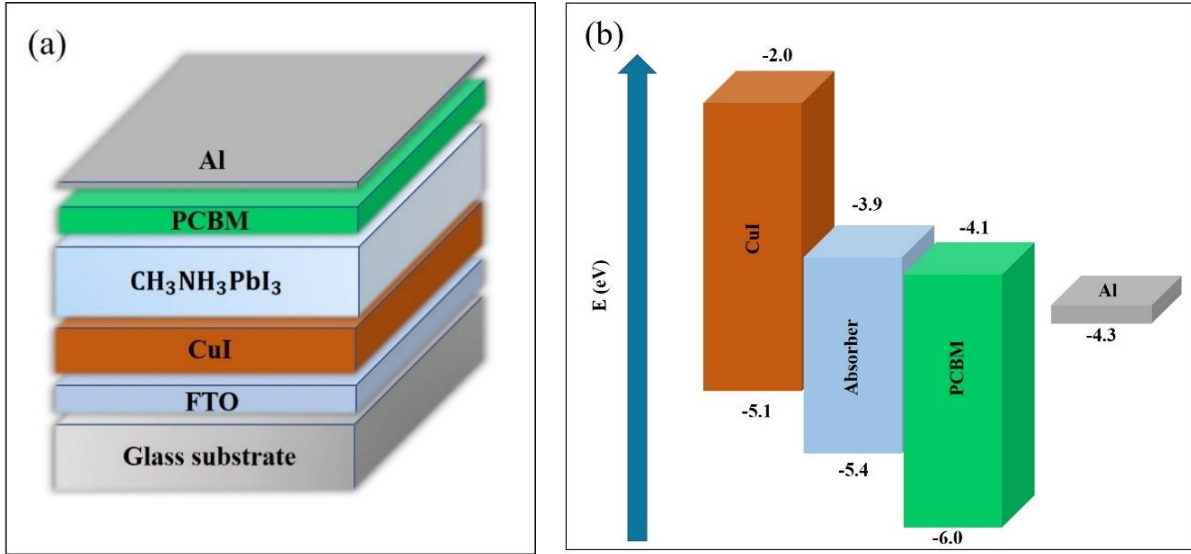


Figure 1. (a) Schematic diagram of inverted PSC with CuI as HTM (b) Band alignment diagram of inverted PSC with CuI as HTM

Parameters	CuI/ $\text{CH}_3\text{NH}_3\text{PbI}_3$ interface	$\text{CH}_3\text{NH}_3\text{PbI}_3$	$\text{CH}_3\text{NH}_3\text{PbI}_3/\text{PCBM}$ interface
Defect type	Neutral	Neutral	Neutral
Capture cross section for holes (cm^2)	1×10^{-19}	2×10^{-14}	1×10^{-19}
Capture cross section for electrons (cm^2)	1×10^{-19}	2×10^{-14}	1×10^{-19}
Energetic distribution	Single	Single	Single
Energy level with respect to E_v (eV)	0.600	0.100	0.600
Characteristic energy (eV)	0.1	0.1	0.1
Total density (cm^{-3})	1×10^{10}	1×10^{14} to 1×10^{19}	1×10^{10}

Parameters	FTO	HTM (CuI)	Absorber (CH ₃ NH ₃ PbI ₃)	ETM (PCBM)
Thickness (μm)	0.500	0.400	0.250	0.010
Relative permittivity ϵ_r	9	6.5[32]	6.5 [33]	4 [34]
Hole mobility μ_p ($\text{cm}^2 \text{V}^{-1}\text{s}^{-1}$)	8	1.69×10^{-4} [35]	10	2×10^{-4} [36]
Acceptor concentration N_A (cm^{-3})	0	2×10^{17} [37]	1×10^{17} [38]	0
Electron mobility μ_n ($\text{cm}^2 \text{V}^{-1}\text{s}^{-1}$)	20	1.69×10^{-4}	10 [39]	2×10^{-3}
Donor concentration N_D (cm^{-3})	2.0×10^{19}	0	0	1×10^{16} [40]
Effective valance band density N_v (cm^{-3})	1.8×10^{19}	1.0×10^{19} [41]	1.8×10^{19} [42]	1.0×10^{19} [43]
Band gap energy E_g (eV)	3.5	3.1 [44]	1.50 [45]	1.9 [46]
Defect density N_t (cm^{-3})	1×10^{15}	1×10^{16}	1×10^{16}	1×10^{14}
Effective conduction band density N_c (cm^{-3})	2.0×10^{18}	2.8×10^{19} [41]	2.2×10^{18} [42]	1.5×10^{18} [47]
Electron affinity χ (eV)	4	2.1 [48]	3.9 [49]	3.9 [50]

Table 1. Defect parameters of interfaces and absorber of p-i-n type PSC with CuI as HTM

Table 2. Simulation parameters of inverted PSC with CuI as HTM.

3. Results and discussion

The J-V curve has been drawn with the physical parameters given in **tables 1** and **2** as shown in curve (a) of **Figure 2a**. J_{sc} of 18.29 mA/cm^2 , V_{oc} of 1.05 V , FF of 65.33% , and PCE of 12.56% are obtained. The simulated device performance and experimental results are consistent for inverted Pb-based PSCs [51]. CuI layer is highly transparent in the visible range from $400 - 800 \text{ nm}$ and this high transparency makes CuI more suitable as HTM in inverted PSC so that more photons can reach absorber to generate charge carriers [52]. From **Figure 2b**, optical absorption edge and maximum absorbance lie at 850 nm and 400 nm respectively in quantum efficiency (QE)

curve covering visible spectrum which is in agreement with experimental work [16]. This agreement validates that input simulation parameters are close to the real device.

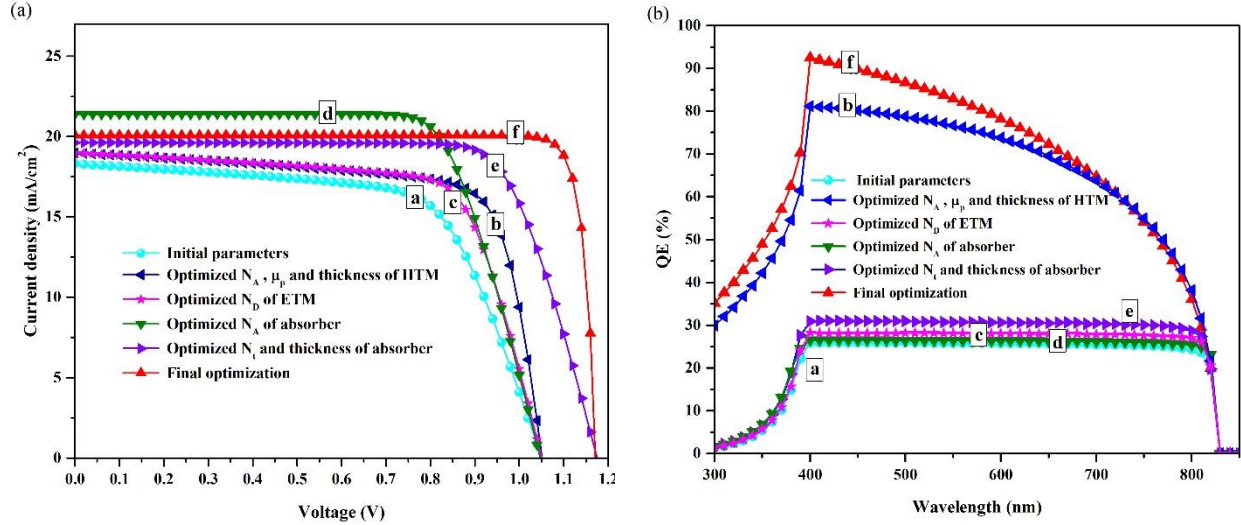


Figure 2. Simulated optimized (a) J-V (b) QE characteristics of inverted PSC

3.1 Influence of doping density (N_A), hole mobility (μ_p) and thickness of CuI layer

N_A of CuI is directly related to the recombination rate and energy bands. Therefore, performance of PSCs is considerably influenced by N_A . J_{sc} is almost constant when N_A of CuI is smaller than $1 \times 10^{15} \text{ cm}^{-3}$. But, J_{sc} increases when N_A of CuI increases from $1 \times 10^{15} \text{ cm}^{-3}$ to $1 \times 10^{18} \text{ cm}^{-3}$ and becomes almost constant beyond $1 \times 10^{18} \text{ cm}^{-3}$ as shown in **Figure 3a**. V_{oc} is observed to be decreasing when N_A is smaller than $1 \times 10^{14} \text{ cm}^{-3}$ and shows saturated behavior with increasing N_A from $1 \times 10^{14} \text{ cm}^{-3}$ to $1 \times 10^{20} \text{ cm}^{-3}$ as shown in **Figure 3a**. FF is observed to be increasing slowly with the increasing N_A up to $1 \times 10^{16} \text{ cm}^{-3}$ then increases rapidly up to $1 \times 10^{20} \text{ cm}^{-3}$. Similarly, PCE also exhibits the same trend with increasing N_A as shown in **Figure 3a**. **Figure 3b** shows that total recombination of charge carriers sharply decreases when N_A increases from $1 \times 10^{15} \text{ cm}^{-3}$ to $1 \times 10^{17} \text{ cm}^{-3}$ which justifies the sharp increase in J_{sc} . Equation (5) can be used to express V_{oc} .

$$V_{oc} = \frac{k_B T}{e} \ln \left(\frac{I_{ph}}{I_s} + 1 \right) \quad (5)$$

Where I_{ph} is photocurrent and I_s is reverse saturation current. It is shown in **Figure 5** that height of the potential barrier increases with the increase of N_A which results in the decrease of I_s . Therefore, V_{oc} increases with the increase of N_A which is also justified by equation (5) and peak value of V_{oc} is obtained (1.05 V) which is exhibited by the plateau in the **Figure 3a**. Finally, it can be seen that N_A has optimized value of $1 \times 10^{19} \text{ cm}^{-3}$. μ_p is the measurement of transport of holes when external electric field is applied. N_A also affects the μ_p of HTM defines its limits the μ_p due to impurity scattering and lattice scattering respectively.

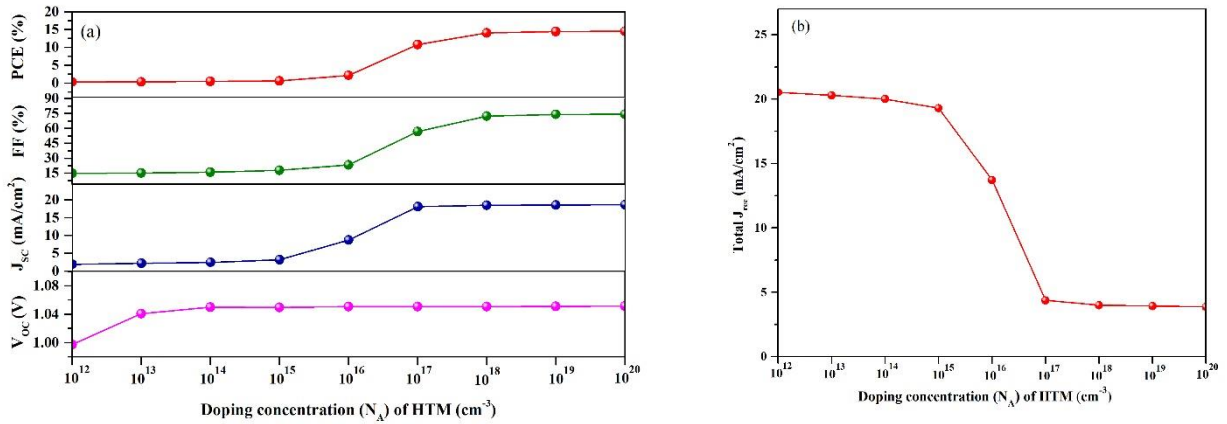


Figure 3. Performance variations of inverted PSC with (a) increasing N_A of HTM (b) total recombination current with the N_A of HTM

The influence of μ_p of CuI has been analyzed on the performance of proposed inverted PSC. J_{sc} and PCE increases with the increase of μ_p of HTM which leads towards the improved charge extraction and charge transport at HTM / absorber interface as shown in **Figure 4a**. FF also increases with the increase of μ_p while V_{oc} remains almost constant. The optimized μ_p is found to be $1 \times 10^{-2} \text{ cm}^2 \text{ V}^{-1} \text{ s}^{-1}$. Furthermore, thickness of CuI as HTM has vital role on the performance of device as generation and recombination rate are affected by the variation in thickness of CuI in

PSC. It is shown from **Figure 4b** that J_{sc} increases when thickness of CuI increases from 0.01 μm to 0.1 μm and then decreases with the increasing thickness of CuI onwards. V_{oc} remains unaffected with the increasing thickness of CuI which indicates that resistivity increases with the increasing thickness of CuI.

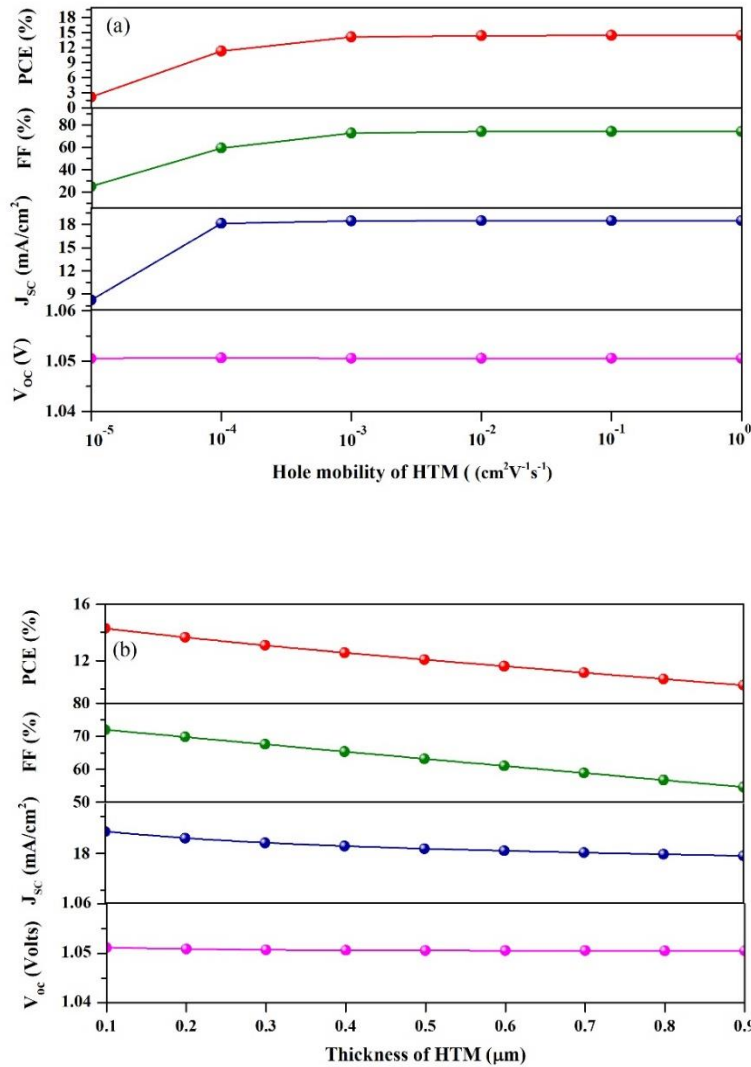


Figure 4. Performance variations of inverted PSC with (a) increasing μ_p (b) increasing thickness of HTM

The best FF is 73 % which is obtained when thickness is 0.1 μm and poor FF is 58 % which is obtained when thickness is 0.9 μm . At the end, optimum performance with J_{sc} of 18.97 mA/cm^2 , PCE of 14.81 %, FF of 74.26 % and V_{oc} of 1.05 V is obtained under the optimized N_{A} of $1 \times 10^{19} \text{ cm}^{-3}$, μ_{p} of $1 \times 10^{-2} \text{ cm}^2 \text{ V}^{-1} \text{ s}^{-1}$ and thickness of 0.1 μm (100 nm). The optimized J-V curve and QE curve are shown in curve (b) of **Figure 2(a-b)**.

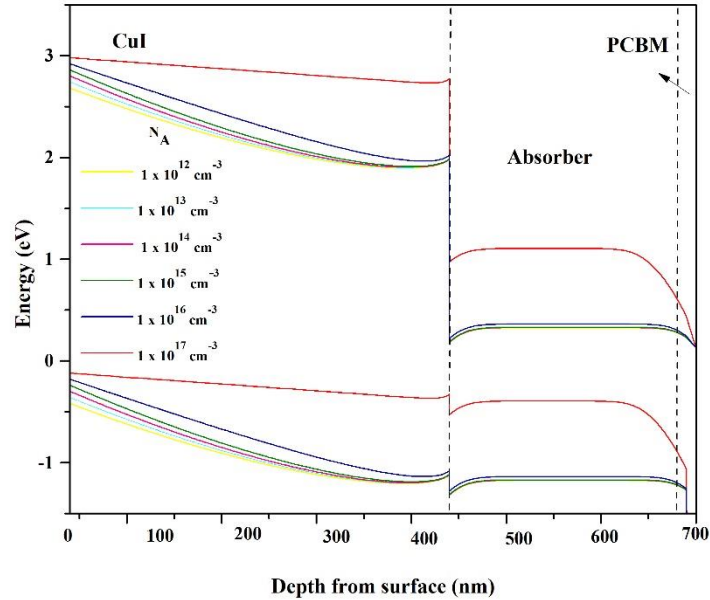


Figure 5. Energy band diagram of inverted PSC with various N_{A} values of CuI

3.2 Influence of doping density (N_{D}) of PCBM layer

The influence of N_{D} of PCBM will be discussed in this section. PCBM is used as ETM in PSC because it has well matched highest occupied molecular orbital (HOMO) and lowest unoccupied molecular orbital (LUMO) with CB and VB of absorber which facilitates the better electron transport to PCBM. At the absorber / PCBM interface, transport of holes is ceased due to low lying HOMO of PCBM as compared to CB of absorber [53]. From **Figure 6a**, J_{sc} is almost constant with the increasing N_{D} of PCBM. This is due to the fact that net generation rate of charge carriers is also constant with the increasing N_{D} of PCBM (**Figure 6b**). V_{oc} increases when N_{D} of PCBM

increases from $1 \times 10^{13} \text{ cm}^{-3}$ to $1 \times 10^{15} \text{ cm}^{-3}$ and saturates to 1.05 V when N_D exceeds $1 \times 10^{15} \text{ cm}^{-3}$ as shown in **Figure 6a**. Since height of potential barrier increases with the increasing of N_D of PCBM, which results in the decrease of I_s . Therefore, V_{oc} increases with the increase of N_D evident from equation (5).

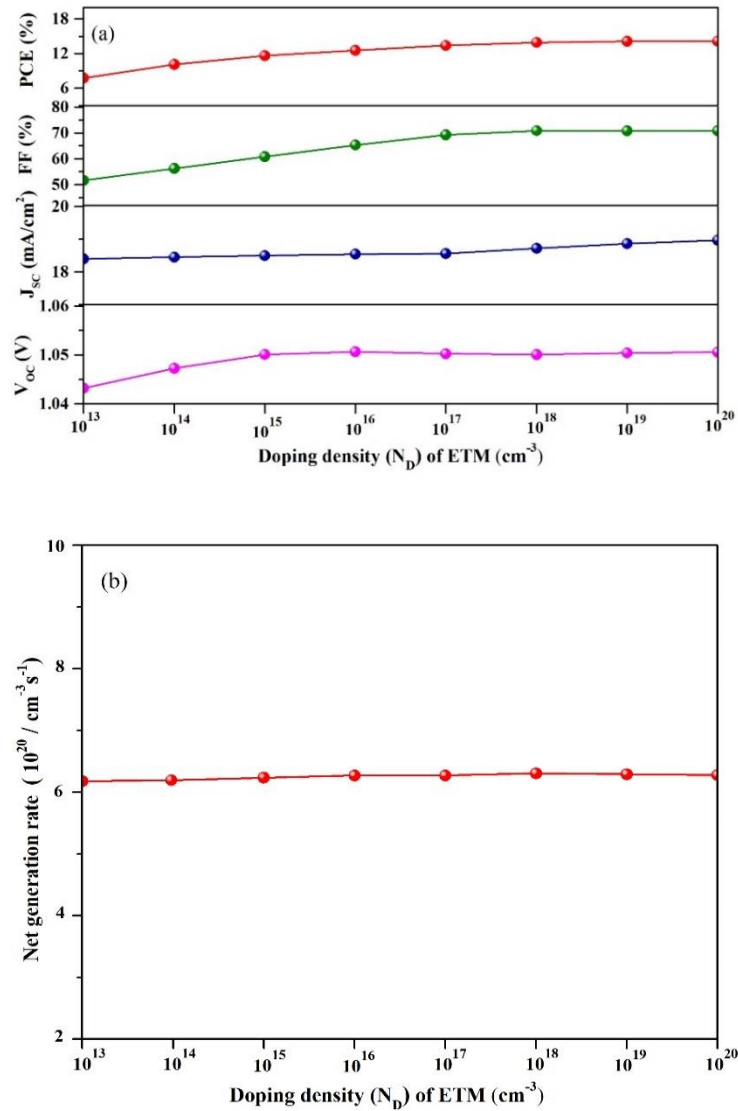


Figure 6. (a) Performance variations of inverted PSC (b) net generation rate of inverted PSC with increasing N_D of ETM

It is also evident that fall in I_s becomes slow when N_D exceeds $1 \times 10^{15} \text{ cm}^{-3}$ leads towards saturated V_{oc} . FF increases when N_D of PCBM increases from $1 \times 10^{10} \text{ cm}^{-3}$ to $1 \times 10^{18} \text{ cm}^{-3}$ and then saturates to 70.8 % upon exceeding the value of N_D from $1 \times 10^{18} \text{ cm}^{-3}$. This leads towards the decrease in resistivity with the increasing N_D of PCBM shown in **Figure 6a**.

PCE increases when N_D of PCBM increases from $1 \times 10^{13} \text{ cm}^{-3}$ to $1 \times 10^{18} \text{ cm}^{-3}$ and saturates to 14.1 % upon exceeding the value of N_D from $1 \times 10^{18} \text{ cm}^{-3}$ as shown in **Figure 6a**. Finally, optimized performance with J_{sc} of 19.01 mA/cm^2 , PCE of 14.01 %, FF of 70.80 % and V_{oc} of 1.05 V is obtained under the optimized N_D of $1 \times 10^{19} \text{ cm}^{-3}$ of PCBM. The curve (c) of **Figure 2(a-b)** represents optimized J-V curve and QE curve with optimized N_D of ETM.

3.3 Influence of N_A of absorber

Doping in absorber layer can enhance the performance of PSCs. Doping (n-type or p-type) depends on nature of dopants. The absorber layer in PSCs can be doped by self-doping process. Majority charge carrier type, carrier transport and density can be manipulated by n-type or p-type self-doping process in absorber layer. Lead iodide (PbI_2) and methyl ammonium iodide (MAI) are inorganic and organic precursors respectively used in the formation of absorber ($\text{CH}_3\text{NH}_3\text{PbI}_3$) layer. Furthermore, doping of absorber depends on the precursor ratio (MAI / PbI_2) [54]. On thermal annealing, MAI rich absorber is p-doped while MAI deficit absorber is n-doped [55].

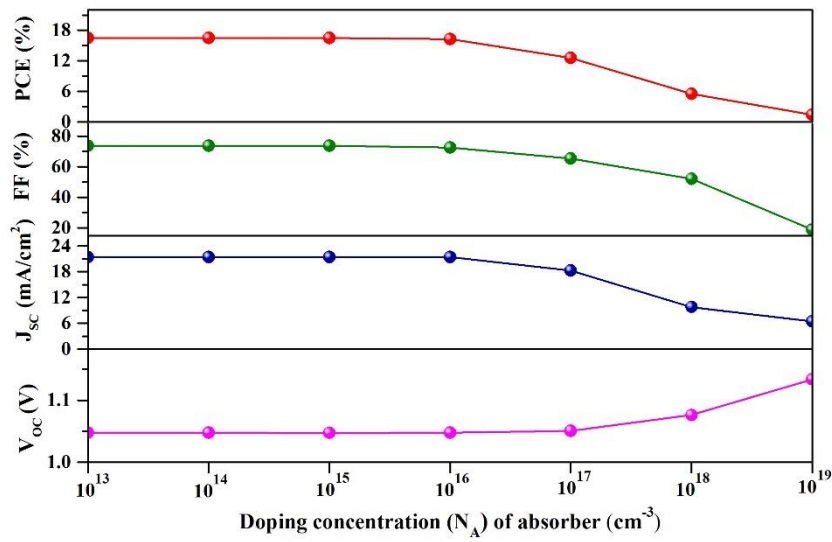


Figure 7. Performance variations of inverted PSC with increasing N_A of absorber

Figure 7 shows the variation in PCE with increasing N_A of absorber. When N_A is $1 \times 10^{15} \text{ cm}^{-3}$ then PCE is maximum and J_{sc} also has the same trend, which shows the better transport and collection of charge carriers across absorber layer. Thus, performance of PSCs can be improved by proper selection of N_A of absorber. When N_A increases beyond $1 \times 10^{15} \text{ cm}^{-3}$, J_{sc} begins to decrease. The internal electrical field is strengthened with the increasing N_A which has very critical role in the performance variation of PSCs. Auger recombination increases with the increasing N_A which is

responsible for the decrease in J_{sc} . The hole transport is also suppressed by various scattering and recombination processes caused by increasing N_A [56]. Therefore, PCE of PSC is increased by enhancing the V_{oc} and J_{sc} with optimum N_A but recombination and scattering processes become prominent with further increase in N_A . Moreover, charge carrier mobility within absorber can be increased at low concentration of charge carriers. The performance is optimized with V_{oc} of 1.05 V, J_{sc} of 21.4 mA/cm², FF of 73.6 % and PCE of 16.4 % when N_A is 1×10^{15} cm⁻³. The comparison between initial and optimized J-V and QE curves are shown in curve (a) and (d) of **Figure 2(a-b)** respectively.

3.4 Influence of N_t and thickness of absorber

N_t is another important absorber's parameter that needs to be discussed. The quality and morphology of absorber layer significantly changes the device performance[57]. Photoelectrons are generated when light is absorbed in the absorber layer. Poor quality of absorber layer leads towards poor coverage of PCBM layer by lead perovskite [58,59]. Recombination rates in absorber layer become dominant when N_t increases leading towards poor quality of film. Diffusion length is the average distance travelled by charge carriers before recombination. Shockley-Read-Hall recombination is the major phenomenon in order to calculate the recombination rate of charge carriers as mentioned in equations (6) – (9).

$$R^{SRH} = \frac{n \cdot p - n_i^2}{\tau_p \cdot (n_o + n') + \tau_n \cdot (p_o + p')} \quad (6)$$

n_o and p_o show the electron and hole concentrations at equilibrium respectively while n' and p' shows electron and hole concentrations in trap defects and valence band respectively. These are expressed as

$$n' = N_c \cdot \exp\left(\frac{-(E_c - E_T)}{k_B \cdot T_L}\right) \quad (7)$$

$$p' = N_v \cdot \exp\left(\frac{-(E_T - E_v)}{k_B \cdot T_L}\right) \quad (8)$$

n_i is the intrinsic carrier concentration while T_L is lattice temperature and E_T is the energy level of trap defect. k_B is Boltzmann constant.

$$n_i^2 = n_o p_o = n' p' = N_c N_v \exp\left(\frac{-E_g}{k_B \cdot T_L}\right) \quad (9)$$

when E_g (eV) $\gg 3k_B T_L$ then thermally generated n_i^2 can be neglected.

In addition to above equations, equations (10) – (12) are used to calculate electron and hole diffusion lengths (L_n and L_p). $\tau_{n,p}$ is carrier life time which can be given as .

$$\tau_{n,p} = \frac{1}{\sigma_{n,p} v_{th} N_t} \quad (10)$$

v_{th} represents thermal velocity and is equal to 10^{+7} cm / s while $\sigma_{n,p}$ represents capture cross-section of charge carriers and N_t is the density of trap defect. Diffusion coefficient (D) is given by

$$D = \frac{\mu k_B T}{q} \quad (11)$$

μ is the carrier mobility, T and q signifies temperature (kelvin) and charge magnitude respectively.

Diffusion length (L) is given as

$$L = \sqrt{D\tau} \quad (12)$$

The validity of simulation is affected very little by ignoring the difference between electron and hole diffusion length. The initial value of N_t is set to be 1×10^{16} cm⁻³ in absorber. When N_t increases in absorber layer then performance of PSC is deteriorated as shown in **Figure 8b**. The effect of N_t on device performance is analysed by considering the diffusion length of charge

carriers which in turn depends on the SRH recombination rate and diffusion length formula. Diffusion length is changed from 113.7 μm to 0.4 μm by changing N_t from 1×10^{14} to $1 \times 10^{19} \text{ cm}^{-3}$ respectively as shown in **Table 3**. The strong impact of N_t is observed on FF which is an important parameter affecting the efficiency of PSCs. FF is as low as ~42 % at N_t of $1 \times 10^{19} \text{ cm}^{-3}$ and saturates to ~74 % for N_t smaller than $1 \times 10^{14} \text{ cm}^{-3}$. V_{oc} and J_{sc} also saturate to 1.17 V and 21.38 mA/ cm^2 for N_t smaller than $1 \times 10^{15} \text{ cm}^{-3}$. FF is the most sensitive to N_t among all the performance parameters of PSCs. Performance of PSCs is affected by another critical parameter which is thickness of absorber layer. **Figure 8a** shows the influence of absorber thickness on the device performance. Thin layer of absorber leads towards poor absorption of light causing low PCE. When absorber thickness increases, PCE increases as well which yields peak value at thickness of 200 nm. When absorber's thickness is increased beyond 200 nm then recombination rate of photogenerated charge carriers increases causing low performance. The optimum performance with V_{oc} of 1.17 V, J_{sc} of 17.61 mA/ cm^2 , FF of 75.35 % and PCE of 17.37 % is achieved with N_t of $1 \times 10^{14} \text{ cm}^{-3}$ and thickness of 200 nm of absorber layer. The optimized J-V and QE curves are shown in curve (e) of **Figure 2(a-b)**.

Table 3. Diffusion length of carriers in absorber layer with corresponding N_t

N_t (cm^{-3})	1×10^{14}	1×10^{15}	1×10^{16}	1×10^{17}	1×10^{18}	1×10^{19}
Diffusion length (μm)	113.7	35.9	11.4	3.6	1.1	0.4

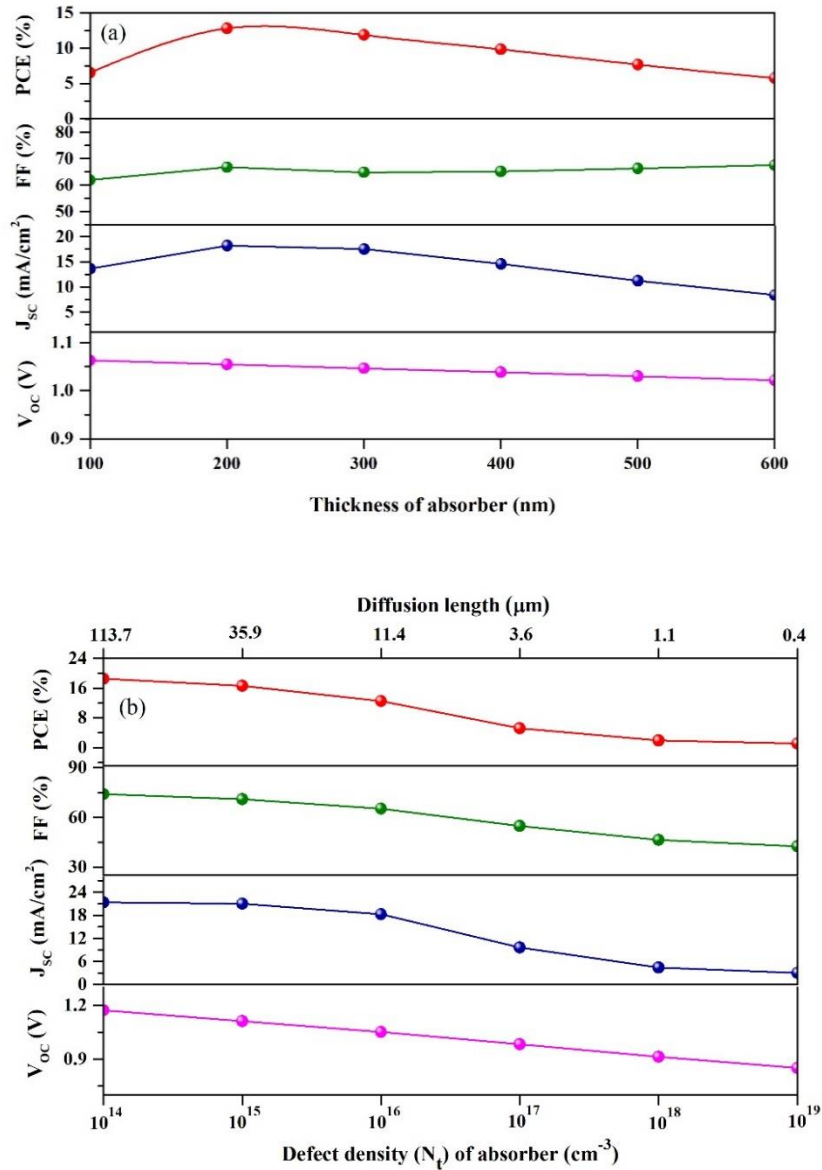


Figure 8. Performance variations of inverted PSC with increasing (a) thickness (b) N_t of absorber

Finally, performance parameters such as V_{oc} of 1.17 V, J_{sc} of 20.08 mA/cm², PCE of 21.06 % and FF of 89.45 % are obtained on optimizing the physical parameters given in **Table 4**. These results are very encouraging as in previously available literature so far, best PCE of 18.4 % for inverted PSC with CuI as HTM was achieved. Final optimised J-V curve is shown in curve (f) of **Figure 2a**. **Table 5** shows the comparison between our simulated results and previously reported

experimental results which also exhibited that better simulation results are achieved on the device modeling of inverted PSC. In the literature, J_{sc} of 22.6 mA/cm² was reported to be higher than J_{sc} through our simulation but V_{oc} and FF are still needed to improve for achieving PCE upto 21.06 %.

Table 4. Optimized parameters of the inverted PSC with CuI as HTM

Optimized parameters	HTM (CuI)	Absorber (CH ₃ NH ₃ PbI ₃)	ETM (PCBM)
Doping density (cm ⁻³)	1×10^{19}	1×10^{15}	1×10^{19}
Defect density (cm ⁻³)	-	1×10^{14}	-
Thickness (nm)	100	200	-
Hole mobility (cm ² V ⁻¹ s ⁻¹)	1×10^{-2}	-	-

Table 5. Performance parameters of inverted PSCs with CuI as HTM for simulated results as well as experimental work reported in the literature.

Parameters	Our simulation results						Experimental results				
	Initial	Optimized N _b of ETM	Optimized μ_p , thickness and N _A of HTM	Optimized N _A of absorber	Optimized N _i and thickness of absorber	Final optimization	[51]	[52]	[60]	[61]	[62]
PCE (%)	12.56	14.10	14.81	16.4	17.37	21.06	12.0	13.58	14.53	16.8	18.4
FF (%)	65.33	70.80	74.26	73.6	75.35	89.45	65.0	62	69	71.3	80.2
J_{sc} (mA/cm ²)	18.29	19.01	18.97	21.4	19.61	20.08	17.3	21.06	20.05	22.6	22.5
V_{oc} (V)	1.05	1.05	1.05	1.05	1.17	1.17	1.03	1.04	1.05	0.99	1.02

This may be achieved by the improvement of crystalline quality and film morphology of absorber and HTM layer. Doped absorber and CuI could further improve the layer and interface quality by replacement of either a part of I or Cu by another element.

4. Conclusion

In this work, theoretical study of p-i-n PSC is carried out in order to find substitute HTM for PEDOT: PSS which is hygroscopic and acidic in nature causing the degradation of the device. Various factors affecting the performance of the device were investigated. These factors include doping density of CuI, PCBM and absorber, along with hole mobility and thickness of CuI, as well as defect density and thickness of absorber. Based on device modeling results, PCE of 16.49 %, J_{sc} of 21.43 mA/cm², FF of 73.6 % and V_{oc} of 1.05 V were obtained after optimizing the doping density of absorber as 1×10^{17} cm⁻³. Further optimization of defect density and thickness of absorber, PCE of 17.37 %, V_{oc} of 1.17 V, FF of 75.35 % and J_{sc} of 19.61 mA/cm² was achieved. Finally, PCE as high as 21.06 %, J_{sc} of 20.08 mA/cm², FF as high as 89.45 % and V_{oc} as high as 1.17 V were achieved upon the optimization of above-mentioned parameters. This research work analyzed the working mechanism of inverted PSC and studied the influence of key physical parameters on the performance of device. Furthermore, CuI is highly hydrophobic which prevent moisture to reach the absorber and from direct contact with FTO, therefore reducing charge recombination at interfaces and enhancing the performance of device. Hence, it is obviously beneficial to use CuI as HTM for the fabrication of stable, efficient and cost-effective p-i-n PSCs. These results show that inverted PSC with CuI as an inorganic HTM has excellent performance compared to widely used organic HTM PEDOT: PSS. CuI is cost effective showing thermal as well as moisture stability which is better alternate to PEDOT: PSS.

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Conflict of Interest

The authors declare no conflict of interest.

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Graphical abstract

