

Audit feasibility for geometric distortion in magnetic resonance imaging for radiotherapy



Meshal Alzahrani^{a,b,*}, David A Broadbent^c, Robert Chuter^{d,e}, Bashar Al-Qaisieh^c, Steven Jackson^d, Hutton Michael^d, Robert I Johnstone^f, Simon Shah^f, Andreas Wetscherek^g, H. Joan Chick^g, Jonathan J Wyatt^{h,i}, Hazel Mhairi McCallum^{h,i}, Richard Speight^c

^a Department of Diagnostic Radiology, Faculty of Applied Medical Sciences, King Abdulaziz University, Jeddah, Saudi Arabia

^b Biomedical Imaging Science Department, Leeds Institute of Cardiovascular and Metabolic Medicine, University of Leeds, Leeds, UK

^c Department of Medical Physics and Engineering, Leeds Teaching Hospitals NHS Trust, Leeds, UK

^d Christie Medical Physics and Engineering (CMPE), The Christie NHS Foundation Trust, Manchester, UK

^e Division of Cancer Sciences, Faculty of Biology, Medicine and Health, University of Manchester, Manchester, UK

^f Guy's and St Thomas' NHS Foundation Trust, London, UK

^g Joint Department of Physics at the Institute of Cancer Research and the Royal Marsden NHS Foundation Trust, London, UK

^h Northern Centre for Cancer Care, Newcastle upon Tyne Hospitals NHS Foundation Trust, Newcastle, UK

ⁱ Centre for Cancer, Newcastle University, Newcastle, UK

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ABSTRACT

Background and purpose: Magnetic Resonance Imaging (MRI) is increasingly being used in radiotherapy (RT). However, geometric distortions are a known challenge of using MRI in RT. The aim of this study was to demonstrate feasibility of a national audit of MRI geometric distortions. This was achieved by assessing large field of view (FOV) MRI distortions on a number of scanners used clinically for RT.

Materials and methods: MRI scans of a large FOV MRI geometric distortion phantom were acquired on 11 MRI scanners that are used clinically for RT in the UK. The mean and maximum distortions and variance between scanners were reported at different distances from the isocentre.

Results: For a small FOV representing a brain (100–150 mm from isocentre) all distortions were < 2 mm except for the maximum distortion of one scanner. For a large FOV representing a head and neck/pelvis (200–250 mm from isocentre) mean distortions were < 2 mm except for one scanner, maximum distortions were > 10 mm in some cases. The variance between scanners was low and was found to increase with distance from isocentre.

Conclusions: This study demonstrated feasibility of the technique to be repeated in a country wide geometric distortion audit of all MRI scanners used clinically for RT. Recommendations were made for performing such an audit and how to derive acceptable limits of distortion in such an audit.

1. Introduction

Traditionally, computed tomography (CT) images have been used to inform radiotherapy (RT) treatment planning. Recently, interest in the use of magnetic resonance imaging (MRI) in RT has increased [1], owing to its superior soft-tissue contrast compared with CT [2].

MRI is typically used in RT to define the tumour and/or organ at risk volumes and then registered to CT for dose calculation. However, this method is susceptible to coregistration errors [3]. For this reason, the magnetic resonance-only (MR-only) pathway for RT planning has been developed to estimate electron density information directly from MRI images [4–6]. Furthermore, MRI-guided RT using a magnetic resonance

linear accelerator (MR-linac) is an emerging technology for RT treatments [7,8].

Geometric distortion remains an inherent issue with MRI that needs to be corrected for [9,10]. In RT planning, uncorrected geometric distortions can lead to target localisation uncertainties [11]. Geometric distortion is more significant when imaging a large field of view (FOV) such as the head and neck/pelvis, in some MR-only applications [12] and MRI-guided RT [13].

The causes of geometric distortions can be divided into two main categories: hardware-related and patient-related distortions. Patient-related distortions, such as chemical shift and magnetic susceptibility, arise due to variations in the magnetic susceptibility of different body

* Corresponding author.

E-mail address: mmzahrani@kau.edu.sa (M. Alzahrani).

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Table 1

MRI acquisition parameters recommended by the phantom manufacturer, and those used on each scanner. Note differences due to limitations in different scanners. Note: The dashes (–) mean the recommended parameters were used.

	Parameters recommended by phantom manufacturer	Siemens Aera, (all centers)	Prisma	Sola	Skyra	Espreo	Unity	Ingenia	GE PET/MR
Seq.	GRE	–	–	–	–	–	–	–	–
FoV (mm × mm)	500 × 500	–	–	–	–	450 × 450	–	501 × 375.5	–
Flip angle	20°	–	–	–	–	–	–	–	–
Number of slices	256	–	–	–	–	–	205	205	–
Slice thickness (mm)	1.95	–	–	–	–	1.75	–	–	–
Slice gap (mm)	0.39	–	–	–	–	0.35	0	0	0
phase-encoding direction	A ≫ P	–	–	–	–	–	–	–	–
TR (ms)	6.2	–	4.4	5.1	5	5	5	5	3.8
TE (ms)	2.18	–	1.58	1.81	1.78	2.39	2.5	–	1.3
Voxel size (mm ³)	1.0 × 1.0 × 2.0	–	–	–	–	–	–	–	–
Pixel BW (Hz/Pix)	490	–	–	488	–	–	–	–	–

tissues and the surrounding air [14]. The magnitude of the distortion can be affected by magnetic field strength, MRI sequence, patient anatomy, receiver bandwidth and the presence of implants [13,15]. Hardware-related distortions occur due to magnetic field inhomogeneity and gradient-nonlinearity [15]. Gradient-nonlinearity is the main cause of geometric distortion in MRI systems [16–18]. MRI scanner gradient performance can be specified both in terms of the maximum spatial gradient strengths that can be achieved and the rate at which the gradients can be switched (the slew rate). Achieving high gradient strengths and slew rates can lead to compromises in gradient linearity [18,19], which may compromise the scanner performance in terms of geometric accuracy.

Although manufacturers generally equip MRI scanners with algorithms that aim to correct hardware-related distortions [20], these are known not to be completely effective [1,21] with some residual geometric distortion generally remaining. Therefore, it is important to assess the magnitude of residual geometric distortion and a number of professional bodies offer advice on performing this. According to the American Association of Physicists in Medicine (AAPM) Report 100 [22], any lengths measured in an image should be within 2% of the true value if the image is to be used for RT purposes. The American College of Radiology (ACR) [23] recommends that length measurements be within ± 2 mm of the actual measurements for their accreditation programme, although this guidance is specific to their phantom.

Gustafsson et al. [17] studied the effects of geometric distortion on RT planning for prostate patients on a 3 T MRI scanner using the same a large FOV MRI distortion phantom used in this study. The repeatability of measurements with such a phantom have also been demonstrated by Wyatt et al. [24].

The first report in the literature assessing geometric distortion in various MRI scanners was from 2012 which compared six 3 T MRI scanners in the Scottish Imaging Network a platform for scientific excellence (SINAPSE) [25]. This work assessed geometric distortion over different imaging volumes quantitatively to ensure the suitability for application such as RT treatment planning.

The objective of the work presented here was to show feasibility of a method for auditing the geometric distortion on a range of MRI scanners used for clinical RT applications and to define procedures for future audits. A secondary objective was to enhance the literature by providing typical values of geometric distortion that can be used in future audits.

2. Materials and methods

A large FOV phantom was used to measure the geometric distortion on 11 MRI scanners, listed in appendix 1, with all major vendors assessed. To preserve anonymity randomly assigned numbers (1–11) were used to refer to scanners in this study.

The large FOV MRI geometric distortion phantom used in the study

was a GRADE phantom (Spectronic Medical AB, Helsingborg, Sweden). The phantom is a plastic container filled with a foam matrix with approximately 1200 spherical polyethylene glycol markers of 17 mm diameter at known locations. The MRI opaque markers are arranged in a grid with a spacing of approximately 50 mm in the central region and 30 mm in the outer region. The phantom size is 50.2 cm × 40.4 cm × 53.4 cm, and the imaging dimensions are 49 cm × 31 cm × 50 cm.

The GRADE phantom was setup on each MRI scanner to its crosshair markings using the scanner's internal lasers. Phased array body (anterior surface) and spine (integrated into the patient couch) coils were used where possible. For two scanners, where space constraints within the bore made this impossible, the integrated body coil was used instead (see appendix 1). Two consecutive MRI scans of the phantom were acquired on each MRI scanner, with the phantom removed from the MRI scanner couch and re-setup on the MRI scanner couch in between acquisitions. This was done to ensure that the distortions measured were reproducible and due to the scanner rather than attributed to setup errors.

A 3D gradient echo (GRE) sequence recommended by the phantom manufacturer was used where possible for all scanners, as defined in Table 1. Due to scanner limitations, some acquisition parameters had to be modified in a way that would not be expected to significantly affect the geometric distortion results. Standard 3D geometric distortion correction was applied for all acquired images. The vendor's standard automatic B₀ shimming mode was used with an adjustment volume identical to the field of view.

The software supplied with the GRADE phantom, MriPlanner (Spectronic Medical AB, Helsingborg, Sweden), was used for data analysis. The software reports the mean and maximum observed distortion (mm) at five distances from the isocentre: < 100 mm, 100–150 mm, 150–200 mm, 200–250 mm, and ≥ 250 mm.

The mean and maximum reported geometric distortion was measured for each distance to isocentre, for each MRI scanner and for each of the two consecutive measurements. The mean of the mean and maximum distortion of the two consecutive results per scanner are defined throughout as mean_{ps} and max_{ps}. For comparison purposes, the mean and standard deviation of mean_{ps} over all scanners, defined as mean_{mean-as} and SD_{mean-as} respectively, were calculated at each distance from the isocentre. Values that did not fall within mean_{mean-as} \pm 2SD_{mean-as} were considered statistically significant outliers. Similarly, the mean and standard deviation of max_{ps} over all scanners, defined as mean_{max-as} and SD_{max-as} respectively, was calculated at each distance from the isocentre. Values that did not fall within mean_{max-as} \pm 2SD_{max-as} were considered statistically significant outliers. In addition, the variance (δ^2) between scanners at each distance from the isocentre was calculated.

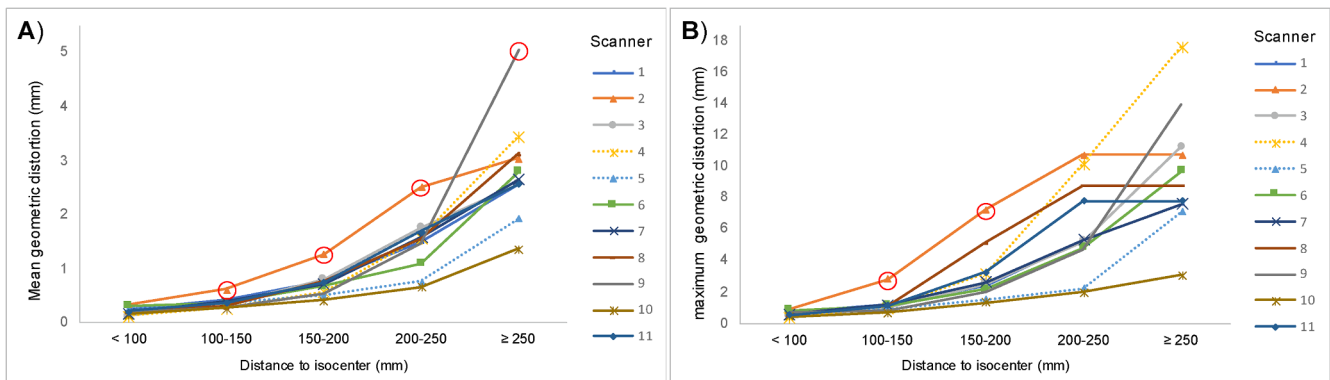


Fig. 1. Geometric distortion for each scanner at 5 different distances to isocentre: A) Mean geometric distortion per scanner (mean_{ps}) and B) Maximum geometric distortion per scanner (max_{ps}). Note: The red circles indicate values that are > 2 standard deviations from the mean over all scanners and hence are considered to be significantly worse/better.

3. Results

Mean_{ps} and max_{ps} for each distance from the isocentre are shown in Fig. 1. For scanner 4 these are based on a single measurement, due to a technical error resulting in loss of data from the second measurement. Table 2 shows the mean and standard deviation over all scanners (mean_{ps} and max_{ps}). Fig. 1 and table 2 shows that, as expected, the distortion increases when moving away from the isocentre. All of the mean_{ps} results were within the $\text{mean}_{\text{mean-as}} \pm 2\text{SD}_{\text{mean-as}}$ limit except those for scanners 2 and 9 (indicated by the circled points in Fig. 1). The greatest mean_{ps} geometric distortion was 5.0 mm on scanner 9, at ≥ 250 mm from the isocentre. In comparison with the other scanners, scanner 2 showed the worst performance at all distances except at ≥ 250 mm from the isocentre. This was considered significant for three measurements with geometric distortions of 0.6 mm at 100–150 mm, 1.3 mm at 150–200 mm, and mm 2.5 at 200–250 mm from isocentre. Scanner 10 showed the best performance in terms of geometric distortion at all distances, but this did not reach significance. δ^2 of the geometric distortion between scanners was found to increase with distance to isocentre as shown in table 2. The general trends for the maximum reported distortion are shown in Fig. 1 and Table 2 and match those of the mean, i.e. the maximum distortion increases with distance to isocentre. The only maximum distortion measurements to be considered significant outliers were for scanner 2 at 100–150 mm and 150–200 mm from isocentre which showed max_{ps} of 2.8 and 7.2 mm respectively.

Scatterplots of the geometric distortion measured for each marker as a function of distance to isocentre for all scanners are shown in appendix 2. The only notable difference between the two consecutive measurements is evident on scanner 3 which has two erroneous points on the second measurement, however these are both at distances of > 250 mm from the isocentre. Some key examples of scatterplots have been included in Fig. 2 for scanners 2, 6, and 10 which can be considered the worst, average and best-performing scanners respectively. In scanner 10, the dots are visibly less scattered at any given

Table 2

Mean and standard deviation of mean_{ps} and max_{ps} over all scanners ($\text{mean}_{\text{mean-as}}$, $\text{SD}_{\text{mean-as}}$, $\text{mean}_{\text{max-as}}$ and $\text{SD}_{\text{max-as}}$) as well as δ^2 between all scanners, at all distances to the isocentre.

Distance from the isocentre (mm)	< 100	100–150	150–200	200–250	≥ 250
$\text{mean}_{\text{mean-as}}$ (mm)	0.2	0.4	0.7	1.5	2.8
$\text{SD}_{\text{mean-as}}$ (mm)	0.1	0.1	0.2	0.5	0.9
$\text{mean}_{\text{max-as}}$ (mm)	0.6	1.2	3.0	6.1	9.6
$\text{SD}_{\text{max-as}}$ (mm)	0.2	0.6	1.7	2.9	3.9
δ^2 (mm ²)	< 0.01	0.01	0.05	0.23	0.78

distance to isocentre than they are for scanner 2.

4. Discussion

The aim of this work was to evaluate the feasibility of auditing geometric accuracy across a number of MRI scanners. Geometric distortion was evaluated in 11 clinical MRI scanners used for RT purposes using a GRADE phantom. This study found that geometric distortion increased with distance from the isocentre, as other studies have reported [21,26–28]. For RT purposes, it has been suggested in the literature that a geometric distortion of < 2 mm is required [13,29]. However, it is unclear whether the mean distortions or the maximum value is intended in these recommendations. This study cannot be considered as an audit study since it was not done under full audit conditions. However, it represents a first step that could serve as a basis for future audits and shows feasibility of such audits. If the results shown here were part of an audit then scanner 2 has been shown to be significantly worse in terms of geometric distortion. Therefore scanner 2 would require further investigation to assess the reason for this higher geometric distortion and if it could be reduced. In this case scanner 2 was a short, wide-bore MRI scanner so it is understandable that it has a higher main field inhomogeneity (and hence larger geometric distortion) compared to the other scanners.

For a future audit it is suggested that limits to warrant further investigation could be based on the mean distortion + 2 SD over a large number of MRI scanners. This should be done at different distances to isocentre with the distances chosen being relevant to the clinical applications of interest. Measurements should be based on mean distortions, rather than maximum distortions as maximum distortions can be effected by a single erroneous point. Geometric distortion of MRI scanners varies depending on the phantom and MRI sequence used and hence for an audit these parameters must be fixed. If a future audit used the GRADE phantom and the specific MRI sequence we have used then the limits of acceptability of such an audit could be based on $\text{mean}_{\text{mean-as}} + 2\text{SD}_{\text{mean-as}}$ for different distances to isocentre as shown in table 2.

Gustafsson et al. [17] used a GRADE phantom with a GE Discovery MR750w 3 T MR Scanner (General Electric Healthcare, Milwaukee, WI), and found mean and maximum distortions at all distances to isocentre similar to the mean values over all scanners that we have shown in Table 2.

This study did not compare differences in measured distortions that depended on whether 3D or 2D geometric distortion correction was used or not. However, Sun et al [30], reported a maximum distortion of 7.5 mm across the pelvis without the use of any correction algorithm, and that distortion decreased to 2.6 mm when 2D correction was used and to 1.7 mm when 3D correction was used. The bandwidth they used in this study was not clarified so a direct comparison between our

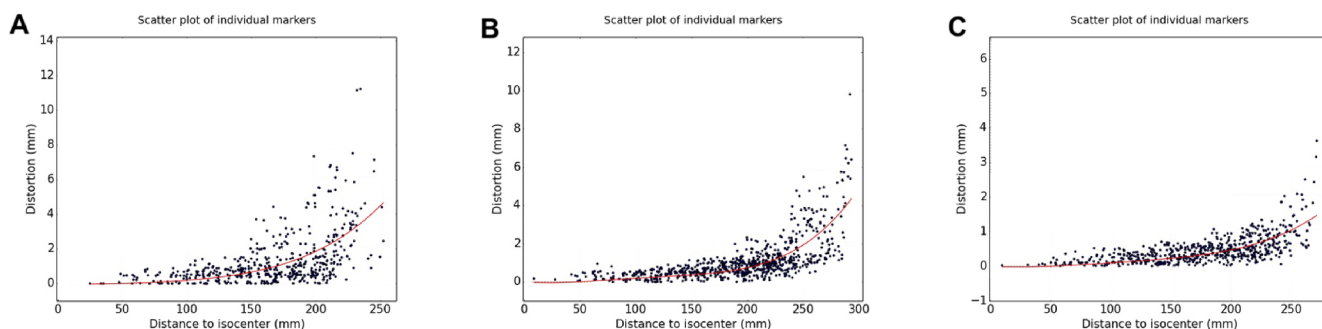


Fig. 2. Scatterplots for a single measurement from 3 different scanners. A) Scanner 2 which represent the worst scanner B) Scanner 6 which is an example of an average scanner C) Scanner 10 which represent the best scanner. Each scatterplot shows the distortion as a function of distance from the isocentre as measured for all markers as well as the trend line calculated using a second-degree polynomial using a least squares method.

results is not valid, however this work shows the importance of using 3D geometric distortion correction consistently during an audit.

The spherical markers in the GRADE phantom are filled with polyethylene glycol solution. For any water-based markers there might be some chemical shifts from doping agents. However, the bandwidth used was large enough to account for this. The present study did not take into account distortions that were patient/phantom induced. According to Gustafsson et al. [17], the magnetic susceptibility induced distortion of the GRADE phantom is < 0.5 mm for all radial distances of < 250 mm from the isocentre. This magnetic susceptibility induced distortion is small in comparison to the maximum distortions measured above 150 mm from the isocentre (above 2 mm) and hence can be ignored. However, in clinical use Walker et al. [14] registered CT images with MRI images obtained by a 3 T scanner and concluded that the maximum distortion was 3.8 times greater than that of the distortion obtained from the phantom. Therefore, although suitable for an audit to compare MRI scanners, reliance only on phantom results is not adequate to fully assess geometric distortions within a patient [31].

This study had some limitations. Firstly, because of a technical problem, only one measurement, rather than two, was used for scanner 4. Secondly, it was not possible to include all the MRI scanners used for RT purposes in England. However, the aim of this work was to demonstrate feasibility on 11 scanners of the methodology that could be used in a country wide audit in the future. A further limitation is that the results for geometric distortion presented are only valid within the phantom for the sequence investigated. The MRI sequence was provided by the manufacturer and was optimised for the phantom and not for a patient and hence the distortions displayed are not representative of the absolute distortions that would be observed in a patient. This limitation is acceptable as the aim of this work was to rigorously compare MRI scanners in clinical use for RT planning and show feasibility for a future audit.

In conclusion, the variance in distortion between scanners was found to be low and distortion was found to increase with distance from the isocentre. This study demonstrates feasibility of the technique to be repeated in a country wide audit of all MRI scanners used clinically for RT. It is recommended in such an audit that mean geometric distortions at clinically relevant distances to isocenter be used to assess MRI scanners. Acceptance limits could be based on the observed variability across multiple scanners.

Declaration of Competing Interest

The authors declare that they have no known competing financial interests or personal relationships that could have appeared to influence the work reported in this paper.

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Appendix A. Supplementary data

Supplementary data to this article can be found online at <https://doi.org/10.1016/j.phro.2020.07.004>.

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