

1 A local model for the limiting configuration of 2 interfacial solitary waves

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8 The limiting configuration of interfacial solitary waves between two homogeneous fluids
9 consisting of a sharp 120° angle with an enclosed bubble of stagnant heavier fluid on top
10 is investigated numerically. We use a boundary integral equation method to compute the
11 almost limiting profiles which are nearly self-intersecting and thus extend the work of Pullin
12 & Grimshaw (*Phys. Fluids* 31, 1988, 3550–3559) by obtaining the overhanging solutions for
13 very small density ratios. To further study the local configuration of the limiting profile, we
14 propose a reduced model that replaces the 120° angle with two straight solid walls intersecting
15 at the bottom of the bubble. Using a series truncation method, a one-parameter family of
16 solutions depending on the angle between the two solid walls (denoted by γ) is found. When
17 $\gamma = 2\pi/3$, it is shown that the simplified model agrees well with the near-limiting wave
18 profile if the density ratio is small, and thus provides a good local approximation to the
19 assumed limiting configuration. Interesting solutions for other values of γ are also explored.

20 1. Introduction

21 It was conjectured by Stokes that for two-dimensional deep surface gravity waves, there
22 exists a family of periodic travelling waves that terminates at an ‘extreme wave’ as it reaches
23 the maximum amplitude. Such limiting configuration, termed the Stokes highest wave, can
24 be characterised by a stagnation point at the crest and an enclosed angle of 120° . The
25 existence of the Stokes highest wave was extensively studied by a variety of authors from
26 asymptotic and numerical perspectives (Havelock 1918; Yamada 1957a; Longuet-Higgins
27 1973; Schwartz 1974; Vanden-Broeck & Schwartz 1979), and ultimately proved rigorously
28 by Amick *et al.* (1982). It was also pointed out by Amick *et al.* (1982) that the Stokes
29 conjecture holds regardless of wavelength and water depth, and in particular, in the limit
30 of infinite wavelength, the extreme solitary wave on water of finite depth features the same
31 limiting crest angle. Yamada (1957b) is the first known author to have solved for the
32 limiting solitary wave numerically (see the book by Okamoto & Shōji (2001) for a detailed
33 description of Yamada’s method). Lenau (1966) used a series truncation method to compute
34 the same wave. Hunter & Vanden-Broeck (1983) improved Lenau’s results.

35 For waves between two homogeneous fluids, the sharp crest of 120° cannot serve as
36 the limiting configuration of the interface since it would result in an infinite velocity in
37 the upper fluid (Meiron & Saffman 1983). Attempts to understand the limiting profile of
38 interfacial periodic waves were made by Saffman & Yuen (1982), Meiron & Saffman (1983)
39 and Turner & Vanden-Broeck (1986), who numerically discovered the overhanging structure
40 (i.e. multivalued wave profiles). Meiron & Saffman (1983) further asserted that the related

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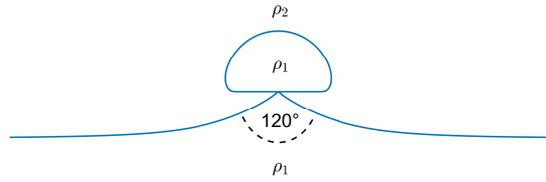


Figure 1: A possible limiting configuration for overhanging interfacial solitary waves: a sharp 120° angle with a closed fluid bubble on top of it.

41 limiting profile would become self-intersecting. Grimshaw & Pullin (1986) obtained the
 42 (almost) self-intersecting solutions when the upper fluid is of infinite depth. They conjectured
 43 that a possible extreme profile features a stagnant fluid bubble on top of a 120° angle. Recently,
 44 Maklakov & Sharipov (2018) conducted a thorough numerical study on the almost limiting
 45 configuration between semi-infinite fluid layers. They obtained highly accurate solutions,
 46 providing reliable evidence for the extreme profile predicted by Grimshaw & Pullin (1986).
 47 Maklakov (2020) discussed the transition from interfacial waves to surface waves when
 48 the density ratio tends to zero. For interfacial solitary waves, Amick & Turner (1986)
 49 proved that a possible extreme configuration is an internal front developed from flattening
 50 and unlimited broadening of the solitary pulse as the wave speed approaches a limiting
 51 value. This theoretical result was verified later by several numerical computations (see,
 52 e.g., Funakoshi & Oikawa 1986; Turner & Vanden-Broeck 1988; Rusås & Grue 2002).
 53 However, Amick & Turner (1986) also showed that the interface could develop a vertical
 54 tangent indicating the existence of multi-valued solutions, thus provided another possibility.
 55 Pullin & Grimshaw (1988) computed the interfacial solitary waves with an overhanging
 56 structure and suggested the existence of a self-intersecting profile. However, they could not
 57 obtain overhanging waves when the density ratio is smaller than 0.0256, which was explained
 58 by a rapid shrinking of the overhanging structure when the density ratio is small and is further
 59 decreased, and therefore more grid points are required to capture it.

60 In the current paper, we consider interfacial solitary waves between two fluids of finite
 61 depths. A boundary integral equation method is used to calculate overhanging solutions and
 62 the results of Pullin & Grimshaw (1988) are extended to very small density ratios. Based on
 63 numerical results and local analysis, we suggest a possible limiting configuration featuring
 64 a 120° angle-bubble structure, akin to the periodic case (see figure 1). A reduced model,
 65 which replaces the curved angle with two straight rigid walls intersecting at the bottom of the
 66 fluid bubble, is proposed and numerically solved using a series truncation method. It turns
 67 out that the simplified model provides a good local approximation for the cases of a small
 68 density ratio when the upper layer is deep enough. The reduced model can also be applied to
 69 periodic interfacial waves due to its local nature.

70 2. Mathematical formulation

71 We consider a two-dimensional solitary wave travelling at speed c between two incompress-
 72 ible and inviscid fluids, bounded above and below by horizontal solid walls. We take a frame
 73 of reference moving with the wave. The x -axis is parallel to the rigid walls. The level $y = 0$
 74 is chosen as the undisturbed level of the interface and gravity is assumed to act in the negative
 75 y -direction. We denote by h_i and ρ_i ($i = 1, 2$) the depth and density in each fluid layer, where
 76 subscripts 1 and 2 refer to fluid properties associated with the lower and upper fluid layers,
 77 respectively. Velocities are measured in units of c and lengths in units of h_1 . The motion

78 of each fluid is assumed to be irrotational, thus we introduce velocity potentials ϕ_1 and ϕ_2 ,
79 which satisfy the Laplace equation in the corresponding fluid layers

$$80 \quad \phi_{i,xx} + \phi_{i,yy} = 0, \quad i = 1, 2. \quad (2.1)$$

81 At the interface, the kinematic and dynamic boundary conditions can be expressed as

$$82 \quad \phi_{i,y} - \phi_{i,x}\eta_x = 0, \quad i = 1, 2, \quad (2.2)$$

$$83 \quad R|\nabla\phi_2|^2 - |\nabla\phi_1|^2 + \frac{2(R-1)}{F^2}\eta = R-1, \quad (2.3)$$

85 where $R = \rho_2/\rho_1 < 1$ for a density-stable configuration, $F = c/\sqrt{gh_1}$ is the Froude number,
86 and g is the acceleration due to gravity. The boundary conditions at the solid walls read

$$87 \quad \phi_{1,y} = 0, \quad \text{at } y = -1, \quad (2.4)$$

$$88 \quad \phi_{2,y} = 0, \quad \text{at } y = h, \quad (2.5)$$

89 where $h = h_2/h_1$ stands for the dimensionless depth of the upper layer. To describe a solitary
90 wave in the comoving frame we require $\eta \rightarrow 0$ and $\phi_{i,x} \rightarrow -1$ as $|x| \rightarrow \infty$ and, additionally,
91 we confine our attention to symmetric waves with the crest at $x = 0$.

92 3. Numerical results via a boundary integral method

93 Following Sha & Vanden-Broeck (1993), we reformulate the problem by using the Cauchy
94 integral formula

$$95 \quad \zeta(z_0) + 1 = \frac{1}{i\pi} \oint_C \frac{\zeta(z) + 1}{z - z_0} dz, \quad (3.1)$$

96 where $z = x + iy$ is the complex coordinate, $\zeta = \phi_x - i\phi_y = u - iv$ is the complex velocity,
97 and C stands for the boundary of the considered domain. We parameterise the interface by
98 the arc length $s \in (-\infty, \infty)$ and let $s = 0$ at $x = 0$. By applying the Cauchy integral formula
99 to the lower and upper fluid layers respectively and taking the real parts, one obtains

$$100 \quad \pi[u_1(\sigma) + 1]$$

$$101 \quad = \int_0^\infty \frac{[(u_1(s) + 1)x'(s) + v_1(s)\eta'(s)][2 + \eta(s) + \eta(\sigma)] - \eta'(s)[x(s) - x(\sigma)]}{[x(s) - x(\sigma)]^2 + [2 + \eta(s) + \eta(\sigma)]^2} ds$$

$$102 \quad + \int_0^\infty \frac{[(u_1(s) + 1)x'(s) + v_1(s)\eta'(s)][2 + \eta(s) + \eta(\sigma)] - \eta'(s)[x(s) + x(\sigma)]}{[x(s) + x(\sigma)]^2 + [2 + \eta(s) + \eta(\sigma)]^2} ds$$

$$103 \quad + \int_0^\infty \frac{[(u_1(s) + 1)x'(s) + v_1(s)\eta'(s)][\eta(s) - \eta(\sigma)] - \eta'(s)[x(s) - x(\sigma)]}{[x(s) - x(\sigma)]^2 + [\eta(s) - \eta(\sigma)]^2} ds$$

$$104 \quad + \int_0^\infty \frac{[(u_1(s) + 1)x'(s) + v_1(s)\eta'(s)][\eta(s) - \eta(\sigma)] - \eta'(s)[x(s) + x(\sigma)]}{[x(s) + x(\sigma)]^2 + [\eta(s) - \eta(\sigma)]^2} ds, \quad (3.2)$$

$$105 \quad \pi[u_2(\sigma) + 1]$$

$$106 \quad = \int_0^\infty \frac{[(u_2(s) + 1)x'(s) + v_2(s)\eta'(s)][2h - \eta(s) - \eta(\sigma)] + \eta'(s)[x(s) - x(\sigma)]}{[x(s) - x(\sigma)]^2 + [2h - \eta(s) - \eta(\sigma)]^2} ds$$

$$107 \quad + \int_0^\infty \frac{[(u_2(s) + 1)x'(s) + v_2(s)\eta'(s)][2h - \eta(s) - \eta(\sigma)] + \eta'(s)[x(s) + x(\sigma)]}{[x(s) + x(\sigma)]^2 + [2h - \eta(s) - \eta(\sigma)]^2} ds$$

$$108 \quad - \int_0^\infty \frac{[(u_2(s) + 1)x'(s) + v_2(s)\eta'(s)][\eta(s) - \eta(\sigma)] - \eta'(s)[x(s) - x(\sigma)]}{[x(s) - x(\sigma)]^2 + [\eta(s) - \eta(\sigma)]^2} ds$$

$$109 \quad - \int_0^\infty \frac{[(u_2(s) + 1)x'(s) + v_2(s)\eta'(s)][\eta(s) - \eta(\sigma)] - \eta'(s)[x(s) + x(\sigma)]}{[x(s) + x(\sigma)]^2 + [\eta(s) - \eta(\sigma)]^2} ds$$

$$110 \quad - \int_0^\infty \frac{[(u_2(s) + 1)x'(s) + v_2(s)\eta'(s)][\eta(s) - \eta(\sigma)] - \eta'(s)[x(s) + x(\sigma)]}{[x(s) + x(\sigma)]^2 + [\eta(s) - \eta(\sigma)]^2} ds, \quad (3.3)$$

111 where the Schwarz reflection principle and the symmetry of the interface with respect to the
 112 y -axis are used. For the computations, equations (3.2) and (3.3) are calculated over a finite
 113 interval $[0, L]$ with L large. Two sets of mesh grids

$$114 \quad \begin{aligned} s_i &= \frac{(i-1)L}{N-1}, \quad i = 1, 2, \dots, N, \\ \sigma_i &= \frac{s_i + s_{i+1}}{2}, \quad i = 1, 2, \dots, N-1, \end{aligned} \quad (3.4)$$

115 are introduced. Then $2N - 2$ algebraic equations can be obtained via evaluating the integrals
 116 at σ_i by the trapezoid rule. The boundary conditions at the interface, (2.2) and (2.3), as well
 117 as the arc length equation

$$118 \quad x'^2(s) + \eta'^2(s) = 1, \quad (3.5)$$

119 are evaluated at s_i , resulting in $4N$ algebraic equations. Since there are $6N + 1$ unknowns,
 120 namely $x'(s_i)$, $\eta'(s_i)$, $u_1(s_i)$, $v_1(s_i)$, $u_2(s_i)$, $v_2(s_i)$ and F (for a given wave height H), three
 121 additional equations are needed to close the system:

$$122 \quad u_1(L) = -1, \quad \eta'(0) = 0, \quad \text{and} \quad \eta(0) = H. \quad (3.6)$$

123 The unknowns at σ_i can be obtained by means of a four-point interpolation formula. For
 124 fixed values of R and h , we calculate solitary waves via Newton's method with an initial
 125 guess being a small-amplitude Gaussian profile. The iteration process is repeated until the
 126 maximum residual error is less than 10^{-8} . We slowly change the value of H (or F) and use the
 127 known solutions as the initial guess, thus solution branches can be systematically explored.

128 Numerical results indicate that unlimited broadening of the central core of solitary
 129 waves that ultimately turn into conjugate flows is likely to occur for small h (see
 130 Turner & Vanden-Broeck 1988). In order to obtain overhanging solutions, we choose large
 131 values for h ($h = 80$ say) in the subsequent computations. Three speed-amplitude bifurcation
 132 curves are shown in Figure 2(a) for the density ratios $R = 0.1, 0.2, 0.3$. Accordingly,
 133 the numerical calculations are performed with $L = 40, 50, 100$ and $N = 1200, 800,$
 134 500 . Some typical wave profiles are plotted in Figure 2(b,c,d). In general, it is found
 135 that along the bifurcation curve solitary waves gradually steepen, reach the maximum
 136 speed corresponding to the first turning point, and form a mushroom-shaped solitary pulse
 137 ultimately. It is observed that multiple turning points may exist on the same branch where
 138 the overhanging structure oscillates between closing and opening before it reaches the
 139 limiting configuration. The wave profile in the bottom figure of 2(c) is the closest to the
 140 proposed limiting configuration shown in Figure 1 among all the numerical solutions that
 141 we obtained. Our numerical results agree well with those found by Pullin & Grimshaw
 142 (1988) who conjectured that all solitary waves for small density ratios would develop an
 143 overhanging structure. Solitary waves with an overhanging structure can also be found for
 144 other values of R , and for instance, Figure 3 shows the numerical results obtained based
 145 on two sets of parameters: $(R, L, N) = (0.01, 8, 2000)$ and $(0.6, 200, 290)$. It is noted that
 146 solutions for $R = 0.01$ extend the result of Pullin & Grimshaw (1988) since they could not
 147 get overhanging profiles for $R < 0.0256$ due to numerical difficulties.

148 Based on the aforementioned numerical evidence, it is reasonable to conjecture that the
 149 limiting configuration is a self-intersecting interface consisting of a sharp angle and a closed
 150 fluid bubble as shown in Figure 1. To verify this assertion, we plot the velocity magnitude
 151 distributions (i.e. $u_{1,2}^2 + v_{1,2}^2$) at the interface in Figure 4(a) for $R = 0.15$ and $h = 80$. It is
 152 clear that there are two segments where velocities above or below the interface are almost

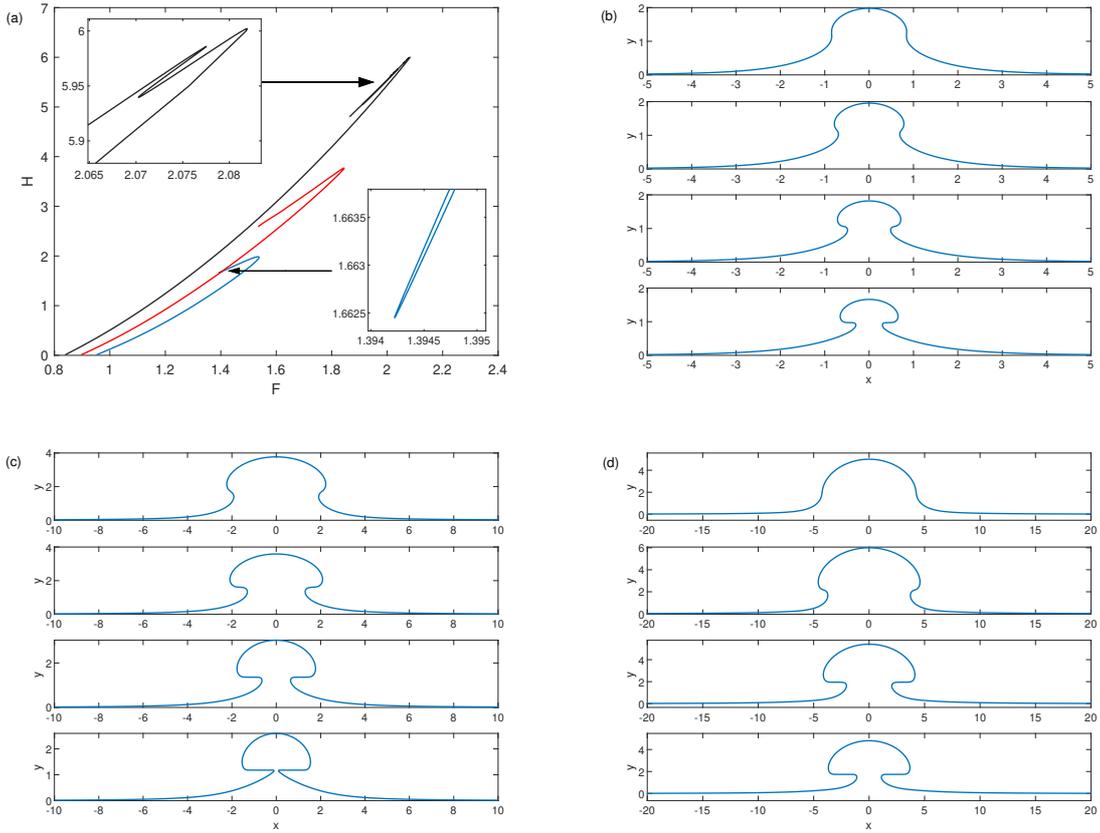


Figure 2: (a) Speed-amplitude bifurcation curves for $h = 80$ and $R = 0.1$ (blue), $R = 0.2$ (red), $R = 0.3$ (dark). (b-d) Typical overhanging profiles for $R = 0.1, 0.2, 0.3$ respectively.

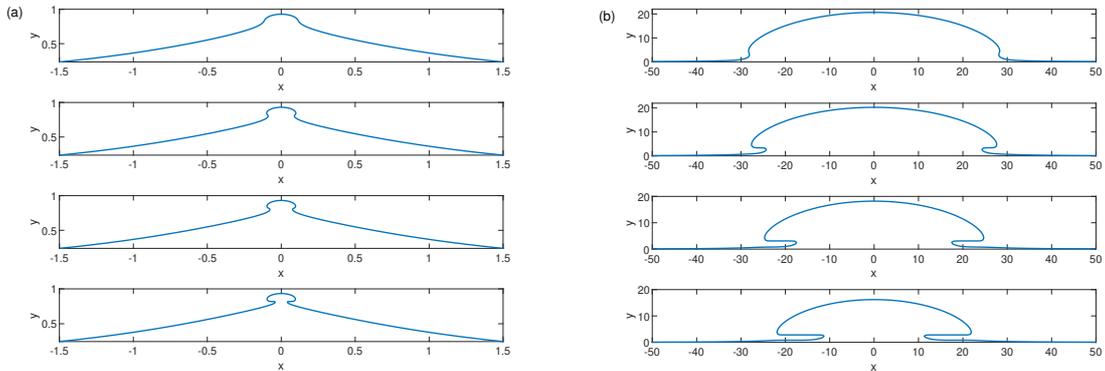


Figure 3: Overhanging waves for $h = 80$ and (a) $R = 0.01$, (b) $R = 0.6$.

153 zero. The common segment on which $u_{1,2}^2 + v_{1,2}^2 < 0.005$ is labeled by a thick black line
 154 in (a) and correspondingly highlighted on the wave profile in (b). Consequently, for the
 155 limiting configuration shown in Figure 1, if it exists, the fluid inside the bubble should be
 156 stationary since closed streamlines are not allowed for irrotational flows. Based on a similar
 157 argument of the Stokes highest wave, the sharp corner attached to the fluid bubble should
 158 be of an interior angle of 120° with the vertex being a stagnation point. On the other hand,
 159 Bernoulli's equation at the stagnation point implies $y_0 = F^2/2$ for all density ratios, where y_0

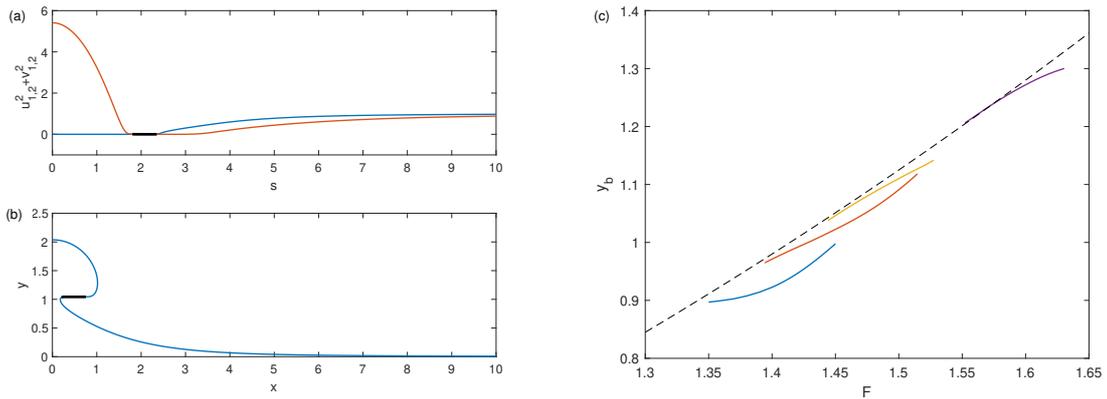


Figure 4: (a) Interfacial velocity magnitude of the upper fluid (red) and lower fluid (blue) for $R = 0.15$ and $h = 80$. The segment on which $u_{1,2}^2 + v_{1,2}^2 < 0.005$ is labeled by the black thick line. (b) Wave profile associated with (a), and the black part of the interface corresponds to $u_{1,2}^2 + v_{1,2}^2 < 0.005$. (c) Numerical relations between y_b and F for $R = 0.08$ (blue), $R = 0.1$ (red), $R = 0.15$ (yellow), and $R = 0.2$ (purple), together with the theoretical prediction $y_0 = F^2/2$ (dashed line). y_b denotes the vertical coordinate of the bubble bottom, and y_0 is the theoretical vertical coordinate of the stagnation point.

160 is the vertical coordinate of the vertex. The theoretical prediction $y_0 = F^2/2$ is plotted as the
 161 dashed line in Figure 4(c). Typical numerical values for $y_b(F)$ are shown in the same figure as
 162 solid lines, where y_b is the vertical coordinate of the flat bottom of the fluid bubble, namely
 163 the part labeled as black in Figure 4(b). The four curves correspond to $R = 0.08, 0.1, 0.15, 0.2$.

164 4. A simplified model

165 Although the almost self-intersecting solutions can be obtained by the boundary integral
 166 equation method, the appearance of the singularity, i.e. the 120° angle, is a formidable
 167 difficulty to overcome. As one can see from Figures 2 and 3, the overhanging structure is
 168 fully localised and shrinks rapidly when the value of R is decreased and, furthermore, the
 169 local structure beneath the bubble looks very much like an obtuse angle between two straight
 170 lines if the density ratio is small, e.g. $R = 0.01$. Motivated by these observations, we attempt
 171 to propose a simplified model to describe the local structure of the limiting configuration for
 172 small density ratios.

173 As shown in the simplified model of Figure 5, the end points A and C, which respectively
 174 represent upstream and downstream sides of a flow, are assumed to extend to infinity. The
 175 lines OA and OC are supposed to be solid walls where impermeability boundary conditions
 176 need to be satisfied. The angle γ is considered to be a parameter, and $\gamma = 2\pi/3$ is the relevant
 177 one to model interfacial waves. This is because the flow inside the angle μ approaches a
 178 stagnation flow as the point O is approached, where μ is the angle between the solid wall
 179 and the bubble bottom (see Figure 5). The flow of fluid 1 inside the angle γ near the point O
 180 reduces then to the local flow considered by Stokes to model surface waves. It then follows
 181 that $\gamma = 2\pi/3$. We note that the bottom part of the bubble near O is horizontal, so that
 182 $\mu = (\pi - \gamma)/2$. This can be justified by a local analysis of the flow inside the angle μ , a flow
 183 bounded above by a free surface and below by a solid wall. It can be shown that the free
 184 surface has to be horizontal at O (the only other possibility is the value $\mu = 2\pi/3$ which is
 185 not relevant here), and the interested reader is referred to the third chapter of Vanden-Broeck
 186 (2010) for details.

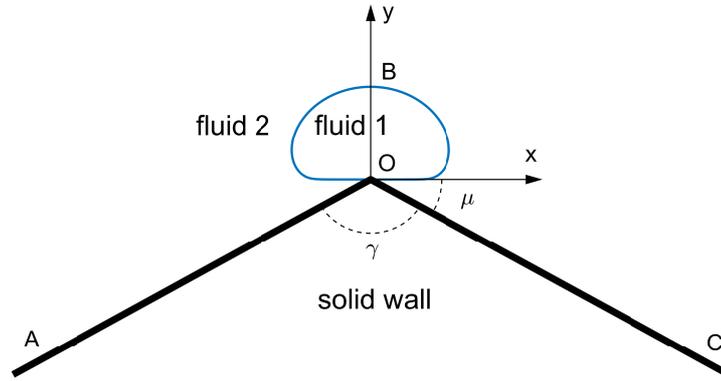


Figure 5: A simplified model: two straight solid walls intersect at the origin forming an angle γ and a closed fluid bubble with flat bottom is on top of the angle.

187 For the sake of convenience, the origin of the Cartesian coordinate system is set to coincide
 188 with the angle vertex O, with the y -axis pointing upward, and the summit of the bubble is
 189 label as B. Since the fluid inside the bubble is stationary, Bernoulli's equation now reads

$$190 \quad \frac{\rho_2}{2} (u_2^2 + v_2^2) + (\rho_2 - \rho_1)g\eta = 0. \quad (4.1)$$

191 Our aim is to find the shape of the fluid bubble as well as the velocity potential ϕ_2 . This is a
 192 single layer problem since the fluid status beneath the interface is either known or irrelevant.

193 To solve the problem, we introduce the complex velocity potential $f = \phi_2 + i\psi$, with
 194 ψ being the stream function. The value of ψ at the interface and along the solid walls as
 195 well as $\phi_2(B)$ are set to zero. It is noted the origin is actually the intersection of two walls,
 196 and hence we denote by O_- and O_+ the left- and right-hand limits when approaching O
 197 along the corresponding walls and let $\Phi = \phi_2(O_+) = -\phi_2(O_-)$ due to symmetry. We then
 198 non-dimensionalise the system by choosing $(\Phi^2/g)^{1/3}$ and $(\Phi g)^{1/3}$ as characteristic length
 199 and velocity scales, respectively. Following the work of Daboussy *et al.* (1998), we solve the
 200 problem by using the series truncation method. We introduce a transformation

$$201 \quad f = -\frac{1+t^2}{2t}, \quad (4.2)$$

202 which maps the upper half f -plane (i.e. the domain occupied by the lighter fluid) onto the
 203 upper half unit disk in the complex t -plane. The images of A, O_- , B, O_+ , C labelled in
 204 Figure 5 are $t = 0, 1, i, -1, 0$. The complex velocity $\zeta = u_2 - iv_2$ is analytic everywhere
 205 except at $t = 0$ and $t = \pm 1$, where the asymptotic behaviors are

$$206 \quad \zeta \sim t^{1-\frac{\gamma}{\pi}}, \quad \text{as } t \rightarrow 0, \quad (4.3)$$

$$208 \quad \zeta \sim (1-t^2)^{2-\frac{2\mu}{\pi}}, \quad \text{as } t \rightarrow \pm 1, \quad (4.4)$$

209 with $\mu = \frac{\pi-\gamma}{2}$. Therefore, the complex velocity ζ can be expressed as

$$210 \quad \zeta = e^{i\frac{\gamma-\pi}{2}} t^{1-\frac{\gamma}{\pi}} (1-t^2)^{2-\frac{2\mu}{\pi}} \xi, \quad (4.5)$$

211 where ξ is an unknown analytic function. We introduce two real functions τ and θ satisfying

212 $\xi = e^{\tau - i\theta}$ and expand $\tau - i\theta$ as

$$213 \quad \tau - i\theta = \sum_{n=0}^{\infty} a_n t^{2n} = \sum_{n=0}^{\infty} a_n \cos 2n\sigma - i \sum_{n=1}^{\infty} a_n \sin 2n\sigma, \quad (4.6)$$

214 where the coefficients a_n are real. At the interface, $t = e^{i\sigma}$ and $\sigma \in [0, \pi]$. Upon noting the
215 identity $x_\phi + iy_\phi = 1/\zeta$, it is easy to verify that

$$216 \quad y_\phi = e^{-\tau} (2 \sin \sigma)^{-2 + \frac{2\mu}{\pi}} \sin \left[\theta - \left(3 - \frac{\gamma}{\pi} - \frac{2\mu}{\pi} \right) \left(\sigma - \frac{\pi}{2} \right) \right], \quad (4.7)$$

$$217 \quad x_\phi = e^{-\tau} (2 \sin \sigma)^{-2 + \frac{2\mu}{\pi}} \cos \left[\theta - \left(3 - \frac{\gamma}{\pi} - \frac{2\mu}{\pi} \right) \left(\sigma - \frac{\pi}{2} \right) \right]. \quad (4.8)$$

218 Thus Bernoulli's equation becomes

$$219 \quad \frac{R}{2} e^{2\tau} (2 \sin \sigma)^{4 - \frac{4\mu}{\pi}} + (R - 1) \int_0^\sigma y_\phi \sin \alpha d\alpha = 0. \quad (4.9)$$

220 To solve equation (4.9), the infinite series in (4.6) are truncated at $n = N - 1$ and N collocation
221 points are uniformly distributed on the interval $[0, \frac{\pi}{2}]$, namely

$$222 \quad \sigma_i = \frac{\pi(i - 1)}{2(N - 1)}, \quad i = 1, 2, \dots, N. \quad (4.10)$$

223 Equation (4.9) is then satisfied at the mesh points $\sigma_2, \sigma_3, \dots, \sigma_N$ with an additional equation

$$224 \quad \int_0^{\frac{\pi}{2}} x_\phi \sin \sigma d\sigma = 0, \quad (4.11)$$

225 which simply means the interface is closed. Finally, this system of N nonlinear equations
226 with N unknowns (a_0, a_1, \dots, a_{N-1}) is solved via Newton's method for a given value of
227 γ , and $N \geq 300$ in all computations. This method of series truncation has been applied
228 successfully to solve many free surface problems (see Vanden-Broeck (2010) for details and
229 references).

230
231 *Case I. $\gamma = 2\pi/3$*

232
233 Numerical results for $\gamma = 2\pi/3$ (i.e. $\mu = \pi/6$) are shown in Figure 6. A typical profile and
234 corresponding streamlines are plotted in (a) for $R = 0.1$. From Bernoulli's equation

$$235 \quad R(u_2 u_{2\sigma} + v_2 v_{2\sigma}) + (R - 1) \sin \sigma \frac{v_2}{u_2^2 + v_2^2} = 0, \quad (4.12)$$

236 which is derived from equation (4.1) by taking the derivative with respect to σ , one can
237 eliminate R by introducing

$$238 \quad u_2' = \sqrt[3]{R/(1 - R)} u_2, \quad v_2' = \sqrt[3]{R/(1 - R)} v_2. \quad (4.13)$$

239 This fact immediately suggests that profiles for different values of R are geometrically similar,
240 which is reasonable since no natural length scale appears in the reduced model. To verify
241 this assertion, numerical solutions are plotted in Figure 6(b) where the profiles from large to
242 small correspond to $R = 0.9, 0.8, 0.6, 0.3, 0.1$ respectively.

243 Figure 7 shows comparisons between solutions of the simplified model and the almost
244 self-intersecting solutions obtained from the boundary integral equation method. The black
245 line represents the assumed 120° angle. To plot these solutions under the same scaling, we
246 enlarge the profiles of the simplified model and then move the profiles vertically so that

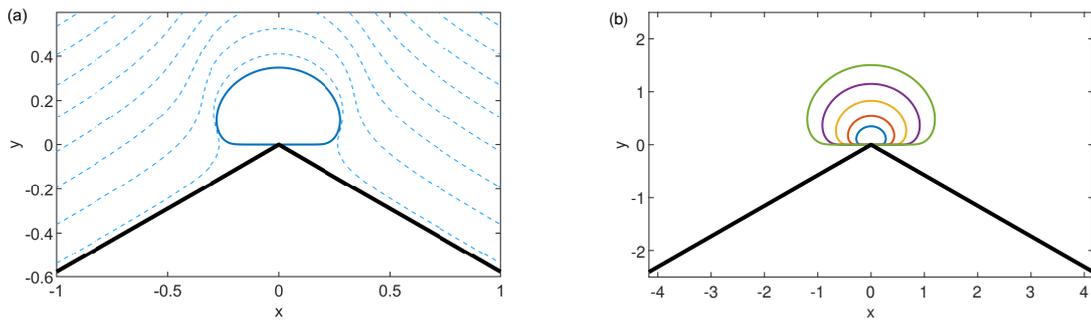


Figure 6: (a) Numerical solution of the simplified model for $\gamma = 2\pi/3$ and $\mu = \pi/6$ (solid curve), together with streamlines (dashed curves). (b) Similarity solutions for $R = 0.9, 0.8, 0.6, 0.3, 0.1$ from large to small.

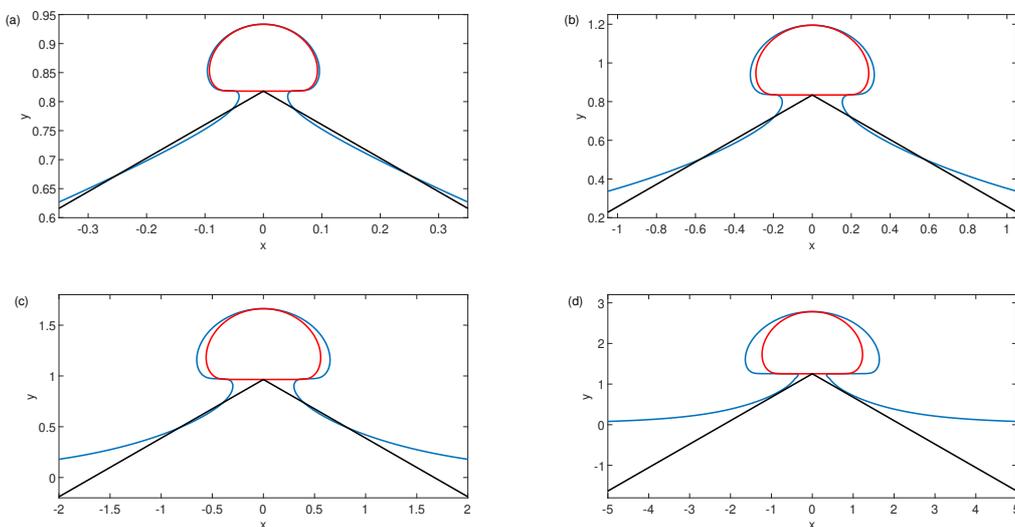


Figure 7: Comparisons between the almost self-intersecting solutions (blue curves) and profiles resulting from the simplified model (red curves). The black lines represent solid walls intersecting at a 120° angle. (a) $R = 0.01$, (b) $R = 0.05$, (c) $R = 0.1$, (d) $R = 0.2$.

247 their top and bottom match the highest point and flat bottom of the bubble structure of the
 248 primitive problem. The density ratios from (a) to (d) are 0.01, 0.05, 0.1, 0.2 respectively. It is
 249 observed that for a small density ratio, the simplified model provides a good approximation
 250 to the almost self-intersecting solution of the primitive equations and further to the limiting
 251 configuration shown in Figure 1, if it exists.

252

253 *Case II. $\gamma \neq 2\pi/3$*

254

255 It is natural to ask what happens to the reduced model when $\gamma \neq \frac{2\pi}{3}$. In fact, numerical
 256 solutions can be found for arbitrary $\gamma \in [0, \pi]$. Four typical solutions with $R = 0.1$ are shown
 257 in Figure 8.

258 Two limiting cases, $\gamma = 0$ and $\gamma = \pi$, merit special attention. As can be seen from Figure
 259 8, the profile becomes more and more circular as the value of γ is decreased. Therefore, one
 260 may expect a perfect circular interface to appear when $\gamma = 0$. In fact, it is not difficult to check
 261 that $\zeta = it(1 - t^2)a_0$ is an explicit solution of equation (4.12), where $a_0 = \sqrt[3]{(1 - R)/4R}$.

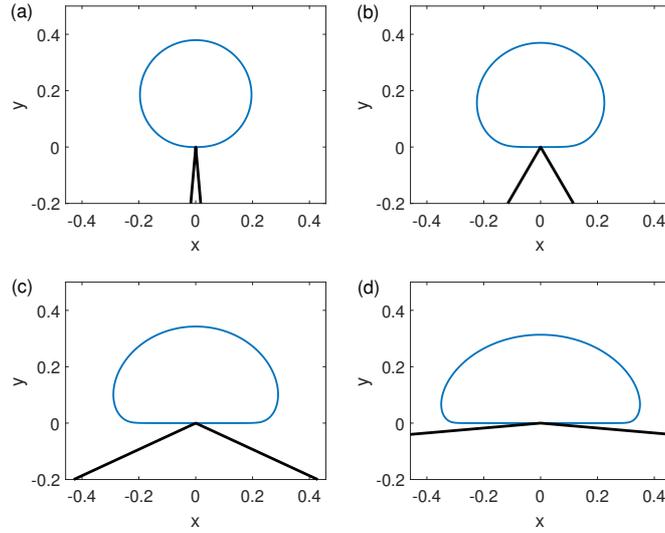


Figure 8: Solutions of the simplified model for (a) $\gamma = \frac{\pi}{18}$, (b) $\gamma = \frac{\pi}{3}$, (c) $\gamma = \frac{13\pi}{18}$, (d) $\gamma = \frac{17\pi}{18}$.

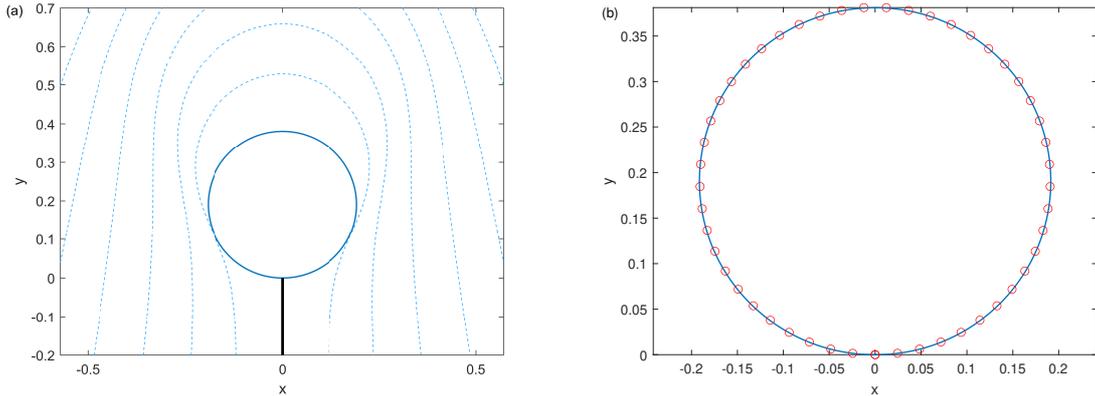


Figure 9: (a) Numerical solution for $\gamma = 0$ and $\mu = \frac{\pi}{2}$ (solid curve) and streamlines (dashed curves). (b) Comparison between the numerical solution (solid curve) and theoretical prediction (red circles).

262 One can then obtain the parametric form of the interface as

$$263 \quad x = -\frac{1}{4a_0} \sin 2\sigma, \quad y = -\frac{1}{4a_0} (\cos 2\sigma - 1), \quad (4.14)$$

264 which is a circle with radius $\frac{1}{4a_0}$. The numerical solution for $R = 0.1$ is plotted in figure 9,
 265 where the profile and streamlines are displayed in (a) while the comparison with the exact
 266 solution is in (b). It thus demonstrates the validity of the numerical algorithm.

267 For the case of $\gamma = \pi$, the bottom of the fluid bubble entirely attaches to the solid wall,
 268 therefore the interface should intersect the solid wall with a 120° angle and form a stagnation
 269 point according to the local analysis. A typical solution for $R = 0.1$ is shown in Figure 10 by
 270 setting $\mu = \frac{2\pi}{3}$ and dropping equation (4.11) since the profile is no longer closed at the origin.
 271 This type of solution, which describes a still water bubble lying on the flat bottom, exists for
 272 all $R \in (0, 1)$ due to the geometrical similarity (4.13). Unlike those shown in Figure 6 that
 273 represent the limiting solutions for $R \ll 1$, the profile shown in Figure 10 corresponds to

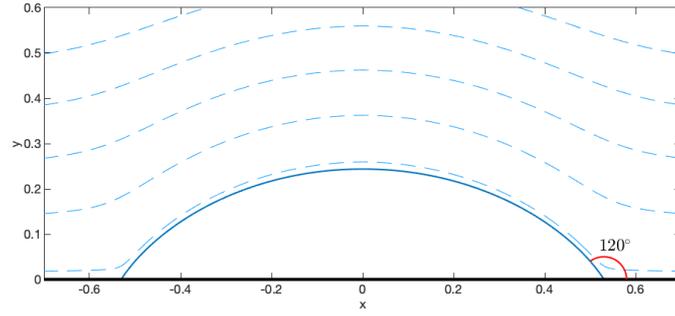


Figure 10: Numerical solution for $\gamma = \pi$ and $\mu = \frac{2\pi}{3}$ (solid curve), together with streamlines (dashed curves).

274 another possible limiting configuration of interfacial solitary waves, which appears under the
 275 Boussinesq limit, i.e. $R \rightarrow 1$. Such solutions were found by Pullin & Grimshaw (1988) when
 276 the upper fluid is infinitely deep. They proposed that in such a scenario solitary waves are
 277 unbounded and calculated the limiting configuration by fixing the wave height and gradually
 278 decreasing the lower layer thickness to zero. In particular, they concluded that the limiting
 279 interface features a half-lens shape with an approximate aspect ratio (i.e. the ratio of width
 280 to height) of 4.36, which perfectly agrees with 4.353 resulting from our simplified model.

281 5. Concluding Remarks

282 In conclusion, we have found numerical evidence for a possible limiting configuration of
 283 interfacial solitary waves. Overhanging solutions which become almost self-intersecting
 284 have been calculated via a boundary integral equation method for various density ratios,
 285 strongly suggesting a limiting configuration characterised by a stagnation point at a 120°
 286 angle and a closed fluid bubble on top of the angle (see Figure 1). A simplified model based
 287 on these numerical results has been proposed to study the local structure of these singular
 288 solutions. Using a series truncation method, we have found exotic solutions depending
 289 on the value of γ , i.e. the angle formed by two intersecting walls. When $\gamma = 2\pi/3$, the
 290 simplified model provides a good approximation to those almost self-intersecting solutions
 291 for small density ratios. Solutions for other values of γ have also been computed. In particular,
 292 we have found an explicit solution featuring a circular profile for $\gamma = 0$, and a solution
 293 corresponding to another limiting configuration of interfacial solitary waves for $\gamma = \pi$.
 294 Furthermore, it is important to mention that the reduced model can also be applied to periodic
 295 interfacial waves due to its local nature. Finally, considering the crest instability of the Stokes
 296 highest waves (see detailed numerical investigations by Longuet-Higgins & Tanaka 1997),
 297 the Kelvin-Helmholtz instability of interfacial gravity waves (Benjamin & Bridges 1997),
 298 and the Rayleigh-Taylor instability due to the mushroom structure, it is very likely that the
 299 almost limiting configurations of progressive interfacial waves are unstable. Therefore, the
 300 competition mechanism among different instabilities and the time-evolution of the instability
 301 are of particular interest which merit further thorough studies. The only paper we know that
 302 provides stability results for interfacial solitary waves is the paper of Kataoka (2006). For
 303 small amplitude solitary waves, linear stability analyses based on the Korteweg-de Vries
 304 (KdV) equation and its modified version (mKdV equation) show that these waves are stable.
 305 Using an asymptotic analysis, Kataoka (2006) constructed a general criterion for the stability
 306 of interfacial solitary waves with respect to disturbances that are stationary relative to the
 307 basic wave. Interesting results were obtained for small density ratios. In particular, Table 1 of
 308 Kataoka (2006) provides critical wave amplitudes H at which an exchange of stability first

309 occurs for air–water solitary waves ($R = 0.0013$) with various depth ratios h . According to
 310 this table, all the waves considered in the present paper are unstable. However, the mechanism
 311 of the instability is of great interest, since it is related to the theory of wave breaking. As said
 312 above, it was suggested that the instability of solitary waves is caused by the crest instability.
 313 Assuming that the local crest instability is also the correct mechanism of interfacial solitary
 314 wave instability, there is still one important question. Kataoka (2006) found that the exchange
 315 of stability occurs at the extremum in the total wave energy. What is the physical connection
 316 between the crest instability, which is a local phenomenon, and the extremum in the total
 317 wave energy, which is a global quantity? On an apparently completely different problem
 318 related to super free fall, Villiermaux & Pomeau (2010) commented on the formation of
 319 a concentrated ‘nipple’ on top of an essentially flat base solution and wondered about the
 320 relevance with wave breaking. They noted that wave breaking does occur with standing
 321 waves (Taylor 1953) and in nature. The formation of ‘nipples’ can easily be observed on
 322 wave crests. These nipples then bend and splash on the sea surface, forming foam and spume.
 323 Is the present study definitely irrelevant to that common but yet unexplained phenomenon?
 324 We believe that some interesting dynamics due to the instability of interfacial solitary waves
 325 at small density ratios is likely to occur.

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332 Declaration of Interests

333 The authors report no conflict of interest.

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