

1 **Melting phase relations in the systems Mg<sub>2</sub>SiO<sub>4</sub>-H<sub>2</sub>O and MgSiO<sub>3</sub>-H<sub>2</sub>O and the**  
2 **formation of hydrous melts in the upper mantle**

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24 **Abstract**

25 High-pressure and high-temperature melting experiments were conducted in the systems  
26  $\text{Mg}_2\text{SiO}_4\text{-H}_2\text{O}$  and  $\text{MgSiO}_3\text{-H}_2\text{O}$  at 6 and 13 GPa and between 1150 to 1900 °C in order  
27 to investigate the effect of  $\text{H}_2\text{O}$  on melting relations of forsterite and enstatite. The  
28 liquidus curves in both binary systems were constrained and the experimental results  
29 were interpreted using a thermodynamic model based on the homogeneous melt  
30 speciation equilibrium,  $\text{H}_2\text{O} + \text{O}^{2-} = 2 \text{OH}^-$ , where water in the melt is present as both  
31 molecular  $\text{H}_2\text{O}$  and  $\text{OH}^-$  groups bonded to silicate polyhedra. The liquidus depression as a  
32 function of melt  $\text{H}_2\text{O}$  concentration is predicted using a cryoscopic equation with the  
33 experimental data being reproduced by adjusting the water speciation equilibrium  
34 constant. Application of this model reveals that in hydrous  $\text{MgSiO}_3$  melts at 6 and 13 GPa  
35 and in hydrous  $\text{Mg}_2\text{SiO}_4$  melts at 6 GPa, water mainly dissociates into  $\text{OH}^-$  groups in the  
36 melt structure. A temperature dependent equilibrium constant is necessary to reproduce  
37 the data, however, implying that molecular  $\text{H}_2\text{O}$  becomes more important in the melt with  
38 decreasing temperature. The data for hydrous forsterite melting at 13 GPa are  
39 inconclusive due to uncertainties in the anhydrous melting temperature at these  
40 conditions. When applied to results on natural peridotite melt systems at similar  
41 conditions, the same model infers the presence mainly of molecular  $\text{H}_2\text{O}$ , implying a  
42 significant difference in physiochemical behavior between simple and complex hydrous  
43 melt systems. As pressures increase along a typical adiabat towards the base of the upper  
44 mantle, both simple and complex melting results imply that a hydrous melt fraction  
45 would decrease, given a fixed mantle  $\text{H}_2\text{O}$  content. Consequently, the effect of pressure

46 on the depression of melting due to H<sub>2</sub>O could not cause an increase in the proportion,  
47 and hence seismic visibility, of melts towards the base of the upper mantle.

48

49 **Keywords:** olivine, enstatite, phase equilibria, hydrous melting, cryoscopic equation,  
50 water speciation.

51

## 52 **1. Introduction**

53 The effect of H<sub>2</sub>O on the formation of silicate melts underlies a number of igneous  
54 processes taking place within the Earth's mantle. H<sub>2</sub>O has an important influence on the  
55 generation of magmas at subduction zones being both a metasomatic agent of the arc  
56 magma source region and responsible for the high degrees of melting that produce these  
57 magmas (e.g. Tatsumi et al., 1986). The lithospheric mantle shows abundant evidence for  
58 metasomatism by H<sub>2</sub>O-bearing melts (e.g. Menzies and Hawkesworth, 1987; Erlank et al.  
59 1987) and several exotic magma types such as kimberlites and lamproites are likely  
60 formed, at least in part, as a result of H<sub>2</sub>O lowering the mantle solidus (e.g. Kushiro et al.,  
61 1968; Kawamoto and Holloway, 1997; Sokol et al., 2013). H<sub>2</sub>O induced melting of the  
62 deep mantle has also been proposed to explain a number of geophysical observations  
63 such as the Earth's seismic low velocity zone (Lambert and Wyllie, 1970; Mierdel et al.,  
64 2007) and possible low velocity layers present on top of the transition zone (Tauzin et al.,  
65 2010) and immediately below it (Schmandt et al., 2014). Recently, it was proposed that  
66 H<sub>2</sub>O-induced melts would tend to migrate in the lower mantle, and transfer H<sub>2</sub>O from  
67 ultramafic to mafic lithologies, as a result of the difference in H<sub>2</sub>O storage capacities of  
68 these rock types (Pamato et al., 2015).

69

70 In order to understand the production of hydrous melts in the Earth's mantle it is  
71 important to constrain how H<sub>2</sub>O affects the melting behaviour of mantle materials. In this  
72 regard, a number of studies have been performed to quantify the effects of H<sub>2</sub>O on  
73 lowering melting temperatures and increasing melt yields in natural mantle rock systems  
74 (Mysen and Boettcher, 1975; Hirose and Kawamoto, 1995; Gaetani and Grove, 1998;  
75 Balta et al., 2011; Tenner et al., 2012b; Novella et al., 2014). Determining the effect of  
76 H<sub>2</sub>O on melting in natural chemical systems is challenging, however, due to the large  
77 number of chemical components that are potentially influenced by H<sub>2</sub>O. These  
78 determinations are further complicated by a number of other instrumental factors, such as  
79 control of oxygen fugacity, attainment of equilibrium, H<sub>2</sub>O and FeO loss from  
80 experimental capsules and the difficulty in determining the H<sub>2</sub>O contents of melts  
81 (Brooker et al., 1998; Liu et al., 2006; Tenner et al., 2012b; Novella and Frost, 2014).

82

83 It has long been appreciated that the effects of H<sub>2</sub>O on silicate melts can be more easily  
84 quantified by examining melting behavior in simple systems (Kushiro et al, 1968;  
85 Kushiro and Yoder, 1969; Kushiro, 1972; Hodges, 1973, 1974). From results of  
86 experiments in simple systems such as Mg<sub>2</sub>SiO<sub>4</sub>-SiO<sub>2</sub>-H<sub>2</sub>O, Kushiro (1972) proposed, for  
87 example, that hydrous mantle partial melts would be more SiO<sub>2</sub>-rich compared to dry  
88 melts. Studies in simple systems can also be used to quantify the effect of H<sub>2</sub>O on mineral  
89 melting at high pressures and experiments have been performed up to conditions  
90 equivalent to those in the mantle transition zone (Kushiro and Yoder, 1969; Luth, 1993;  
91 Inoue, 1994). While relatively detailed melting phase relations on hydrous forsterite

92 (Kushiro and Yoder, 1969; Hodges 1973) and enstatite (Kushiro and Yoder, 1969;  
93 Kushiro et al., 1968) exist up to 3 GPa, phase relations at higher pressures are more  
94 sparse and show less mutual agreement. Luth (1993) and Inoue (1994) investigated the  
95 melting behavior of forsterite with 17-20 wt% H<sub>2</sub>O up to pressures of 12 and 15.5 GPa,  
96 respectively, although the two studies are in poor agreement. In addition, Inoue (1994)  
97 also studied the phase relations of hydrous enstatite and an intermediate Mg/Si ratio  
98 composition to similar pressures. However, in this previous study more emphasis was  
99 placed on determining the conditions of the hydrous solidus rather than quantifying the  
100 effect of melt H<sub>2</sub>O content on the melting temperature.

101

102 Recently, several studies on natural multicomponent systems have proposed generalized  
103 models for the effects of H<sub>2</sub>O on peridotite melting temperatures (Medard and Grove,  
104 2008; Tenner et al., 2012a). While such models are quite successful in reproducing the  
105 experimental observations, they make assumptions concerning both the thermodynamic  
106 data and the mechanism by which H<sub>2</sub>O dissolves in melts that can be more easily tested  
107 using results on simplified systems. In simplified systems additional constraints are also  
108 provided by calorimetric measurements such as those performed to determine the entropy  
109 of melting (Bottinga, 1985; Navrotsky et al., 1989; Richet et al., 1993; Tangeman et al.,  
110 2001). One advantage of examining experiments in simple systems is that treatment with  
111 relatively simple thermodynamic models should provide a firmer basis for understanding  
112 hydrous melting on a physicochemical level (Burnham, 1975; Silver and Stolper, 1985)  
113 and can be used to examine how the effect of H<sub>2</sub>O on melting may be further modified by  
114 pressure.

115

116 The goal of this study is to determine the melting phase relations in the systems  
117  $\text{Mg}_2\text{SiO}_4\text{-H}_2\text{O}$  and  $\text{MgSiO}_3\text{-H}_2\text{O}$  at upper mantle conditions. In particular, we investigate  
118 the  $\text{H}_2\text{O}$  contents of melts in equilibrium with forsterite and/or enstatite as a function of  
119 temperature at high pressure by bracketing the location of the hydrous liquidus curves.  
120 The experimental data are analysed using thermodynamic models to provide insight into  
121 the  $\text{H}_2\text{O}$  dissolution mechanism and its effects at high pressures. Results are presented for  
122 both systems at 6 and 13 GPa corresponding to  $\sim 180$  and  $\sim 390$  km depth in the mantle,  
123 and temperatures ranging between 1150 to 1900 °C.

124

## 125 **2. Experimental and analytical details**

126 Two sets of compositions were prepared for experiments in the systems  $\text{Mg}_2\text{SiO}_4\text{-H}_2\text{O}$   
127 and  $\text{MgSiO}_3\text{-H}_2\text{O}$ . In the system  $\text{Mg}_2\text{SiO}_4\text{-H}_2\text{O}$ , starting compositions were mixed from  
128 two end-member compositions:  $\text{Mg}_2\text{SiO}_4$  (forsterite) synthesized from high purity oxides,  
129  $\text{MgO}$  and  $\text{SiO}_2$ , and a 2:1 molar mixture of  $\text{Mg}(\text{OH})_2$  (brucite) and  $\text{SiO}_2$ . The pure  
130 forsterite was synthesized by firing the oxides at 1500 °C for 2 hours and then grinding  
131 the sintered mix for 1 hour under ethanol. This firing and grinding process was repeated 4  
132 times. The 2:1 brucite-silica mixture corresponds to a composition of  $\text{Mg}_2\text{SiO}_4$  with 20.4  
133 wt%  $\text{H}_2\text{O}$  in the bulk. In order to prepare this end member, brucite and  $\text{SiO}_2$  were dried  
134 overnight at 120 °C and 1000 °C, respectively. The calculated amount of each component  
135 was then weighed, ground for 1 hour under ethanol and dried under an infrared lamp. By  
136 varying the mass proportions of the end member compositions a range of mixtures were  
137 prepared with variable  $\text{H}_2\text{O}$  content but with a constant stoichiometry of  $\text{Mg}/\text{Si} = 2$  (Table

138 1). All mixtures with water contents less than 20.4 wt% were prepared by grinding the  
139 weighed proportions of dry forsterite and forsterite with 20.4 wt% bulk H<sub>2</sub>O for 30  
140 minutes under ethanol, and then drying. Before each mixture was prepared the forsterite  
141 end-member was dried at 1000 °C for one hour and the water-bearing forsterite end-  
142 member was dried overnight at 120 °C. This approach was also followed for the  
143 preparation of starting mixtures in the system MgSiO<sub>3</sub>-H<sub>2</sub>O. In this case, an end-member  
144 1:1 molar mixture of brucite and SiO<sub>2</sub>, corresponding to a composition of MgSiO<sub>3</sub> with  
145 15.2 wt% bulk H<sub>2</sub>O, was initially prepared (Table 1). The dry end-member MgSiO<sub>3</sub> was  
146 prepared from high purity oxides MgO and SiO<sub>2</sub> and the dry and hydrous end-members  
147 were mixed in different mass proportions to obtain the compositions given in Table 1.  
148 Once prepared, all final mixtures were stored in a furnace at 120 °C to limit the  
149 adsorption of water.

150

151 Platinum or platinum/rhodium multi-chamber capsules were fabricated from 2 mm  
152 diameter Pt or Pt/Rh (Pt<sub>90</sub>Rh<sub>10</sub>) rods cut into 1 mm long sections. The resulting discs were  
153 spark eroded on one surface, obtaining rows of 4 to 6 chambers per disc with the  
154 chambers being 0.25 mm in diameter and approximately 0.66 mm deep. Each chamber  
155 was loaded with a different starting powder such that H<sub>2</sub>O contents increased across the  
156 row of chambers. Sample powders were packed into each chamber using a tungsten-  
157 rhenium needle. When packed sufficiently the chambers remained full even when air was  
158 blown over the surface. Blowing air removed extraneous sample powders from chambers  
159 that had not yet been loaded. The Pt capsules were closed by placing a second Pt disc  
160 0.25 mm thick on top of the chambers, which was held closed under pressure. When

161 Pt/Rh capsules were employed the open extremities of the chambers were closed by  
162 placing on top 6 foils of Pt/Rh with total thickness of ~0.25 mm.

163

164 High pressure and high temperature experiments were carried out using a multianvil  
165 apparatus installed at the Bayerisches Geoinstitut (BGI). The experiments were  
166 performed in an 18/11 assembly, with an 18 mm edge length Cr<sub>2</sub>O<sub>3</sub>-doped MgO  
167 octahedral pressure medium and 11 mm WC-anvil corner truncations. Experiments at 6  
168 GPa were performed using a 500 tonne Walker-type multi anvil press and a 5000 tonne  
169 Kawai-type multianvil press. The experiments at 13 GPa were carried out only with the  
170 5000 tonne multianvil apparatus. The pressure calibration at 6 GPa was performed using  
171 the CaGeO<sub>3</sub> garnet to perovskite phase transition (Ross et al, 1986) for the 500 tonne  
172 multianvil apparatus, while the pressure calibration described by Frost et al. (2004) was  
173 employed for the experiments performed with the 5000 tonne press. A stepped graphite  
174 heater was used in the experiments at 6 GPa, while for those performed at 13 GPa a  
175 stepped LaCrO<sub>3</sub> heater was employed. Temperatures during the experiments were  
176 monitored using a W<sub>97</sub>Re<sub>3</sub>–W<sub>75</sub>Re<sub>25</sub> (D type) thermocouple inserted within an alumina  
177 sleeve. The thermocouple junction was in contact with the base of the spark eroded  
178 capsules, ~0.5 mm from the sample chambers, with an estimated temperature uncertainty  
179 of 50 °C (Frost et al., 2004). However, higher uncertainty (100 °C) is considered for  
180 experiments where the thermocouple reading failed and temperature was determined  
181 based on power-temperature calibrations. A 25 µm thick foil of rhenium was placed on  
182 the top of the capsule in order to avoid direct contact between the capsule and the  
183 thermocouple junction. The maximum temperature fluctuation during the experiments



184 was  $\pm 5$  °C. The capsule was surrounded by MgO spacers and sleeves. Each experiment  
185 was first pressurised over 4 hours then heated in ~15 minutes to target temperature where  
186 it remained for up to 30 minutes depending on target temperature. Once completed, the  
187 experiment was quenched by turning off the power supply to the graphite/LaCrO<sub>3</sub> heater,  
188 and decompression was carried out over approximately 15 hours.

189

190 After each experiment, the Pt or Pt/Rh sample disk was recovered, mounted in epoxy and  
191 polished in the absence of water. Due to the high porosity of the charges, impregnation  
192 with either epoxy resin or superglue was often required in order to avoid loss of material  
193 during the polishing. Once the samples were polished, phase identification and chemical  
194 analyses were carried out using a JEOL-JXA-8200 electron microprobe (EMPA) at the  
195 BGI. Conditions of 15 kV and 15 nA for the accelerating voltage and beam current,  
196 respectively, were adopted in all the analyses, using a beam diameter of ~1  $\mu\text{m}$ . Standards  
197 for SiO<sub>2</sub> and MgO were forsterite and enstatite, respectively, and all the analyses were  
198 processed following the ZAF corrections.

199

200 Raman spectroscopy was conducted on some of the experimental charges to confirm the  
201 nature of the mineral phases produced. The analyses were performed using a LABRAM  
202 Raman spectrometer installed at the BGI and operating with a He-Ne laser with 632 nm  
203 red-line wavelength. Analyses were performed with a total of 3 spectrum collections and  
204 an accumulation time of 15 seconds each.

205

206 **3. Results**

207 Sections of typical experimental runs are shown in Fig. 1. At both pressures of 6 and 13  
208 GPa melts quenched to produce a fine intergrowth of crystals. However, crystals that  
209 were solid phases during heating of the experiments were easily distinguished from the  
210 quenched crystals based on their euhedral character and grain size. In some experiments  
211 quenched areas with different grain sizes and crystallite shapes could be observed that  
212 might be interpreted as separate coexisting liquids, or vapour (Fig. 1a). Given that the  
213 H<sub>2</sub>O contents of the charges are relatively low for fluid-saturated conditions to be  
214 encountered (e.g. Mibe et al., 2002), it seems more likely that these differences in texture  
215 result from local differences in nucleation and growth during quenching of the  
216 experiments. All quench textures are consistent with an origin as H<sub>2</sub>O-bearing melts  
217 rather than aqueous fluids. This distinction is made based on the quench crystal density  
218 compared to previous studies performed at lower temperatures where a sub-solidus  
219 aqueous fluid phase was encountered (Mibe et al. 2002).

220

221 Sections were ground by hand to over half way through the sample chambers to verify  
222 the absence of crystals in experiments interpreted to have encountered superliquidus  
223 conditions. Continual checks were made during grinding to examine for crystals that  
224 might not otherwise appear in the final section. Some samples were ground more than  
225 80% through to ensure that no crystals were present in the charge. The small size of the  
226 sample chambers should ensure that thermal gradients across the samples are minimal.  
227 The large relative size of the metal capsule should also help to relax thermal gradients.  
228 Based on measurements performed in similar assemblies using two pyroxene

229 thermometry (Brey et al., 1990), the thermal gradients within each chamber are estimated  
230 to be  $<20$  °C.

231

232 Several experiments were performed at the same conditions but with different heating  
233 durations in order to assess H<sub>2</sub>O loss from the Pt capsules during the experiments. Two  
234 experiments loaded with the same starting mixtures were performed at 6 GPa and 1400  
235 °C for 5 and 30 minutes, respectively, and in both cases the resulting assemblages in each  
236 of the sample chambers were identical. At 13 GPa the same result was obtained in two  
237 experiments performed at 1450 °C. These observations imply that significant loss of H<sub>2</sub>O  
238 does not occur in experiments with run durations up to 30 minutes at temperatures up to  
239 1450 °C. However, it was observed that in some experiments performed at higher  
240 temperatures ( $>1650$  °C), run durations greater than 30 minutes led to substantial  
241 crystallisation, likely due to H<sub>2</sub>O loss from the Pt capsule. Therefore, experiments  
242 performed above 1650 °C were held at target temperature for 5-20 minutes only.

243

### 244 **3.1 Experimental results at 6 GPa**

245 Experimental conditions and phase assemblages of the runs performed at 6 GPa for both  
246 Mg<sub>2</sub>SiO<sub>4</sub>-H<sub>2</sub>O and MgSiO<sub>3</sub>-H<sub>2</sub>O systems are summarized in Table 2. In the forsterite-  
247 H<sub>2</sub>O system, experiments were performed from 1250 to 1650 °C (Fig. 2). In some runs  
248 performed at 1250 °C crystals of enstatite were also observed, possibly suggesting  
249 incongruent melting at these conditions. However, this observation is not in agreement  
250 with the experimental results of Inoue (1994), which indicate the transition from  
251 congruent to incongruent melting of forsterite in the system Mg<sub>2</sub>SiO<sub>4</sub>-H<sub>2</sub>O to occur

252 between 7.7 and 12 GPa. Rather than incongruent melting, the appearance of enstatite is  
253 possibly due to slight variations of certain starting mixtures from the Fo-H<sub>2</sub>O join, which  
254 would be more visible at high degrees of crystallization. Our data suggest that the  
255 invariant curve Fo + En = Liquid is passing very close to the fo-H<sub>2</sub>O line and possibly  
256 crossing it (Fig. 3), explaining the observed phase relations (Table 2). In experiments  
257 conducted at temperatures above 1250 °C, the run products contained either forsterite and  
258 melt or melt only, implying congruent melting. The run with the highest H<sub>2</sub>O content  
259 (20.4 wt%) produced crystals in equilibrium with quenched melt at 1250 °C, hence it had  
260 not yet reached the liquidus temperature (Table 2). However, at temperatures higher than  
261 1250 °C, most experiments had one or more chambers that contained a supraliquidus  
262 product that comprised only quenched melt. At 1400 °C, for example, forsterite crystals  
263 coexisting with melt were produced in charges with H<sub>2</sub>O contents of 7.9, 9.7, 13.8 wt%,  
264 but the run with 18.3 wt% H<sub>2</sub>O contained only hydrous melt (Fig. 1b, Table 2). The  
265 proportion of crystals in each of these runs decreases in agreement with the lever rule as  
266 the crystal-melt region is crossed as a function of H<sub>2</sub>O content in the system. No  
267 interpretation of these proportions is made, however, as it may be inaccurate due to the  
268 particular sample section obtained during polishing.

269

270 In the MgSiO<sub>3</sub>-H<sub>2</sub>O system, experiments were carried out from 1050 °C to 1650 °C, with  
271 starting mixtures containing up to 15.2 wt% H<sub>2</sub>O (Table 2, Fig. 4). All run products  
272 contained enstatite and melt or melt only, indicating that melting occurred congruently  
273 over the entire temperature range. In one experiment (V704, Table 2) a tiny crystal of  
274 forsterite was found as an inclusion in a large enstatite crystal, but this was most likely a

275 consequence of chemical inhomogeneity in the starting mixture. The enstatite liquidus is  
276 bracketed at 1650 °C at ~10 wt% H<sub>2</sub>O and at 1500 °C at ~15 wt% H<sub>2</sub>O.

277

### 278 **3.2 Experimental results at 13 GPa**

279 Experimental conditions and phase assemblages observed at 13 GPa for both systems  
280 Mg<sub>2</sub>SiO<sub>4</sub>-H<sub>2</sub>O and MgSiO<sub>3</sub>-H<sub>2</sub>O are summarized in Table 3. Experiments were  
281 performed between 1300 and 1900 °C. In the Mg<sub>2</sub>SiO<sub>4</sub>-H<sub>2</sub>O system, forsterite was found  
282 to melt incongruently to an assemblage containing enstatite, forsterite and hydrous melt  
283 at temperatures below 1600 °C (Fig. 5). However, the congruent forsterite liquidus could  
284 be bracketed at 1700 °C between 13.8 and 20.4 wt% H<sub>2</sub>O and at 1900 °C between 5 and  
285 13.8 wt % H<sub>2</sub>O (Table 3). At 1300 °C, for example, the formation of forsterite in  
286 equilibrium with melt was observed at the highest bulk water contents (20.4 wt%), while  
287 enstatite was also crystallized at lower bulk H<sub>2</sub>O contents. This is possibly due to the fact  
288 that the univariant Fo + En = Liquid curve has moved closer to the Fo-H<sub>2</sub>O join and small  
289 variations within the bulk composition causes enstatite to crystallize (Fig. 3). At 1500 °C,  
290 the Mg<sub>2</sub>SiO<sub>4</sub> plus 5 wt% H<sub>2</sub>O starting mixture produced forsterite and melt along with  
291 minute crystals of MgO (estimated to be <1 vol%). The lower temperature of this  
292 experiment compared to others where MgO was not observed implies that the MgO  
293 crystals most likely formed due to a slight inhomogeneity in the starting mixture, rather  
294 than an incongruent melting reaction. As we do not observe the presence of MgO in any  
295 other of the experiments it is likely that the Fo + Per = Liquid univariant curve crosses  
296 the Fo-H<sub>2</sub>O join at lower H<sub>2</sub>O contents than studied (Fig 3), which can be then roughly  
297 constrained using the study of Presnall and Walter (1993).

298

299 In the system  $\text{MgSiO}_3\text{-H}_2\text{O}$ , enstatite melted congruently at 1900 °C and the liquidus  
300 curve was bracketed at this temperature between 4.3 and 10 wt%  $\text{H}_2\text{O}$  (Fig. 6). However,  
301 in some of the experiments performed between 1300 and 1700 °C, the formation of small  
302 crystals of stishovite occurred along with enstatite and melt, in agreement with  
303 observations of Yamada et al. (2004) at 13.5 GPa. The presence of stishovite may be due  
304 to the fact that En + St + L univariant curve has moved near to the En- $\text{H}_2\text{O}$  join, or even  
305 crossed it (Fig. 3). This phase, however, was observed only as a minor component, ~2  
306 vol%, and is, therefore, not expected to cause significant departures from the determined  
307 phase relations. Additionally, the enstatite liquidus curve was bracketed at 1700 °C  
308 between 6.2 and 11.8 wt%  $\text{H}_2\text{O}$ . At 1600 °C, the most  $\text{H}_2\text{O}$ -rich charge (15.2 wt%  $\text{H}_2\text{O}$ )  
309 produced an assemblage of enstatite plus melt, which constrains the minimum  $\text{H}_2\text{O}$   
310 concentration of the liquidus melt at this temperature.

311

## 312 **4. Discussion**

313

### 314 **4.1 Model for hydrous melting of $\text{Mg}_2\text{SiO}_4$ and $\text{MgSiO}_3$**

315 A number of studies have examined the melting point depression of silicate minerals as a  
316 function of  $\text{H}_2\text{O}$  content in the melt using the cryoscopic equation (e.g. Silver and Stolper  
317 1985; Medard and Grove, 2008; Hirschmann et al., 2009; Myhill et al., 2016). For  
318  $\text{Mg}_2\text{SiO}_4$  at the liquidus, for example,

319

$$320 \quad \ln a_{\text{Mg}_2\text{SiO}_4}^{\text{melt}} = \frac{-\Delta_m G^\circ}{RT} \quad (1)$$

321

322 where  $\Delta_m G^\circ$  is the standard state Gibbs free energy of melting of pure forsterite (see  
323 Appendix) and  $a_{\text{Mg}_2\text{SiO}_4}^{\text{melt}}$  is the activity of the  $\text{Mg}_2\text{SiO}_4$  component in the binary  $\text{Mg}_2\text{SiO}_4$ -  
324  $\text{H}_2\text{O}$  melt. At temperatures below the pure forsterite melting point,  $\Delta_m G^\circ$  can be  
325 determined by integrating the entropy of melting of pure  $\text{Mg}_2\text{SiO}_4$ ,  $\Delta_m S^\circ$ , between the  
326 temperature of interest,  $T$ , and the anhydrous melting point,  $T_m$ . Assuming that  $\Delta_m S^\circ$  is  
327 constant with temperature, Eq. (1) becomes:

328

$$329 \quad \ln a_{\text{Mg}_2\text{SiO}_4}^{\text{melt}} = \frac{\Delta_m S^\circ (T - T_m)}{RT}. \quad (2)$$

330

331 The standard entropies of melting for  $\text{Mg}_2\text{SiO}_4$  and  $\text{MgSiO}_3$  solid phases have been  
332 derived from calorimetric measurements at 1 bar (e.g. Navrotsky et al. 1989; Richet et al.,  
333 1993) and expressions for  $\Delta_m S^\circ$  at higher pressures can be determined from data on the  
334 anhydrous melting curves combined with equations of state for solid and liquid  $\text{Mg}_2\text{SiO}_4$   
335 or  $\text{MgSiO}_3$  (see Appendix).

336

337 Use of the cryoscopic equation requires a plausible relationship between the activity and  
338 concentration of silicate species in the hydrous melt, which will depend on the  $\text{H}_2\text{O}$   
339 concentration in the melt and its dissolution mechanism. Empirical molecular mixing of  
340  $\text{Mg}_2\text{SiO}_4$  or  $\text{MgSiO}_3$  and  $\text{H}_2\text{O}$  does not produce a sufficient depression of the liquidus to  
341 explain the experimental data and it has long been recognized that upon dissolution in  
342 silicate melts  $\text{H}_2\text{O}$  dissociates into hydroxyl groups bonded to the silicate framework

343 (Burnham 1975, 1979, 1994; Stolper, 1982; Silver and Stolper, 1989; Zotov and Keppler,  
344 1998), i.e.

345



347

348 Spectroscopic analyses indicate that both molecular H<sub>2</sub>O and OH<sup>-</sup> groups are present in  
349 silicate melts (e.g. Stolper, 1982, Dixon and Stolper, 1995), and their properties are  
350 temperature-dependent (Nowak and Behrens, 1995; Zotov and Keppler, 1998). Silver and  
351 Stolper (1985) proposed a thermodynamic model to describe the effects of H<sub>2</sub>O  
352 speciation on the activity of silicate melt components. They assumed that all three species  
353 (H<sub>2</sub>O, O<sup>2-</sup> and OH<sup>-</sup>) mix ideally following a homogeneous melt equilibrium (Eq. 3). The  
354 activity of the silicate component,  $a_{\text{Mg}_2\text{SiO}_4}^{\text{melt}}$ , is related to the mole fraction of non-protonated  
355 oxygen atoms in the melt,  $X_{\text{O}^{2-}}^{\text{melt}}$ , through the expression

356

$$357 \quad a_{\text{Mg}_2\text{SiO}_4}^{\text{melt}} = (X_{\text{O}^{2-}}^{\text{melt}})^r \quad (4)$$

358

359 where  $r$  is the number of oxygen atoms available for protonation and mixing per formula  
360 unit of silicate, with the chosen formula unit being consistent with the value of  $\Delta_m S^\circ$ .  
361 Setting  $r=4$  for Mg<sub>2</sub>SiO<sub>4</sub> or 3 for MgSiO<sub>3</sub> implies that H can bond to any of the oxygen  
362 atoms in the silicate melt structure.

363

364 The extent of H<sub>2</sub>O dissociation in the silicate melt (Eq. 3) is described by the equilibrium  
365 constant  $K$ ,



366

367 
$$K = \frac{(X_{\text{OH}^-}^{\text{melt}})^2}{X_{\text{H}_2\text{O}}^{\text{melt}} X_{\text{O}^{2-}}^{\text{melt}}} \quad (5)$$

368

369 Following mass balance,

370

371 
$$X_{\text{H}_2\text{O}^{\text{tot}}}^{\text{melt}} = X_{\text{H}_2\text{O}}^{\text{melt}} + 0.5X_{\text{OH}^-}^{\text{melt}} \quad (6)$$

372

373 where  $X_{\text{H}_2\text{O}^{\text{tot}}}^{\text{melt}}$  is the total mole fraction of H<sub>2</sub>O in the silicate-H<sub>2</sub>O melt. Solving Eqs. (5)

374 and (6) simultaneously, subject to the closure constraint

375

376 
$$X_{\text{H}_2\text{O}}^{\text{melt}} + X_{\text{OH}^-}^{\text{melt}} + X_{\text{O}^{2-}}^{\text{melt}} = 1 \quad (7)$$

377

378 yields mole fractions of all three species in the hydrous melt. Substituting Eq. (5) and (6)

379 into Eq. (7) yields

380

381 
$$X_{\text{H}_2\text{O}^{\text{tot}}}^{\text{melt}} = 1 - X_{\text{O}^{2-}}^{\text{melt}} + \frac{KX_{\text{O}^{2-}}^{\text{melt}} - \sqrt{(KX_{\text{O}^{2-}}^{\text{melt}})^2 + 4KX_{\text{O}^{2-}}^{\text{melt}} - 4K(X_{\text{O}^{2-}}^{\text{melt}})^2}}{4} \quad (8)$$

382

383 which is evaluated for the fraction of non-protonated oxygen atoms in the melt. The

384 corresponding activity of the silicate melt component is calculated from Eq. (4) and the

385 liquidus temperature is then defined by Eq. (2). In order to compare the results of the

386 model with experimental data,  $X_{\text{H}_2\text{O}^{\text{tot}}}^{\text{melt}}$  can be converted to  $w_{\text{H}_2\text{O}^{\text{tot}}}^{\text{melt}}$ , the mass fraction of  
 387 H<sub>2</sub>O dissolved in the melt using,

388

$$389 \quad w_{\text{H}_2\text{O}^{\text{tot}}}^{\text{melt}} = \frac{X_{\text{H}_2\text{O}^{\text{tot}}}^{\text{melt}} M_{\text{H}_2\text{O}}}{X_{\text{H}_2\text{O}^{\text{tot}}}^{\text{melt}} M_{\text{H}_2\text{O}} + \left(1 - X_{\text{H}_2\text{O}^{\text{tot}}}^{\text{melt}}\right) \frac{M_{\text{sil}}}{r}} \quad (9)$$

390

391 where  $M_{\text{H}_2\text{O}}$  is the molar mass of water (18.015 g/mol) and  $M_{\text{sil}}$  is the molar mass of the  
 392 silicate formula unit.

393

#### 394 **4.1.1 Liquidus depression at 6 GPa**

395 Fig. 2 shows the experimental results for the forsterite liquidus as a function of melt H<sub>2</sub>O  
 396 content at 6 GPa compared to liquidus calculations using several limiting cases of the  
 397 thermodynamic model. The thermodynamic data used to determine the anhydrous  
 398 melting point of Mg<sub>2</sub>SiO<sub>4</sub> and  $\Delta_m S^\circ$  at the pressure and temperature of interest are listed  
 399 in Table A (see Appendix and Supplementary Material).

400

401 Three different curves for the Mg<sub>2</sub>SiO<sub>4</sub> liquidus are shown calculated for different values  
 402 of the dissociation equilibrium constant,  $K$ . If all H<sub>2</sub>O is completely dissociated to OH<sup>-</sup> ( $K$   
 403 =  $\infty$ ), the experimental data at the lowest temperatures are in poor agreement with the  
 404 model as the experimental liquidus becomes less depressed at high H<sub>2</sub>O contents. On the  
 405 other hand, if all H<sub>2</sub>O is dissolved in the molecular form ( $K = 0$ ), the predicted liquidus  
 406 curve is not in agreement with experimental data at any H<sub>2</sub>O concentration. The change  
 407 in slope of the experimental liquidus implies that  $K$  is not constant over the range of

408 experimental temperatures, but must change from a high or infinite value (>50) above  
409 1400 °C to <10 below 1300 °C, i.e. molecular H<sub>2</sub>O becomes more important as the H<sub>2</sub>O  
410 saturated solidus is approached. Variations in  $K$  with temperature can be described using  
411 the function,

$$413 \quad \ln K = \frac{a}{T} + b, \quad (10)$$

414  
415 which mimics the enthalpic and entropic contributions to  $K$ . The experimental data do not  
416 provide sufficient constraints to determine the  $a$  and  $b$  coefficients in Eq. (10) uniquely  
417 due to their high correlation. Values of  $a \sim -7000$  K and  $b \sim 5.6$  are in reasonable  
418 agreement, however, with the data and their uncertainties. A different set,  $a = -8000$  K  
419 and  $b = 8$ , recently proposed for alkaline basalt by Lesne et al. (2011) based on  
420 spectroscopic measurements would also just fit the experimental uncertainties, but start to  
421 diverge at temperatures below 1300 °C. The experimental data can only be used to imply  
422 a qualitative, strong dependence of  $K$  on temperature. Independent *in-situ* spectroscopic  
423 data would be required to provide a more accurate estimate of this dependence.

424  
425 Although the model is relatively simple, improvements that would provide a significantly  
426 better fit to the experimental data are relatively limited, without making the model  
427 completely empirical. For example, a slightly better agreement between the liquidus  
428 curve and the experimental data at ~1450 °C can only be achieved by decreasing the  
429 standard entropy of forsterite melting at 1 bar, which is already near the lower limit  
430 derived from calorimetric studies (see Appendix). Non-ideal mixing can be included in

431 the model, however, a simple symmetric mixing parameter between the  $\text{Mg}_2\text{SiO}_4$  and  
 432  $\text{H}_2\text{O}$  components produces no significant improvement of the fit. In addition, such terms  
 433 have been shown to be unnecessary to describe the effect of  $\text{H}_2\text{O}$  on melting at lower  
 434 temperatures, where non-ideal effects should be even more important (Silver and Stolper,  
 435 1985).

436

437 We further compare our experimental results with the model of Tenner et al. (2012a),  
 438 which is based on the limiting case where all  $\text{H}_2\text{O}$  dissolves as  $\text{OH}^-$ . In Fig. 2, the liquidus  
 439 is calculated according to this model using the same thermodynamic data as above and  
 440 assuming  $r = 4$  (random protonation of all oxygen atoms), which is analogous to using a  
 441 single-oxygen formula unit for the silicate end-member (Tenner et al. 2012a; their Eqs. 9  
 442 and 11). The predicted liquidus is substantially different from that obtained from the  
 443 Silver and Solper (1985) model with  $K = \infty$ , although both models should be equivalent  
 444 in describing the liquidus depression when  $\text{H}_2\text{O}$  dissolves completely as  $\text{OH}^-$ . The  
 445 difference arises in the conversion relationships for the mass fraction of  $\text{H}_2\text{O}$  by Silver  
 446 and Stolper (1985) and Tenner et al. (2012a). To bring these two models to numerical  
 447 consistency, the following relationship would have to be used to calculate the mole  
 448 fraction of  $\text{OH}^-$  in the melt from the  $\text{H}_2\text{O}$  mass fraction,

449

$$450 \quad X_{\text{OH}^-}^{\text{melt}} = 2 \frac{w_{\text{H}_2\text{O}^{\text{tot}}}^{\text{melt}} / M_{\text{H}_2\text{O}}}{w_{\text{H}_2\text{O}^{\text{tot}}}^{\text{melt}} / M_{\text{H}_2\text{O}} + (100 - w_{\text{H}_2\text{O}^{\text{tot}}}^{\text{melt}}) / M_{\text{sil}}}, \quad (11)$$

451

452 rather than the conversion equation proposed by Tenner et al. (2012a). The model of  
453 Tenner et al. (2012a) has been found to quite accurately reproduce the liquidus of  
454 experiments performed in natural complex systems when silicates are mixed on a 3-  
455 oxygen formula basis. However, the model does not reproduce data on  $\text{Mg}_2\text{SiO}_4$  at 6  
456 GPa, regardless of the silicate molecular unit considered, providing an independent  
457 confirmation that  $\text{H}_2\text{O}$  upon dissolution in silicate melt incompletely dissociates to  $\text{OH}^-$ .

458

459 A further complexity in the model would be to consider the possibility that not all of the  
460 oxygen atoms in the melt structure are available for protonation but, for example,  $r = 1$  or  
461 2 per 4-oxygen formula unit (silicate polyhedron) due to local avoidance or ordering  
462 principles. This consideration raises two issues, however. First, it would imply a  
463 maximum limit for  $\text{H}_2\text{O}$  solubility in the melt, which appears to be not the case. Second,  
464 if the number of oxygen sites, which are accessible for proton bonding became an  
465 adjustable parameter and were allowed to change, for example, with the  $\text{H}_2\text{O}$   
466 concentration, the resulting fit parameters would be highly correlated with  $K$ . These  
467 parameters cannot be meaningfully constrained without an independent estimate of  $K$ .  
468 Therefore, the Silver and Stolper (1985) model with temperature-dependent speciation in  
469 the melt supported by current estimates for  $\Delta_m S^\circ$  of forsterite and the pressure-  
470 temperature melting curve of anhydrous forsterite appears to provide an adequate and  
471 well-constrained approximation of the experimental data.

472

473 In Fig. 4 experimental results bracketing the  $\text{MgSiO}_3\text{-H}_2\text{O}$  liquidus at 6 GPa are  
474 compared with the same set of models as described above. The model that considers

475 complete dissociation to  $\text{OH}^-$  ( $K = \infty$ ) agrees with experimental data at the highest  
476 temperatures investigated (above 1600 °C). At lower temperatures, the experimental data  
477 again imply a shallower liquidus slope that is not consistent with the complete  
478 dissociation of  $\text{H}_2\text{O}$  into  $\text{OH}^-$ . On the other hand, mixing with molecular  $\text{H}_2\text{O}$  only ( $K =$   
479  $0$ ) results in a liquidus curve far outside of the experimental uncertainties. A model that  
480 considers variation of  $K$  with temperature (Eq. 10) fulfils the constraints imposed by the  
481 experiments, although a large range of parameters in this equation can provide an  
482 adequate fit to the data. The curve in Fig. 4 was calculated with values of  $a = -6000$  K  
483 and  $b = 4.5$  with  $K$  decreasing from  $\sim 7$  at 2100 °C to  $\sim 2$  at 1300 °C. In addition, two  
484 models from Tenner et al. (2012a) that assume mixing of silicate molecules with 1- and  
485 3-oxygen formula units, respectively, are shown in Fig. 4. The model of Tenner et al.  
486 (2012a) based on 1-oxygen per formula unit predicts values within the experimental  
487 uncertainties. However, these authors find the best agreement with melting data using  
488 natural peridotite composition when a 3-oxygen silicate molecule is assumed but, as  
489 shown in Fig. 4, this is in poor agreement with the data in this simple  $\text{MgSiO}_3\text{-H}_2\text{O}$   
490 subsystem.

491

492 Both enstatite and forsterite melting experiments at 6 GPa can be described by Silver and  
493 Stolper (1985) models that assume mixing of H on all silicate oxygen atoms and a  
494 temperature-dependent dissociation of  $\text{H}_2\text{O}$ , which proceeds towards complete  $\text{OH}^-$   
495 formation above  $\sim 1400$  °C. It is interesting to note that the mass fraction (wt %) of  $\text{H}_2\text{O}$   
496 in the liquidus melt at a given temperature is nearly identical at 6 GPa for both  $\text{MgSiO}_3$   
497 and  $\text{Mg}_2\text{SiO}_4$  over the entire temperature range.

498

#### 499 **4.1.2 Liquidus depression at 13 GPa**

500 In Fig. 5 experiments bracketing the  $\text{Mg}_2\text{SiO}_4\text{-H}_2\text{O}$  liquidus at 13 GPa are shown and  
501 compared to the same models as described for the results at 6 GPa. The melting of pure  
502  $\text{Mg}_2\text{SiO}_4$  becomes incongruent above 10 GPa, with  $\text{Mg}_2\text{SiO}_4$  reacting to produce  $\text{MgO}$   
503 and melt at the solidus (Presnall and Walter, 1993). Upon the addition of  $\text{H}_2\text{O}$  to the  
504 system, melting becomes congruent between 1700-1900 °C (Table 3). For the purpose of  
505 modelling the forsterite liquidus, thermodynamic data for congruent  $\text{Mg}_2\text{SiO}_4$  melting at  
506 lower pressures have been extrapolated using the melt model of de Koker and Stixrude  
507 (2009) to 13 GPa. Models using complete dissociation into  $\text{OH}^-$  by Silver and Stolper  
508 (1985) with  $K = \infty$  and by Tenner et al. (2012a) do not reproduce the experimental data  
509 (Fig. 5). The best agreement with the experimental liquidus is found for the limiting case  
510 of no dissociation, that is, mixing of molecular  $\text{H}_2\text{O}$  ( $K = 0$  or 0.2). There are, however,  
511 larger inherent uncertainties in performing this evaluation at 13 GPa arising from the  
512 melting temperature assumed for anhydrous  $\text{Mg}_2\text{SiO}_4$ . Although the thermodynamic  
513 model of de Koker and Stixrude (2009) used here provides some theoretical justification  
514 for the extrapolation, the resulting dramatic change predicted in the  $\text{H}_2\text{O}$  speciation most  
515 probably arises from resulting inaccuracies in the temperature of metastable forsterite  
516 melting. By assuming an anhydrous melting temperature that is 250 °C higher than  
517 predicted by the anhydrous melting model, the temperature-dependent model for  $K$   
518 calibrated at 6 GPa for  $\text{Mg}_2\text{SiO}_4$  can be equally applied at 13 GPa. We conclude,  
519 therefore, that it is more likely that the anhydrous melting temperature is in error, than  
520 that there is a dramatic shift in  $\text{H}_2\text{O}$  speciation at high pressure. This highlights the

521 problems of examining melting point depression in incongruent systems, which are likely  
522 to be even more complex for natural multicomponent systems such as mantle peridotite  
523 melts.

524

525 For  $\text{MgSiO}_3$ , the liquidus depression at 13 GPa is consistent with the Silver and Stolper  
526 (1985) model for nearly complete dissociation to  $\text{OH}^-$  in the melt (Fig. 6). While this is in  
527 contrast to  $\text{Mg}_2\text{SiO}_4$  at the same pressure, it is in better agreement with the experimental  
528 results at 6 GPa. Introducing a temperature dependence to  $K$  is not justified by the data,  
529 within the experimental uncertainties. A molecular  $\text{H}_2\text{O}$  model is far outside of the  
530 experimental constraints, however, as is the model of Tenner et al. (2012a).

531

#### 532 **4.2 The effect of pressure on liquidus depression due to $\text{H}_2\text{O}$ in simple and complex** 533 **silicate systems**

534 The liquidus depression under hydrous conditions in comparison to the anhydrous  
535 melting point is shown for both the  $\text{MgSiO}_3\text{-H}_2\text{O}$  and  $\text{Mg}_2\text{SiO}_4\text{-H}_2\text{O}$  systems at 6 and 13  
536 GPa in Fig. 7. Experimental data of Kushiro et al. (1968) for  $\text{MgSiO}_3\text{-H}_2\text{O}$  at 1 GPa and  
537 between 1375 and 1525 °C are used in order to provide an additional comparison; a value  
538 of  $K = 0.5$  in the Silver and Stolper (1985) formulation provides a good fit to these data.  
539 For  $\text{MgSiO}_3$ , pressure enhances the influence of  $\text{H}_2\text{O}$  in depressing the melting  
540 temperature in line with thermodynamic estimates for the entropy of fusion and the  
541 anhydrous melting curve of  $\text{MgSiO}_3$ . The effect of pressure on the water-driven melting  
542 point depression of  $\text{MgSiO}_3$  is best explained by an increase in the dissociation of  $\text{H}_2\text{O}$



543 with increasing pressure, with essentially no molecular H<sub>2</sub>O being involved above 1400  
544 °C, at pressures of 6 GPa and higher.

545

546 For the Mg<sub>2</sub>SiO<sub>4</sub>-H<sub>2</sub>O binary, however, there is an apparent decrease in the effect of H<sub>2</sub>O  
547 on liquidus depression between 6 and 13 GPa. As discussed above this is most likely  
548 caused by an underestimate in the metastable melting temperature of anhydrous Mg<sub>2</sub>SiO<sub>4</sub>,  
549 which melts incongruently above 10 GPa. If the anhydrous melting temperature is  
550 assumed to be 250 °C higher at 13 GPa, then the effect on liquidus depression is reversed.  
551 This implies that the extrapolated melting curve for Mg<sub>2</sub>SiO<sub>4</sub> is incorrect. The Silver and  
552 Stolper (1985) model with values of  $K = \sim 0.2$  at 2100 °C and approaching 0 at 1300 °C  
553 successfully reproduce experimental data of Hodges (1974) at 3 GPa in the forsterite-H<sub>2</sub>O  
554 system. Data at 3 GPa show lower melting temperature depression in comparison to those  
555 at 6 GPa, is in agreement with the pressure trend observed in the enstatite-H<sub>2</sub>O system  
556 and further suggesting a positive effect of pressure on melting temperature depression.

557

558 In Fig. 7, data for the liquidus depression due to H<sub>2</sub>O for melts of natural peridotite  
559 composition are shown from Tenner et al. (2012a) at 3.5 GPa and Novella and Frost  
560 (2014) at 6 GPa. The depression of melting due to H<sub>2</sub>O is much smaller for these  
561 complex melts compared to either of the simple systems at the same pressure. This  
562 difference is partly due the lower anhydrous liquidus temperatures of the natural  
563 multicomponent melts. As indicated by Eq. (2) the magnitude of the liquidus depression  
564 should increase with the anhydrous melting temperature, as observed in all experiments.  
565 In Fig. 7 these data are fitted using a Silver and Stolper (1985) model with molar mass of

566 37 g/mol per single-oxygen formula unit and a  $\Delta_m S^\circ = 0.4 \text{ J}/(\text{K}\cdot\text{g})$  (Tenner et al., 2012a;  
567 Kojitani and Akaogi, 1997). A constant value of  $\Delta_m S^\circ$  in Eq. (2) is assumed at all  
568 pressures and temperatures and the anhydrous melting temperatures are taken from  
569 Walter (1998). The best correspondence with experiments at 3.5 GPa requires a  
570 temperature dependent value of  $K$ , which starts near unity close to the anhydrous melting  
571 temperature but decreases to effectively zero below 1200 °C. Although there is only one  
572 data point available at 6 GPa the depression of melting is consistent with a similar model  
573 as at 3.5 GPa, with the only difference being the anhydrous melting temperature. The  
574 Silver and Stolper (1985) model, therefore, implies a much smaller extent of H<sub>2</sub>O  
575 dissociation into OH<sup>-</sup> and a greater proportion of molecular H<sub>2</sub>O in multicomponent melts  
576 when compared to simple systems. This difference may have several origins, however.  
577 First, the value of  $\Delta_m S^\circ$  employed for peridotite melt is poorly constrained as it is derived  
578 from calorimetric measurements in the CaO-MgO-Al<sub>2</sub>O<sub>3</sub>-SiO<sub>2</sub> system at 1 bar (Kojitani  
579 and Akaogi, 1997) and it may not suitably account for the effects of pressure and  
580 composition. Second, it is possible that certain components present in the natural  
581 peridotite melt compositions, such as Al<sub>2</sub>O<sub>3</sub>, cause a reduction in the effect of H<sub>2</sub>O on the  
582 configurational entropy of the melt. As a result of such distinct behaviour, the effect of  
583 H<sub>2</sub>O on melting in such simple systems may be quite far away from that in complex  
584 mantle melts.

585

586 Although the justification as to how the melt OH<sup>-</sup> mole fraction is calculated is somewhat  
587 unclear in the model of Tenner et al. (2012a), particularly in relation to the Silver and  
588 Stolper (1985) model, it is interesting to note that it does closely predict the liquidus

589 depression for complex peridotitic melts at both 3.5 and 6 GPa. The model is based on a  
590 3-oxygen melt described by Eq. (11) and it predicts curves identical to those shown in  
591 Fig. 7 using the Silver and Stolper (1985) model for the natural peridotite data at 3.5 and  
592 6 GPa. Although only empirical in its nature, it tends to numerically mimic decreasing  
593 protonation of the oxygen sites in the silicate melt structure, and it produces a good fit to  
594 the natural multicomponent data with fewer adjustable parameters. As there seems to be  
595 no clear justification to the way in which the OH<sup>-</sup> mole fraction is derived in the Tenner et  
596 al. (2012a) model, the predictive capacity may be a coincidence.

597

#### 598 **4.2.1 Hydrous melts along adiabatic temperature gradient**

599 A number of seismic observations appear to show evidence for low shear wave velocities  
600 at the base of the upper mantle above the 410 km discontinuity (e.g. Song et al., 2004;  
601 Vinnik et al., 2009; Jasbinken et al., 2010; Tauzin et al., 2010). These observations have  
602 been proposed to result from the presence of low degree volatile-bearing melts at these  
603 depths (Bercovici and Karato, 2003). Assuming that the upper mantle has a constant H<sub>2</sub>O  
604 content, it might be possible to explain the visibility of H<sub>2</sub>O induced melting at the base  
605 of the upper mantle if pressure enhances melt productivity at these conditions. One way  
606 that this might occur is if less H<sub>2</sub>O were required to stabilise melts with increasing  
607 pressure.

608

609 In Fig. 7 the speciation model of Silver and Stolper (1985) using a temperature-dependent  
610 value of  $K$  varying between ~1 and 0 at 3.5 and 6 GPa is extrapolated to 13 GPa by  
611 assuming an anhydrous melting temperature of 1900 °C at this pressure (Takahashi,

612 1986). The model by Tenner et al. (2012a) would predict an identical liquidus depression.  
613 The results of this extrapolation are given in Fig. 8, which shows the H<sub>2</sub>O content in  
614 MgSiO<sub>3</sub>, Mg<sub>2</sub>SiO<sub>4</sub> and peridotite melts determined at upper mantle adiabatic  
615 temperatures (potential temperature ~1350 °C).

616

617 With increasing pressure the amount of H<sub>2</sub>O required to stabilize Mg<sub>2</sub>SiO<sub>4</sub> melt along a  
618 mantle adiabat increases quite substantially between 6 and 13 GPa. This means that for a  
619 system with a fixed H<sub>2</sub>O content, the percentage of melt will decrease towards conditions  
620 of the base of an upper mantle. This effect would work in conjunction with an increase in  
621 the forsterite-melt H<sub>2</sub>O partition coefficient with pressure (see Hirschmann et al., 2009;  
622 Novella et al., 2014), which would also act to decrease the percentage of melting for a  
623 given bulk H<sub>2</sub>O concentration. By contrast, the H<sub>2</sub>O content of a MgSiO<sub>3</sub> melt appears to  
624 actually decrease slightly between 6 and 13 GPa, which could in theory lead to an  
625 increase in the percentage of melting for a fixed H<sub>2</sub>O content. However, the decrease in  
626 melt H<sub>2</sub>O content is small and this effect would be counteracted by an increase in the  
627 enstatite-melt partitioning coefficient with pressure, calculated from the literature (Rauch  
628 and Keppler, 2002; Yamada et al., 2004; Withers and Hirschmann, 2007; Withers et al.,  
629 2011) and melt H<sub>2</sub>O content from this study. Peridotite melts are also predicted to require  
630 more H<sub>2</sub>O to be stable at higher pressures, although the H<sub>2</sub>O concentrations tend to vary  
631 very little towards the base of the upper mantle similar in fact to MgSiO<sub>3</sub>. This analysis  
632 indicates that there is no evidence for increasing melt productivity due to H<sub>2</sub>O towards  
633 the base of the Earth's upper mantle, although it has to be recognised that there is some  
634 uncertainty as the results for peridotite are being extrapolated above 6 GPa.

635

636 In order for the proportion of hydrous melting to increase and therefore be seismically  
637 more visible towards the base of the upper mantle, the bulk mantle at these conditions  
638 would need to be significantly enriched in H<sub>2</sub>O. Such a localized enrichment in H<sub>2</sub>O at  
639 this depth would require an effective fractionation process to maintain high H<sub>2</sub>O  
640 concentrations at this depth. Bercovici and Karato (2003) proposed that hydrous melts  
641 formed under these conditions may be neutrally buoyant and, therefore, separate from the  
642 upwelling mantle and concentrate to form a low-velocity zone. Such a separation will  
643 depend on melt density, which in turn will depend on the melt H<sub>2</sub>O concentration. Melt  
644 density experiments by Matsukage et al. (2005) favour such a scenario, although their  
645 H<sub>2</sub>O concentrations (~6 wt%) are approximately 50 % of those estimated in this study for  
646 natural peridotitic melts at the bottom of the upper mantle (Fig. 8). Following the density  
647 systematics of Jing and Karato (2009), partial melts in equilibrium with peridotite at 13  
648 GPa should be much less dense than the surrounding mantle if the H<sub>2</sub>O contents in the  
649 melt are close to those predicted here (Fig. 8).

650

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662

### 663 **Appendix: Thermodynamic relations and parameters**

664 The Mie-Grüneisen equations of state (EOS) were employed to determine the Gibbs  
665 energy of melting ( $\Delta_m G^0$ ) of forsterite and enstatite required for the cryoscopic equation  
666 in the  $\text{Mg}_2\text{SiO}_4\text{-H}_2\text{O}$  and  $\text{MgSiO}_3\text{-H}_2\text{O}$  binaries. Expressions to define the Gibbs energy  
667 for  $\text{Mg}_2\text{SiO}_4$  and  $\text{MgSiO}_3$  were taken from Stixrude and Lithgow-Bertelloni (2011) for  
668 solids and from de Koker and Stixrude (2009) for liquids and are based on the  
669 fundamental thermodynamic relation between the Helmholtz energy ( $F$ ) and the Gibbs  
670 energy:

671

$$672 \quad G(P, T) = F(V, T) + PV, \quad (\text{A.1})$$

673

674 where  $V$  is the volume,  $P$  is the pressure and  $T$  is the temperature. The Helmholtz energy  
675 at elevated pressure and temperature is obtained by stepwise integration from ambient  
676 conditions ( $T_0 = 298.15$  K,  $P_0 = 101325$  Pa) *via* isothermal compression at reference  
677 temperature (c) and isochoric heating (th), which accounts for the effect of thermal  
678 vibrations:

679

$$680 \quad F(V, T) = F(P_0, T_0) + \Delta F_c(T_0) + \Delta F_{\text{th}}(V). \quad (\text{A.2})$$

681

682 The contribution to the Helmholtz energy due to isothermal compression ( $\Delta F_c$ ) was  
 683 calculated from the third-order Birch-Murnaghan EOS (Murnaghan, 1937; Birch, 1947;  
 684 e.g. Poirier, 2000):

685

$$686 \quad \Delta F_c(T_0) = 9K_0V_0 \left[ \frac{f^2}{2} + \frac{af^3}{3} \right]. \quad (\text{A.3})$$

687

688 The EOS is based on the finite strain theory, where the finite strain ( $f$ ) and the factor  $a$  are  
 689 calculated as follows:

690

$$691 \quad f = \frac{1}{2} \left[ \left( \frac{V_0}{V} \right)^{2/3} - 1 \right] \quad (\text{A.4})$$

692

693 and

694

$$695 \quad a = \frac{3}{2} (K'_0 - 4). \quad (\text{A.5})$$

696

697 In this formulation,  $K_0$  and  $V_0$  correspond to the bulk modulus and the volume,  
 698 respectively, at the reference pressure and temperature, and  $K'_0$  is the first pressure  
 699 derivative of the bulk modulus at reference conditions. The volume ( $V$ ) of the phase at the  
 700 pressure and temperature of interest was found in order to satisfy the following relation:

701

$$702 \quad P = P_c + P_{\text{th}}, \quad (\text{A.6})$$

703

704 where

705

$$706 \quad P_c = 3K_0 f (2f + 1)^{5/2} (1 + fa) \quad (A.7)$$

707

708 The equations of state for thermal pressure ( $P_{th}$ ) and calculation of the relevant  
709 thermodynamic properties differ for liquid and solid phases. For the liquid phases, the  
710 thermal pressure is defined by

711

$$712 \quad P_{th} = \frac{\gamma}{V} c_v (T - T_0) \quad (A.8)$$

713

714 where  $c_v$  is the isochoric heat capacity, and  $\gamma$ , representing the Grüneisen parameter, is a  
715 function of volume as follows

716

$$717 \quad \gamma = \gamma_0 + \gamma' \left( \frac{V}{V_0} - 1 \right) \quad (A.9)$$

718

719 where  $\gamma_0$  is the Grüneisen parameter at the reference conditions and  $\gamma'$  is its first  
720 derivative with respect to the volume. The thermal contribution to the Helmholtz energy  
721 ( $\Delta F_{th}$ ) of a liquid is then defined by:

722



723 
$$\Delta F_{\text{th}}(V) = -S_0(T - T_0) - c_v \left[ T \ln \left( \frac{T}{T_0} \right) - (T - T_0) \right] - c_v(T - T_0) \left[ (\gamma_0 - \gamma') \ln \left( \frac{V}{V_0} \right) + (\gamma - \gamma_0) \right]$$

724 (A.10)

725 where  $S_0$  is the standard entropy of the substance at a reference state chosen to be  
 726 consistent with literature data as described above (see Table A).

727

728 For the solid phases, a slightly different approach was used starting with the calculation  
 729 of the volume at the pressure and temperature of interest ( $V$ ). The thermal pressure of the  
 730 solid phase was determined using an expression for the Debye thermal energy ( $E_{\text{th}}$ ), that  
 731 is,

732

733 
$$P_{\text{th}} = \frac{\gamma}{V} [E_{\text{th}}(V, T) - E_{\text{th}}(V, T_0)]$$

734 (A.11)

734

735 and, in this case, the Grüneisen parameter is calculated as

736

737 
$$\gamma = \gamma_0 \left( \frac{V}{V_0} \right)^{q_0},$$

738 (A.12)

738

739 where  $q_0$  is a constant, and the thermal internal energy ( $E_{\text{th}}$ ) is defined by the Debye  
 740 model for the lattice vibrational energy

741

742

743 
$$E_{\text{th}} = 9nRT \left( \frac{T}{\theta} \right)^3 \int_0^t \frac{t^3}{e^t - 1} dt, \quad (\text{A.13})$$

744

745 where  $R$  is the universal gas constant,  $n$  is the number of atoms per formula unit,  $t = \theta/T$ ,

746 with the Debye temperature ( $\theta$ ) calculated as

747

748 
$$\theta = \theta_0 e^{\frac{\gamma_0 - \gamma}{q_0}}. \quad (\text{A.14})$$

749

750 The corresponding expression for the thermal Helmholtz energy ( $F_{\text{th}}$ ) of the solid phases,

751 defined as the Debye approximation of the quasi-harmonic vibrational density of states, is

752 as follows:

753

754 
$$F_{\text{th}}(V) = 9nRT \left( \frac{T}{\theta} \right)^3 \int_0^t \ln(1 - e^{-t}) t^2 dt. \quad (\text{A.15})$$

755

756 The thermal contribution to the Helmholtz energy ( $\Delta F_{\text{th}}$ ) of the solid phases between the

757 reference temperature ( $T_0$ ) and that of interest ( $T$ ) at the constant volume of interest ( $V$ ), is

758 found by difference:

759

760 
$$\Delta F_{\text{th}}(V) = F_{\text{th}}(V, T) - F_{\text{th}}(V, T_0). \quad (\text{A.16})$$

761

762 The thermodynamic properties employed in the calculations of the Gibbs energy for solid

763 and liquid  $\text{Mg}_2\text{SiO}_4$  and  $\text{MgSiO}_3$  are summarized in Table A and are based on previous

764 compilations by de Koker and Stixrude (2009) and Stixrude and Lithgow-Bertelloni  
765 (2011) for liquid and solid phases, respectively. The Helmholtz energy for liquid  
766 substances at reference conditions ( $F_0$ ) was empirically calculated from the room  
767 pressure melting temperatures as explained by Liebske and Frost (2012). The reference  
768 state volumes ( $V_0$ ) and entropies ( $S_0$ ) for the liquid end-members were slightly altered  
769 compared to those reported by de Koker and Stixrude (2009) in order to obtain better  
770 agreement with the experimental melting temperatures and to be consistent with  
771 calorimetric data for the enthalpy of melting of  $\text{MgSiO}_3$  and  $\text{Mg}_2\text{SiO}_4$  (Navrotsky et al.,  
772 1989; Richet et al., 1993). Specifically, the thermodynamic data of  $\text{Mg}_2\text{SiO}_4$  liquid of de  
773 Koker and Stixrude (2009) had to be modified such that the value of  $\Delta_m S^\circ$  for forsterite at  
774 1 bar was consistent with 52.7 J/(K·mol) proposed by Navrotsky et al. (1989). This is at  
775 the lower end of the range of values reported in the literature, which vary from 70 to 47.5  
776 J/(K·mol) (Bottinga, 1985; Navrotsky et al., 1989; Richet et al., 1993; Tangeman et al.,  
777 2001). Values for the standard heat capacity and volume of  $\text{Mg}_2\text{SiO}_4$  liquid were then  
778 also adjusted to bring the model into agreement with experimental data on the melting  
779 curve of  $\text{Mg}_2\text{SiO}_4$  (Davis and England, 1964; Kato and Kumazawa, 1985; Presnall and  
780 Walter, 1993).

781

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962

### 963 **Figure captions**

964 **Fig. 1:** Backscattered electron (BSE) images of experiments performed at 6 GPa in the  
965 Mg<sub>2</sub>SiO<sub>4</sub>-H<sub>2</sub>O system. The bright material is the Pt capsule. Grey crystals (50 to 100 µm  
966 across) of forsterite can be easily distinguished from the fine grain quenched melt. (a):

967 figure corresponds to experiment V649 (Table 2) where in order from left to right are  
968 sample chambers containing starting mixtures of  $\text{Mg}_2\text{SiO}_4$  plus 5, 10, 15 and 20.4 wt%  
969  $\text{H}_2\text{O}$  in the bulk. The third chamber from the left shows two quench textures in the same  
970 charge with different fibrous grain sizes, likely formed due to differences in nucleation  
971 and crystal growth (see text). **(b)**: BSE image of experiment V660 (Table 2) where, from  
972 left to right, starting mixtures of  $\text{Mg}_2\text{SiO}_4$  with 7.9, 9.7, 13.8 and 18.3 wt%  $\text{H}_2\text{O}$  (bulk)  
973 were employed.

974 **Fig. 2:** Phase diagram of the  $\text{Mg}_2\text{SiO}_4$ - $\text{H}_2\text{O}$  system at 6 GPa showing experimental data  
975 and models for the liquidus curves (described in the text). Data points determined in this  
976 study are displayed by black and grey symbols (Table 2) while data from Luth (1993) at 6  
977 GPa and Inoue (1994) at 5.5 GPa are shown by blue and green symbols, respectively.  
978 Data from Luth (1993) and Inoue (1994) were determined for bulk compositions of  
979  $\text{Mg}_2\text{SiO}_4$  plus 20.4 wt%  $\text{H}_2\text{O}$  but are plotted at slightly higher  $\text{H}_2\text{O}$  content to aid  
980 visibility. The liquidus at approximately 20 wt%  $\text{H}_2\text{O}$  is  $\sim 200$  °C lower than reported by  
981 Inoue et al. (1994) at 5.5 GPa but is in agreement, within uncertainty, with the data of  
982 Luth (1993) at 6 GPa. The plotted liquidus curves are all constrained by the dry melting  
983 temperature of forsterite at 6 GPa reported by Kato and Kumazawa (1985). Details  
984 regarding the different curves are reported in the text. Uncertainties of 1 wt% in the melt  
985 composition and 50-100 °C for the temperature of the experiments (see text) are  
986 displayed by the error bars.

987 **Fig. 3:** Indicative ternary phase diagrams in the system  $\text{MgO}$ - $\text{SiO}_2$ - $\text{H}_2\text{O}$ . Phase relations  
988 are tentatively constrained at 6 (top) and 13 (bottom) GPa by the experimental results  
989 reported in this study and the literature. Starting compositions in the forsterite- $\text{H}_2\text{O}$  and

990 enstatite-H<sub>2</sub>O joins are plotted as black circles, on a molar basis. Fo: forsterite; En:  
991 enstatite; Per: periclase; St: stishovite; L: liquid (or melt). The dashed line indicates the  
992 Fo + En = L reaction curve while the dotted lines show the possible location of the Fo +  
993 Per = L (toward MgO corner) and En + St = L (toward SiO<sub>2</sub> corner) curves.

994 **Fig. 4:** The depression of the MgSiO<sub>3</sub> liquidus curve at 6 GPa as a function of melt H<sub>2</sub>O  
995 content. Data points determined in this study (Table 2) are displayed by black symbols  
996 while green symbols are from Inoue (1994), plotted at slightly higher H<sub>2</sub>O content to aid  
997 visibility. Uncertainties of 1 wt% in the melt composition and 50-100 °C for the  
998 temperature of the experiments (see text) are displayed by the error bars. Curves  
999 describing the liquidus determined by different models as described in the text are also  
1000 shown. The liquidus curves are all constrained by the dry melting temperature of enstatite  
1001 at 6 GPa reported by Kato and Kumazawa (1985).

1002 **Fig. 5:** Melting phase relations in the Mg<sub>2</sub>SiO<sub>4</sub>-H<sub>2</sub>O system at 13 GPa. Uncertainties of 1  
1003 wt% in the melt composition and 50-100 °C for the temperature of the experiments (see  
1004 text) are displayed. The dry melting temperature of forsterite at 13 GPa was calculated to  
1005 be 2200 °C by extrapolation of the equations of state of de Koker and Stixrude (2009).

1006 **Fig. 6:** The melting phase relations in the MgSiO<sub>3</sub>-H<sub>2</sub>O system at 13 GPa. Uncertainties  
1007 of 1 wt% in the melt composition and 50-100 °C for the temperature of the experiments  
1008 (see text) are displayed. The dry melting temperature of enstatite at 13 GPa was  
1009 calculated to be 2250°C using the model of de Koker and Stixrude (2009). Values of  $a = -$   
1010 8000 K and  $b = 8$  were employed in the calculation of constant  $K$  (red line).

1011 **Fig. 7:** The depression in the hydrous melting temperature as a function of H<sub>2</sub>O for  
1012 MgSiO<sub>3</sub>-H<sub>2</sub>O (black lines), Mg<sub>2</sub>SiO<sub>4</sub>-H<sub>2</sub>O (green lines) and natural (blue lines) melt  
1013 compositions between 1 and 13 GPa. Hydrous garnet peridotite melt compositions are  
1014 from Tenner et al. (2012a) at 3.5 GPa (red dots) and Novella and Frost (2014) at 6 GPa  
1015 (grey square). The blue curves are fitted to these data, as described in the text.

1016 **Fig. 8:** Melt H<sub>2</sub>O contents as a function of pressure determined at 3.5, 6 and 13 GPa and  
1017 at temperatures corresponding to a mantle adiabat (1350 °C, 1400 °C and 1500 °C,  
1018 respectively). Peridotite data are taken from the curves shown in Fig. 7.