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A Coupled Model of Interior Balanced and Boundary Flow

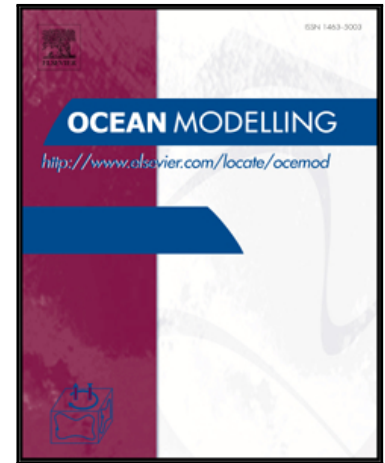
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## 1 **Highlights**

- 2 • Boundary-interior flow interaction
- 3 • Boundary condition determination
- 4 • Mesoscale energy loss
- 5 • Boundary wave dynamics

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**A Coupled Model of Interior Balanced and Boundary Flow**B Deremble<sup>1</sup>

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**Abstract**

Ocean circulation modeling requires parameterizations of sub-grid scale processes, which in turn involves two separate issues. First, the parameterization should mirror the effect of important sub-grid dynamics and second, constants and boundary conditions as required by the parameterization must be determined. In modern ocean circulation modeling, many parameterizations take the form of viscous operators with poorly known coefficients, and the boundary conditions options are free-slip, partial-slip or no-slip, suitably adjusted for the order of the operator. The extent to which viscous operators are dynamically apt is unclear and there is virtually no dynamical guidance on how to choose between the boundary conditions. Often the decision about the suitability of the parameterizations and the boundary conditions is made based on qualitative characteristics of the solution, which is somewhat subjective. Here, a dynamical boundary layer model is developed that explicitly determines the boundary potential vorticity fluxes resulting from the sub-grid scale interactions of the resolved flow with the boundaries. When applied to a quasi-geostrophic model, comparisons of model evolution with high resolution primitive equation simulations are favorable. The recipe outlined here, while far from a complete parameterization of boundary dynamics, represents a step towards resolving the issues currently surrounding sub-grid scale parameterization.

<sup>24</sup> The results also argue that boundary dynamics naturally dissipate balanced energy and are likely  
<sup>25</sup> to represent a principal means by which the oceanic mesoscale energy budget is balanced.  
<sup>7</sup>

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## 1. Introduction

Ocean circulation models employ sub-gridscale parameterizations often represented in the momentum equations as viscous-like operators where the order of the operator can be higher than second. While there are good numerical reasons for this choice, there is no real dynamical justification for it. Poorly known parameters are involved in them and, perhaps even more importantly, several different lateral boundary condition choices are available for them. It is a matter of well-known numerical experience that the nature of mature model circulation is quite sensitive to the sub-gridscale details, affecting such important features as Gulf Stream separation (Bryan et al. (2006), Schoonover et al. (2017)). Indeed, the choices for parameter values and boundary conditions are often made based on which combination results in qualitative model features, such as Gulf Stream separation, that are most realistic. Guidance in sub-gridscale parameterization from dynamical considerations would be of great value, but this is an area in which progress has been slow. The purpose of this paper is to contribute to this topic through examination of a category of boundary mechanics that results in a viscous-like control on interior flows. In contrast to existing parameterizations, the results are relatively insensitive to details of the implementation. We suggest that the approach taken here is a step towards a more complete dynamically based prescription for interior-boundary interactions. A second result is that boundary dynamics are likely to be a significant sink of interior mesoscale energy.

### *a. Background*

The problem of parameterization and boundary condition choices in ocean circulation models arose with the earliest dynamical circulation models. Stommel (1948) avoided lateral boundary conditions by the use of a bottom drag; Munk (1950) with a frictional operator used no-slip boundary conditions. In both cases, the parameterizations and boundary conditions were central

49 to the solutions so obtained. The first attempts at numerical circulation modeling were based in  
50 quasi-geostrophic (qg) dynamics and a variety of viscous operators and boundary condition com-  
51 binations were attempted. A clear demonstration of the solution dependence on the choice of  
52 either partial slip or no-slip appears in Haidvogel et al. (1992). While the no-flux boundary condi-  
53 tion is appropriate for the flow normal to the boundary, the physically suggested no-slip boundary  
54 condition on the tangential flow is less clear due to model discretization (Adcroft and Marshall  
55 (1998)). The manner in which the free-slip/no-slip choice affects the interior in realistic models  
56 with irregular coastlines is also an issue (Adcroft and Marshall (1998)).

57 Most modern ocean simulations are based on the primitive equations which, while dynamically  
58 richer than qg, still exhibit a strong dependence on boundary interactions. Bryan et al. (2006)  
59 systematically investigated parameterization and resolution sensitivities of a North Atlantic circu-  
60 lation model and illustrated the dependency of Gulf Stream separation to them. Here the type of  
61 boundary condition was held fixed (they employed free-slip), however the values and grid-scalings  
62 of the viscous coefficients result in vastly different behaviors. The effects, being centered on Gulf  
63 Stream separation, demonstrate the importance of both the explicit boundary condition and the  
64 amplitude of the various parameters.

65 Most modern circulation models employ a combination of second (Laplacian) and higher order  
66 sub-grid scale parameterizations with parameter values tuned to provide a circulation close to that  
67 of the real ocean (see Chassignet and Garraffo (2001) and Madec (2006)). While the results are  
68 often quite pleasing according to this metric, it is recognized that there is a real need for a better  
69 dynamical understanding of boundary physics in order to remove some of this ambiguity.

70 The model developed in this paper is offered as a step in this direction. The analysis is strongly  
71 rooted in qg dynamics, in which the most significant shortcoming of the boundaries relative to  
72 the real ocean is the restriction to vertical walls. However, the physics that arise involve interior

73 flow interaction with boundary waves and, as such, clear dynamical analogs exist with wave types  
74 belonging to more complicated topography and sloping boundaries. In addition, favorable compar-  
75 isons with primitive equation results suggest that the involved dynamics transcend qg parameteric  
76 limitations. We propose that qg has in this case illuminated processes relevant to the primitive  
77 equations, as it has done frequently in other past settings, such as eddy dynamics. In the present  
78 setting, it is connections between small scale boundary dynamics and the interior balanced flow  
79 that have been captured in the dynamical boundary layer model (DBM) appended to the interior  
80 equations. This study builds on Dewar et al. (2011) where the boundary dynamics were explored  
81 in isolation from their feedback onto the interior. The present study seeks to close the problem by  
82 properly coupling the DBM and the interior so that they evolve simultaneously.

83 While some degree of success has been achieved in this exercise, the parameterization is by  
84 no means complete. Rather, one aspect, hopefully a significant one, of boundary dynamics is  
85 extracted from the complete physical system and clarified.

86 Model development is given in Section 2, and is followed by comparisons between a suite of  
87 models in the next section. Impacts on the system energetics are investigated in Section 4 and the  
88 paper ends with a summary and discussion of future work.

89 **2. Model Development**

90 We start with the hydrostatic equations written in density coordinates

$$\frac{\partial}{\partial t}u + u\frac{\partial}{\partial x}u + v\frac{\partial}{\partial y}u + H\frac{\partial}{\partial \rho}u - fv = -\frac{\partial}{\partial x}M + X \quad (1a)$$

$$\frac{\partial}{\partial t}v + u\frac{\partial}{\partial x}v + v\frac{\partial}{\partial y}v + H\frac{\partial}{\partial \rho}v + fu = -\frac{\partial}{\partial y}M + Y \quad (1b)$$

$$\frac{\partial}{\partial \rho}M = gz \quad (1c)$$

$$\frac{\partial}{\partial t}\frac{\partial}{\partial \rho}z + \nabla \cdot \left( \mathbf{u} \frac{\partial}{\partial \rho}z \right) + \frac{\partial}{\partial \rho}e = 0 \quad (1d)$$

91 where  $u, v$  are horizontal velocities,  $f$  the Coriolis frequency,  $\rho$  density,  $z$  depth of a density surface,92  $(X, Y)$  'viscous' effects and  $M$  the Montgomery potential,

$$M = p + (\rho - \rho_o)gz \quad (2)$$

93 with  $p$  dynamic pressure and  $\rho_o$  a reference density. The quantity  $H$  represents the non-

94 conservative processes affecting density, i.e.

$$\frac{d}{dt}\rho = H \quad (3)$$

95 and is related to the entrainment,  $e$ , by

$$e = H\frac{\partial}{\partial \rho}z \quad (4)$$

96 The depth variable,  $z$ , is broken into a background part dependent only on  $\rho$  and a fluctuation

$$z = \overline{z(\rho)} + z'(x, y, \rho, t) \quad (5)$$



97 In keeping the usual quasi-geostrophic (qg) approach,  $\bar{z}$  (analogous to  $N^2$  in a level model) is  
 98 assumed known. The equations are now scaled in the classical qg way. The result is  
 12

$$\varepsilon\left(\frac{\partial}{\partial t}u + u\frac{\partial}{\partial x}u + v\frac{\partial}{\partial y}u + \Lambda H\frac{\partial}{\partial \rho}u\right) - fv = -\frac{\partial}{\partial x}M + X_oX \quad (6a)$$

$$\varepsilon\left(\frac{\partial}{\partial t}v + u\frac{\partial}{\partial x}v + v\frac{\partial}{\partial y}v + \Lambda H\frac{\partial}{\partial \rho}v\right) + fu = -\frac{\partial}{\partial y}M + Y_oY \quad (6b)$$

$$\frac{\partial}{\partial \rho}M = z \quad (6c)$$

$$\left(\frac{\partial}{\partial \rho}\bar{z}\right)\nabla \cdot \mathbf{u} + \varepsilon\left(\frac{\partial}{\partial t}\frac{\partial}{\partial \rho}z + \nabla \cdot \left(\mathbf{u}\frac{\partial}{\partial \rho}z\right)\right) + \Lambda\frac{\partial}{\partial \rho}e = 0 \quad (6d)$$

99 where  $f$  and all other variables are now non-dimensional and the prime has been dropped from  
 100 the perturbation depth. The parameter  $\varepsilon = U_o/(fL)$  is the Rossby number. The scalings for the  
 101 frictional and diapycnal terms are  $X_o$ ,  $Y_o$  and  $\Lambda$  respectively and are assumed small.

102 Following well-known methods, the above are expanded in powers of the Rossby number, lead-  
 103 ing eventually to the qg equation written in density coordinates

$$\frac{\partial}{\partial t}q + \frac{1}{f}J(M_o, q) = -\nabla \cdot \mathbf{F}_q; \quad q = \frac{1}{f}\nabla^2 M_o - \frac{f}{\bar{z}_\rho}\frac{\partial^2}{\partial \rho^2}M_o \quad (7)$$

104 where  $M_o$  is the lowest order contribution to the Montgomery potential, which is analogous to the  
 105 more familiar equation in depth coordinates. Here  $\mathbf{F}_q$  is the flux of pv due to non-conservative  
 106 effects and other notation is standard. The explicit form of  $\mathbf{F}_q$  is

$$\mathbf{F}_q = \left(\frac{\Lambda}{\varepsilon}H\frac{\partial}{\partial \rho}v_o - \frac{Y_o}{\varepsilon}Y\right)\mathbf{i} + \left(\frac{X_o}{\varepsilon}X - \frac{\Lambda}{\varepsilon}H\frac{\partial}{\partial \rho}u_o\right)\mathbf{j} \quad (8)$$

107 and is consistent with the results of Marshall et al. (2001). We will assume (7) holds everywhere in  
 108 the basin interior. Having shown how non-conservative effects (i.e.  $e$  and  $X$ ,  $Y$ ) appear in qg, we  
 109 will not include them for convenience in the following analysis. They will eventually be included  
 110 again where needed.

111 We examine the possibility that the essential dynamics on the boundary are richer than simple  
 112 qg. In particular, we are interested in interactions between the interior qg flow and flows on

113 the boundary, where Kelvin waves (Pedlosky (2013)) are active. Low mode Kelvin waves when  
 114 viewed from a qg perspective are too fast to be perturbed at leading order by the circulation,  
 115 but higher mode Kelvin waves move more slowly and can be expected to interact with the qg  
 116 flows. Such modes are also associated with short spatial scales in the horizontal (high mode  
 117 deformation radii) and vertical (high mode number). We will build a boundary layer model for qg  
 118 by introducing these two short spatial scales in a standard multiple scales analysis.

119 The procedure will be illustrated for the western boundary layer, although generalization to other  
 120 boundaries is straightforward. We simply substitute

$$\frac{\partial}{\partial x} \rightarrow \frac{\partial}{\partial x} + \frac{1}{\varepsilon} \frac{\partial}{\partial \chi} \quad (9a)$$

$$\frac{\partial}{\partial \rho} \rightarrow \frac{\partial}{\partial \rho} + \frac{1}{\varepsilon} \frac{\partial}{\partial \Gamma} \quad (9b)$$

121 where  $\chi$  is a short zonal variable of  $O(\varepsilon)$  relative to the first baroclinic deformation radius and  $\Gamma$  is  
 122 a short density interval of  $O(\varepsilon)$  relative to the full density range, for the existing zonal and density  
 123 derivatives in (6a). All variables are now expanded in powers of the Rossby number  $\varepsilon$ .

#### 124 a. Multiscale Expansion

125 The leading order equations are somewhat different than the usual qg result due to the presence  
 126 of the fast variables

$$\frac{\partial}{\partial \chi} (u_o \frac{\partial}{\partial \Gamma} z_o) + \frac{\partial}{\partial \rho} \bar{z} \frac{\partial}{\partial \chi} u_o = 0 \quad (10a)$$

$$\frac{\partial}{\partial \chi} M_o = \frac{\partial}{\partial \Gamma} M_o = 0 \quad (10b)$$

$$u_o (\frac{\partial}{\partial \chi} v_o + f) = -\frac{\partial}{\partial y} M_o \quad (10c)$$

127 Eq. (10a) can be written

$$\frac{\partial}{\partial \chi} (u_o \frac{\partial}{\partial \Gamma} z_o) + (\frac{\partial}{\partial \rho} \bar{z}) u_o = 0 \quad (11)$$

128 as the mean state stratification  $\bar{z}$  depends only on  $\rho$ . Thus, because the quantity  $u_o(\frac{\partial}{\partial \Gamma} z_o + \frac{\partial}{\partial \rho} \bar{z})$  is  
 129 a constant throughout the boundary layer, the no-flux condition at the boundary requires it to be  
 130 zero. We also assume the stratification is non-trivial, so in the boundary layer

$$u_o = 0 \quad (12)$$

131 which is expected in qg theory. This however does not imply  $\frac{\partial}{\partial x} u_o$  vanishes in the boundary layer.

132 A second ramification of (12) is

$$\frac{\partial}{\partial y} M_o = 0 \quad (13)$$

133 (see 10c) or that leading order pressure on the boundary is a constant. Again, this agrees with  
 134 classical qg analysis.

135 At the next order in Rossby number, one obtains

$$\frac{\partial}{\partial t} \frac{\partial}{\partial \Gamma} z_o + (\frac{\partial}{\partial \Gamma} z_o + \frac{\partial}{\partial \rho} \bar{z}) (\frac{\partial}{\partial x} u_o + \frac{\partial}{\partial y} v_o + \frac{\partial}{\partial \chi} u_1) + u_1 \frac{\partial}{\partial \Gamma} \frac{\partial}{\partial \chi} z_o + v_o \frac{\partial}{\partial \Gamma} \frac{\partial}{\partial y} z_o = 0 \quad (14a)$$

$$\frac{\partial}{\partial \rho} M_o + \frac{\partial}{\partial \Gamma} M_1 = z_o \quad (14b)$$

$$f v_o = \frac{\partial}{\partial x} M_o + \frac{\partial}{\partial \chi} M_1 \quad (14c)$$

$$\frac{\partial}{\partial t} v_o + u_o \frac{\partial}{\partial x} v_o + v_o \frac{\partial}{\partial y} v_o + u_1 \frac{\partial}{\partial \chi} v_o + u_o \frac{\partial}{\partial \chi} v_1 + f u_1 = -\frac{\partial}{\partial y} M_1 \quad (14d)$$

136 where  $u_o$  has been retained for the moment. Eqs. (10c) and (14c) can be used to eliminate  $M_o$

$$f (\frac{\partial}{\partial x} u_o + \frac{\partial}{\partial y} v_o) = -\frac{\partial}{\partial x} u_o \frac{\partial}{\partial \chi} v_o + \frac{\partial}{\partial y} \frac{\partial}{\partial \chi} M_1 \quad (15)$$

137 Note that the form of (15) converges to leading order divergence-free flow as  $\chi \rightarrow \infty$ .

138 Similarly, (14d) and (10c) can be used to eliminate  $M_1$

$$\frac{\partial}{\partial t} \frac{\partial}{\partial \chi} v_o + u_1 \frac{\partial^2}{\partial \chi^2} v_o + v_o \frac{\partial}{\partial \chi} \frac{\partial}{\partial y} v_o + (\frac{\partial}{\partial \chi} v_o + f) (\frac{\partial}{\partial x} u_o + \frac{\partial}{\partial y} v_o + \frac{\partial}{\partial \chi} u_1) = 0 \quad (16)$$

139 Eq. (16) can be combined with (14a) to yield

$$\frac{D}{Dt} \left( \frac{\frac{\partial}{\partial \chi} v_o + f}{\frac{\partial}{\partial \Gamma} z_o + \frac{\partial}{\partial \rho} \bar{z}} \right) = 0 \quad (17)$$

140 where

$$\frac{D}{Dt} = \frac{\partial}{\partial t} + u_1 \frac{\partial}{\partial \chi} + v_o \frac{\partial}{\partial y} \quad (18)$$

141 Eq. (17) is the potential vorticity equation of the boundary layer and reduces to the identity

$$\frac{D}{Dt} \frac{f}{\frac{\partial}{\partial \rho} \bar{z}} = 0; \chi \rightarrow \infty \quad (19)$$

142 Eq. (17) is analogous to the pv equation used in Dewar et al. (2011) and describes dynamics on  
143 the small boundary scales. We segregate the boundary dynamics from the interior dynamics by  
144 requiring the boundary responses to have vanishing pv anomaly,

$$\frac{\frac{\partial}{\partial \chi} v_o + f}{\frac{\partial}{\partial \Gamma} z_o + \frac{\partial}{\partial \rho} \bar{z}} = \frac{f}{\frac{\partial}{\partial \rho} \bar{z}} \quad (20)$$

145 Using (10b) and (14c) reduces (20) to

$$\frac{\partial^2}{\partial \chi^2} M_1 - \frac{f}{\frac{\partial}{\partial \rho} \bar{z}} \frac{\partial^2}{\partial \Gamma^2} M_1 = 0 \quad (21)$$

146 which is the elliptic equation also appearing in Dewar and Hogg (2010) and Dewar et al. (2011).  
147 The solution of this equation is obtained by projecting it on the complete set of orthogonal func-  
148 tions defined by the eigenvalue problem

$$\frac{\partial^2}{\partial \Gamma^2} F_n - \frac{\frac{\partial}{\partial \rho} \bar{z}}{f} \lambda_n^2 F_n = 0; \quad \frac{\partial}{\partial \Gamma} F_n = 0; \quad \rho = (\rho_s, \rho_b) \quad (22)$$

149 The equation resulting from (21) admits growing and decaying exponentials, the latter of which  
150 is retained to be consistent with the boundary layer analysis (see Dewar and Hogg (2010) for a  
151 discussion of the linear limit).

### 152 *b. Boundary-Interior Connection*

153 At this point, the analysis has shown the interior pv equation is faced with a constant pressure on  
154 the boundary, but the value of the constant is unknown. In addition, the dynamics of the boundary

155 layer reside in the elliptic equation (21) which needs boundary conditions at  $\chi = 0$  for a unique  
 156 solution.

157 The first step to obtain this information is to evaluate (14d) at the wall

$$\frac{\partial}{\partial t} v_o + v_o \frac{\partial}{\partial y} v_o + \frac{\partial}{\partial y} M_1 = 0 \quad (23)$$

158 Integrating (23) around the domain yields

$$\frac{\partial}{\partial t} \int_{\partial A} \mathbf{v}_o \cdot \mathbf{n} dl = 0 \quad (24)$$

159 provided the along wall velocity is continuous. If, as in the classical qg equations, the along wall  
 160 flow is provided only by the interior geostrophic dynamics, (24) becomes

$$\frac{\partial}{\partial t} \int_{\partial A} \nabla M_o \cdot \mathbf{n} dl = 0 \quad (25)$$

161 which is the usual condition determining the boundary Montgomery potential value (see  
 162 McWilliams (1977)).

163 However, in the present case, from (14c), the quantity  $v_o$  is seen to consist of two parts, a  
 164 geostrophic part connected to the interior and a geostrophic (in the along wall direction) part that  
 165 belongs to the boundary. Thus, (23) can be rewritten

$$\begin{aligned} & \frac{\partial}{\partial t} \frac{\partial}{\partial \chi} M_1 + v_g \frac{\partial}{\partial y} \frac{\partial}{\partial \chi} M_1 + \frac{\partial}{\partial \chi} M_1 \frac{\partial}{\partial y} v_g + \\ & \frac{\partial}{\partial \chi} \frac{M_1}{f} \frac{\partial}{\partial y} \frac{\partial}{\partial \chi} M_1 + f \frac{\partial}{\partial y} M_1 = -f \left( \frac{\partial}{\partial t} v_g + v_g \frac{\partial}{\partial y} v_g \right) \end{aligned} \quad (26)$$

166 where  $v_g$  denotes the interior geostrophic meridional velocity evaluated at  $x = 0$ .

167 Note that the solution of (26) is a prediction for the normal derivative of  $M_1$  and, as such, is the  
 168 boundary condition needed to uniquely solve (21). Eq. (26) is also the equation solved in Dewar  
 169 et al. (2011) to compute the forced Kelvin wave response given a specified interior geostrophic  
 170 field. The differences here are that the interior is allowed to evolve dynamically and interact with

171 the boundary response via the solution to (23). The boundary connection to the interior remains to  
 172 be determined.  
 17

173 Eq. (26) is hyperbolic and the characteristic solution of it leads to isopycnals pinching together,  
 174 and the unphysical result that  $v_o$  becomes multivalued (see Dewar et al. (2011)). At such locations,  
 175 we instead require that fronts form and stabilize when the isopycnals become vertical (i.e. they  
 176 are so-called 'weak' or discontinuous solutions (Whitham (1974)) of (23)). The fully developed  
 177 forms for the fronts are characterized by

$$\frac{\partial}{\partial \chi} v_o + f = \frac{\partial}{\partial \Gamma} z_o + \frac{\partial}{\partial \rho} \bar{z} = 0 \quad (27)$$

178 The latter constraint is equivalent to the layer thickness vanishing, while the former is a statement  
 179 of zero absolute vorticity and is needed for the potential vorticity to remain finite. With vanishing  
 180 layer thickness, and associated discontinuities in along-wall velocity, the quantity  $v_o$  becomes

$$v_o = v_s + \sum_i \Delta v_i H(\mathbf{x} - \mathbf{x}_i) \quad (28)$$

181 where  $v_s$  is a smooth function,  $\mathbf{x}$  is a location on the boundary and the index  $i$  denotes the front at  
 182 location  $\mathbf{x}_i$ . The function  $H$  is related to the usual Heaviside function and is defined by

$$H(x) = 0; \quad x < 0; \quad H(0) = 1/2; \quad H(x) = 1; \quad x > 0 \quad (29)$$

183 In other words, the along wall velocity is a smooth function interrupted by a series of step dis-  
 184 continuities. The various derivatives in (26) thus involve Dirac delta functions, and the full line  
 185 integral in (25) becomes a sum of measures of the discontinuities at the fronts. Recalling that the  
 186 full along wall velocity is composed of both a (smooth) interior geostrophic velocity and a wall  
 187 response

$$\frac{\partial}{\partial t} \int_{\partial A} \mathbf{v}_g \cdot \mathbf{n} dl = -\sum_i \left( \left( -\frac{\partial}{\partial t} \mathbf{x}_i \right) \Delta(v_i) + \Delta \frac{v_i^2}{2} + \Delta M_{1,i} \right) \quad (30)$$

188 where  $\frac{\partial}{\partial t} \mathbf{x}_i$  denotes the rate at which the front at  $\mathbf{x}_i$  moves. According to (30), fronts modify net  
 189 geostrophic circulation which, in turn, influences the value of the boundary Montgomery potential.  
 18

190 A change in net circulation is equivalent to a change in integrated vorticity, which implies the  
 191 appearance of new vorticity in the interior, so it is still necessary to indicate how the circulation  
 192 changes in (30) appear as qg vorticity. Recalling that in the presence of viscous effects, the adia-  
 193 batic (i.e.  $e = 0$ ) qg equation is

$$\frac{d}{dt} q_o = -\nabla \cdot \mathbf{F}_q = \frac{\partial}{\partial x} Y - \frac{\partial}{\partial y} X \quad (31)$$

194 where viscous scalings have been set to unity and  $X, Y$  are the nonconservative effects working on  
 195 the momentum equations. When solving the viscous qg equations numerically, it is thus necessary  
 196 to apply a net boundary pv flux to the equations, which for a north-south boundary consists of the  
 197 value of  $Y$  on the boundary.

198 The full boundary velocity equation including viscous effects is

$$\frac{\partial}{\partial t} v_o + v_o \frac{\partial}{\partial y} v_o + \frac{\partial}{\partial y} M_1 = Y \quad (32)$$

199 where  $Y$  is expected to be small everywhere but in the fronts. With  $Y$  explicitly present, the  
 200 structure for  $v_o$  becomes smooth (i.e. the fronts are no longer discontinuous, but are locations of  
 201 very large but finite gradients), so if we consider an integration over a boundary segment from just  
 202 behind a front to just ahead of a front, there results

$$\left(-\frac{\partial}{\partial t} y_i\right) \Delta v_i + \Delta\left(\frac{v_i^2}{2}\right) + \Delta M_{1,i} = \int_{y_i^-}^{y_i^+} Y dy \quad (33)$$

203 Equivalently, the value of the net boundary flux at the frontal location is determined by the front  
 204 parameters. Effectively, the front injects vorticity into the domain, where the ultimate source of  
 205 the vorticity is viscosity. The full solution of the qg system thus consists of simultaneously solving  
 206 the qg equation (with (30) as a boundary condition) and (32), using the latter to determine the pv

flux from the boundaries into the interior via (33). The equations (30), (32) and (33) constitute our DBM.

### 3. Numerical Examples

We have implemented the above procedure in the quasi-geostrophic model Q-GCM (Hogg et al. (2003)). The viscous term  $Y$  is parameterized as an along wall Laplacian acting on  $v_o$ , which with the viscous coefficient used here ( $\nu = 50m^2/s$ ) was sufficient to control the fronts.

We have compared the parameterized qg evolution with numerical solutions obtained using the MITgcm (Marshall et al. (1997)) and the isopycnal model GOLD (Hallberg (2000)) run at high resolution.

Parameters typical of a mid-latitude  $\beta$  plane ocean have been used, i.e.  $f = 10^{-4} s^{-1}$  and  $\beta = 2 \times 10^{-11} s^{-1}$ . The basic state stratification for the MITgcm was set by a linear temperature profile in the vertical

$$T_b = \Delta T \left(1 - \frac{z}{H}\right), \quad (34)$$

with  $H = 1000m$  the depth of the water column and  $\Delta T = 5 K$  the temperature difference between the top and the bottom. The same profile was used to determine layer temperatures in both GOLD and Q-GCM. A linear equation of state is used with thermal expansion coefficient  $\alpha = 2 \times 10^{-4} K^{-1}$ .

We consider the initial value problem of a monopolar vortex situated 75km east and 200km north of the southwestern corner of a 500km  $\times$  500km domain (see Fig. 1). The form used for the vortex was

$$v_\theta(r) = v_o F(z) \frac{\tanh(r/r_o)}{\cosh^2(r/r_o)}, \quad (35)$$

with

$$F(z) = 1 - erf(z/z_o) \quad (36)$$



where  $r$  is a radial coordinate extending from vortex center,  $r_o = 75km$ ,  $z_o = 500m$  and  $v_\theta$  is the corresponding swirl velocity. The initial vortex position was sufficiently far from the boundaries that the above formulas were used without modification at the walls.

The horizontal structure of the vortex is a continuous approximation of the Rankine vortex (Doswell 1984). At any height  $z$ , we use the geostrophic balance to recover the pressure field

$$\frac{dP}{dr} = fv_\theta, \quad (37)$$

which can in turn be used to infer the density field via the hydrostatic balance. The vertical function (36) is chosen such that both the velocity and the density anomalies are maximum at the surface. This field is used to initialize the three models, all of which employ a  $1km$  horizontal resolution. The MITgcm employs 100 levels with a resolution of  $10m$ , while GOLD and Q-GCM both use 10 layers with a constant reduced gravity of  $10^{-3}m s^{-2}$ . The vertical profile of temperature from the MITgcm and the layer thicknesses from GOLD are plotted in Fig. 2. Note that there is no outcropping in the layered model because all of the outcropped densities in the MITgcm are contained within in the uppermost GOLD model layer. We use a harmonic viscosity of  $\nu = 50 m^2 s^{-1}$  for GOLD and Q-GCM,  $\nu = 10 m^2 s^{-1}$  for MITgcm and free slip boundary conditions in all cases.

### *a. Results*

A typical vortex sequence as shown in surface relative vorticity appears in Fig. 3 from the GOLD experiment, in Fig. 4 for the MITgcm experiment and in Fig. 5 from the Q-GCM experiment. Early on the vortex migrates westward towards the wall due to  $\beta$ . As it is squeezed on the wall it deforms and propagates northward as expected from 'image' (see Crosby et al. (2013) and references therein) dynamics (Day 20). This part of the evolution is entirely consistent with purely

248 balanced dynamics. For unknown reasons, the initial westward vortex drift differs between the  
249 models; the GOLD vortex arrives at the wall a few days earlier than in either the MITgcm or  
250 Q-GCM (compare to Figs. 4, 5).

251 Upon commencing northward propagation, a very strong cyclonic vorticity filament is peeled  
252 away from the wall by the vortex in all models (Figs. 3a, b; 4a, b; 5a, b). The source of the  
253 vorticity is, however, not a frictional sublayer as the boundary conditions are free slip. This part  
254 of the evolution has no analog in inviscid  $qg$  theory. A similar result was seen in Dewar and Hogg  
255 (2010), and the explanation provided there involved the arresting of southward propagating Kelvin  
256 waves by the northward directed flows of the anticyclonic vortex.

257 If sufficiently strong, the newly formed cyclonic filament rolls up onto itself to form a macro-  
258 scopic cyclone (Fig. 3b) which pairs up with the primary anticyclone to form a dipole. This occurs  
259 for all three models, although the strength of the cyclonic partner varies and so the subsequent evo-  
260 lution can follow more than one path. The asymmetric pair in GOLD moves the primary vortex  
261 away from the wall and they follow a curved trajectory eventually returning to the wall ((see Days  
262 30 and 40); Fig. 3b, c). The GOLD dipole splits when it again encounters the wall: the cyclone  
263 moves southward and the anticyclone resumes its northward migration. At this point, a new cycle  
264 of cyclonic vorticity generation begins (Fig. 3d).

265 The details of the dipolar evolution are highly dependent on the amount of newly created vor-  
266 ticity at the boundary. Strong vorticity creation (compared to the vorticity of the primary vortex),  
267 moves the pair faster away from the wall and, as seen in the MITgcm results, can even split the  
268 primary vortex into two parts (cf. Fig. 4d). For weak vorticity generation, the positive vorticity  
269 filament may simply be advected around the primary cyclone without forming a coherent vortex.  
270 In such a situation, the primary vortex may not move away from the wall. This is seen early in the

271 Q-GCM vortex, although continued cyclonic vorticity generation eventually results in a cyclonic  
 272 vortex.

273 Figs. 6, 7, and 8 illustrate the vorticity injection process. Here, the interface displacement (con-  
 274 tours) and velocity (colors) on the wall are plotted. In all three cases, as the anticyclone migrates  
 275 northward, the upper layers 'pinch' such that the flow in these layers is blocked. Most importantly,  
 276 there is effectively a discontinuity in the velocity profile and the Montgomery potential in these  
 277 layers upon which we base the PV injection in the qg model (see (33)). This is consistent with  
 278 the mean flow-Kelvin wave interaction idea that the anticyclone presence is critical to maintaining  
 279 the discontinuity. Indeed, if the subsequent evolution moves the vortex away from the boundary,  
 280 the front can dissolve. This is seen at Day 40 in Fig. 6c, where the vortex has been forced away  
 281 from the wall by the newly created cyclone. As the cycle restarts, we observe strong similarities  
 282 between the plots in Fig. 6b and 6d. The sequences displayed in these figures are not identical, but  
 283 agree qualitatively in the marked evolution of the wall isopycnals and the appearance of cyclonic  
 284 vorticity.

285 The initial condition in these experiments consists only of anticyclonic vorticity and, for that  
 286 matter, negative pv anomaly (not shown). Cyclonic vorticity for the most part appears in areas  
 287 consistent with our explanation based on front formation, i.e. it streams from regions on the wall  
 288 slightly north of the vortex center. However, cyclonic vorticity also appears elsewhere in many  
 289 of the plots, as in Fig. 3b, c and d. The other cyclonic zones are not of a wall origin, as can  
 290 be seen in Fig. 9a, which shows potential vorticity at Day 40 from the GOLD results. Note in  
 291 particular the cyclonic streamer along the southwestern boundary between 50km and 200km in  
 292 Fig. 3c. This feature is visible in pv as a streamer whose value is not anomalously high; rather  
 293 at  $pv \sim 1 \times 10^{-6} m^{-1} s^{-1}$  it corresponds to the background. Since the wall injects pv into the system  
 294 and the cyclonic streamer is not anomalous in pv, it is clear that cyclonic vorticity is a result of

295 conservative pv evolution. In contrast, the large region of intense cyclonic vorticity paired with  
296 the original vortex in Fig. 3c corresponds to a strong positive pv anomaly in Fig. 9a. Because such  
23  
297 pv is not present in the initial condition, it can only be the result of wall injection. Such behavior  
298 is characteristic of the pv fields in both the GOLD and MITgcm runs. An example of pv from the  
299 Q-GCM at Day 40 appears in Fig. 9b. Here again a positive pv anomaly appears at the location  
300 of cyclonic vorticity, but nowhere else. By construction, the source of this pv is due to the wall  
301 interaction, which supports our theoretical modeling.

302 In Fig. 10, we plot the time series of the mean circulation in the upper layer (total circulation  
303 divided by the area of the domain). Recall that the models all employ free-slip boundaries, so the  
304 boundary effect on circulation would normally be expected to be small. This is what happens ini-  
305 tially. Until day 20 there is no significant variation in the circulation as the vortex moves westward  
306 towards the wall. However, between day 20 and day 40 strong circulation changes are seen, even  
307 to the point of reversing the sign of the circulation. At day 40, the mean circulation is about 10  
308 times stronger than its initial absolute value. This increase corresponds to the injection of cyclonic  
309 filaments into the domain (see Figs. 3, 4, and 5). As mentioned previously, the injection starts  
310 earlier in GOLD. After the initial injection, we expect the three curves to only qualitatively match:  
311 in MITgcm, the injection is stronger and forces the vortex further away from the wall such that the  
312 next peel off and strong circulation change do not occur before day 70.

313 In Fig. 10, we also add a curve for an MITgcm experiment using  $v = 50 \text{ m}^2 \text{ s}^{-1}$  (dashed red  
314 line) instead of  $v = 10 \text{ m}^2 \text{ s}^{-1}$  as discussed previously. For this configuration (using the same vis-  
315 cosity as GOLD and Q-GCM), the vorticity injection was much weaker and inadequate for the  
316 formation of a coherent cyclone. The reason for this distinction is due to the potentially very dif-  
317 ferent physical effects of 'horizontal' viscosity in isopycnal and level models. Away from fronts  
318 where isopycnals have small slopes, layer horizontal and level horizontal viscosity play compa-

319 rable roles. Near fronts, however, 'horizontal' layer viscosity in transferring momentum along  
 320 isopycnals acts almost in a vertical sense, whereas in a level model, momentum transfers are  
 24  
 321 largely across isopycnals. This works to smooth the along wall velocity profile for a level model  
 322 such that front formation and the accompanying vorticity injection are suppressed. The tendency  
 323 for the isopycnals to form fronts in that experiment was largely suppressed (not shown).

#### 324 4. Energetics Consequences

325 Consider now the balanced energetics of a closed basin. This is obtained by multiplying the  $qg$   
 326  $pv$  equation by the Montgomery potential and integrating by parts.

$$\begin{aligned}
 & \int_{\rho_s}^{\rho_b} \int_S (M_o \frac{\partial}{\partial t} q + M_o \mathbf{u}_o \cdot \nabla q) \frac{\partial}{\partial \rho} \bar{z} dA d\rho = \\
 & \int_V (M_o \frac{\partial}{\partial t} q_o + M_o \mathbf{u}_o \cdot \nabla q_o) dV = \\
 & - \frac{\partial}{\partial t} \int_V \left[ \frac{(\nabla M_o)^2}{2f} - \frac{f}{\frac{\partial}{\partial \rho} \bar{z}} \frac{(\frac{\partial}{\partial \rho} M_o)^2}{2} \right] dV \\
 & + \int_z \left[ \oint M_o \frac{\partial}{\partial t} \nabla M_o \cdot \mathbf{n} dl \right] dz - \int_S f_o w_e M_o dA = - \int_V M_o \nabla \cdot \mathbf{F}_Q dV \quad (38)
 \end{aligned}$$

327 where  $w_e$  denotes any Ekman pumping energy source. The no-normal flow conditions have been  
 328 used to eliminate advection and the domain extends into the overlap region of the boundary layer  
 329 where  $qg$  is still accurate. The boundary layer analysis assures that the leading order Montgomery  
 330 on the edge must be a constant on any isopycnal, thus allowing it to be migrated outside of the  
 331 boundary line integral in (38). The result is

$$\frac{\partial}{\partial t} \int_V (K + P) dV = - \int_S w_e M_o dA + \int_z M_o \int \frac{\partial}{\partial t} \nabla \frac{M_o}{f} \cdot \mathbf{n} dl dz - \Xi \quad (39)$$

332 where free slip boundaries have been used,

$$K = \frac{(\nabla M_o)^2}{2f} \quad (40)$$

333 and

$$P = \frac{f}{\frac{\partial}{\partial \rho} \bar{z}} \frac{(\frac{\partial}{\partial \rho} M_o)^2}{2} \quad (41)$$

334 are the kinetic and potential energies seen in (38) and  $\Xi$  denotes viscous loss proportional to  
335 velocity gradients squared integrated over the domain.

336 A statement about the net geostrophic circulation change is needed to complete the equation.

337 This is obtained from (30), such that (39) becomes

$$\frac{\partial}{\partial t} \int_V (K + P) dV = - \int_S w_e M_o dA - \Xi - \int_z \Sigma_i \left( \left( -\frac{\partial}{\partial t} \mathbf{x}_i \right) \Delta(v_o) + \Delta \frac{v_o^2}{2} - \Delta M_1 \right) M_o dz \quad (42)$$

338 Thus the fronts governed by (26) act like an energy sink on the interior balanced flow. Physically  
339 the sink represents flow up the pressure gradients along the boundaries set up and maintained by  
340 the wall dynamics.

341 Eq. (42) (with  $w_e = 0$ ) can be used to examine the energetics in the present case. Fig. 11 (left)  
342 compares the time evolution of the kinetic and potential energy relative to their initial values in  
343 the three models. The curves all show their strongest behavior from days 20 to 40 during the  
344 period of strong wall-vortex interaction. Consistently among the three models, potential energy  
345 transfers aggressively to kinetic energy during this interval. The level of kinetic energy reached  
346 after 40 days is about twice its initial value (not shown). After 40 days, the APE dropped by  
347 50% in both Q-GCM and Gold and 25% in MITgcm (not shown). After 40 days in MITgcm,  
348 we mentioned previously that the interaction with the wall is less pronounced as the eddy moves  
349 away from the wall. This tendency is also visible in the PE and KE curves. Note also the overall  
350 energetic behavior differs between the MITgcm and the layer models. This is due to the differences  
351 in model construction and the differing trajectories of the vortex relative to the wall.

352 Total energy evolutions from the three model runs appear in Fig. 11 (right). Very early ( $< 20$   
353 day) energy decreases slowly at a rate that can be accounted for from internal dissipation,  $\Xi$ . This

354 changes significantly once the vortices begin interaction with the boundary. Consistent with our  
355 earlier discussion, total energy decays first for GOLD, where the vortex experiences its earliest  
26  
356 encounter with the wall. Both GOLD and Q-GCM exhibit roughly comparable decay rates. The  
357 MITgcm is considerably slower in energy loss. However, upon inspection of Fig. 7, it is seen  
358 that after the initial wall encounter, the cyclone is able to push the vortex away from the boundary  
359 much more effectively in the MITgcm than in the other models. As a result, the MITgcm cyclonic  
360 vorticity generation, and thus energy decay, for the duration of the experiments is much less.

## 361 5. Summary

362 We have revisited the problem of boundary conditions for general circulation models. When  
363 applied to the problem of a westward drifting vortex encountering a boundary, classical qg im-  
364 plementations with free-slip boundary conditions leave the net circulation of the domain virtually  
365 unchanged. In contrast, primitive equation models inject strong cyclonic vorticity into the domain  
366 and as a result lose energy considerably faster when compared to the qg result. We have proposed  
367 a boundary layer analysis that, when used in a qg model (effectively as a DBM), endows it with  
368 energy and vorticity behavior like that computed from the primitive equation models.

369 The essence of the analysis is in the interaction between interior balanced dynamics and bound-  
370 ary dynamics, the latter generally arising because of the no-normal flow boundary condition. The  
371 wall dynamics are constrained to have no potential vorticity anomaly; for the case of a wall, Kelvin  
372 waves are the result. When the interior flow imposes a velocity on the wall in excess of a Kelvin  
373 wave phase speed, the blocked downstream wave propagation builds a finite amplitude response  
374 in the form of fronts. Regularization of the fronts, given their form, requires either viscous or  
375 diabatic effects that, when expressed in a pv framework constitute a pv flux from the wall. The  
376 size of the flux can be computed from the front characteristics themselves and as such does not

377 require an explicit viscous or diabatic coefficient. The effect of the wall parameterization is to add  
378 the frontal pv flux to the preexisting interior pv distribution. This effect, when introduced into qg,  
379 qualitatively and quantitatively (if not exactly) amends the qg evolution to that seen in primitive  
380 equation models. We have also found that these mechanics effectively drain energy from the inte-  
381 rior balanced flow, suggesting that a resolution to the open question of the fate of balanced energy  
382 involves boundary dynamics.

383 While we think of this as a DBM for subgrid-scale parameterization, it describes only a subset  
384 of possible interior-boundary interactions. These mechanics require an interior flow counter to  
385 the direction of topographic waves; the case of oppositely directed flows remains unstudied. Fur-  
386 ther, aspects of the present interaction remain unclear. The boundary fronts govern the amplitude  
387 of the effect on the interior, but the nature of the frontal dynamics remains unclear. The fronts  
388 themselves are related to the pv fluxes, thus making the feedback relatively insensitive to poorly  
389 known parameters like eddy diffusivities, but we have also found too large of an eddy viscosity  
390 can damp these mechanics. We speculate that the fronts exist in a regime independent of viscous  
391 coefficients, but have yet to uncover this regime. We have also shown only how to amend sub-grid  
392 scale qg dynamics with our DBM. Further studies will explore recipes for including these effects  
393 into the sub-grid scale parameterization of primitive equations.

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## 397 APPENDIX

### 398 **An Augmented Jacobian for Stratified QG**



399 The Arakawa Jacobian is routinely used for the advection operator in quasi-geostrophy. While it  
 400 is generally apt, stratified qg boundary conditions are not necessarily consistent with the classical  
 28  
 401 implementation. The analytical properties of the Jacobian for constant boundary  $p$  are

$$\begin{aligned}\int_A J(p, q) dA &= 0 \\ \int_A pJ(p, q) dA &= \int_A J\left(\frac{p^2}{2}, q\right) dA = 0 \\ \int_A qJ(p, q) dA &= \int_A J\left(p, \frac{q^2}{2}\right) dA = 0\end{aligned}\quad (\text{A1})$$

402 because of no normal flow. As shown by Salmon and Talley (1989), the classical Arakawa dis-  
 403 cretization is consistent with these properties only if the boundary  $p(\partial A)$  vanishes, which in a  
 404 stratified system is not generally true. Equivalently, the classical Arakawa formulation does not  
 405 meet (A1), as can be shown by straightforward numerical integration. Holland (1978) noticed this  
 406 and instead developed an energy equation by multiplying the pv equation by a pressure adjusted  
 407 for the boundary pressure. Here, closely following Salmon and Talley (1989), a generalization to  
 408 the Arakawa Jacobian is developed that allows for non-zero boundary pressure.

409 Potential vorticity conservation implies

$$\int_A \alpha \left( \frac{\partial}{\partial t} q + J(p, q) \right) dA = 0 \quad (\text{A2})$$

410 for any  $\alpha(x, y)$ . Manipulating the arguments, one can show

$$\int_A \alpha J(p, q) dA = \int_A q J(\alpha, p) dA \quad (\text{A3})$$

411 by using only the no-normal flow condition on  $p$ . However, if the other permutation of arguments  
 412 is attempted, there results

$$\int_A \alpha J(p, q) dA = \int_A p J(q, \alpha) dA - p(\partial A) \int_{\partial A} \nabla q \cdot \mathbf{t} dl \quad (\text{A4})$$

413 where  $\mathbf{t}$  is the unit vector tangential to the domain boundary. The last integral on the right hand  
 414 side is not guaranteed to vanish for non-zero boundary pressure.

415 The integrated Jacobian can in general be written

$$\begin{aligned}
 \int_A \alpha J(p, q) dA &= a \int_A \alpha J(p, q) dA + \\
 b \left( \int_A p J(q, \alpha) dA - p(\partial A) \int_{\partial A} \alpha \nabla q \cdot \mathbf{t} dl \right) &+ c \int_A q J(\alpha, p) dA
 \end{aligned} \tag{A5}$$

416 where  $a + b + c = 1$ . We now express (A2) symbolically in discrete form

$$\begin{aligned}
 \sum_i \delta A_i \alpha_i \left( \frac{\partial}{\partial t} q \right)_i &= \sum \delta A_i [a \alpha_i J_i(p_j, q_k) + b p_i J_i(q_j, \alpha_k) + \\
 c q_i J_i(\alpha_j, p_k)] &+ \delta l_i p(\partial A) \alpha_i (\nabla q)_i \Delta_{i,ib} = F(\alpha_i, q_j, p_k; a, b, c)
 \end{aligned} \tag{A6}$$

417 where  $\delta A_i$  is the area element associated with point  $i$ ,  $\delta l_i$  the line element associated with boundary

418 point  $i$  and  $\Delta_{i,ib}$  is the Kronecker delta function defined by

$$\begin{aligned}
 \Delta_{i,ib} &= 1; \quad i = ib \\
 \Delta_{i,ib} &= 0; \quad \textit{otherwise}
 \end{aligned} \tag{A7}$$

419 with  $ib$  the index of a point on the boundary. The Salmon and Talley (1989) notation has been

420 used, but the form of  $F$  is different. From (A6), one can show

$$- \frac{\partial}{\partial t} q_i = \frac{\partial}{\partial \alpha_i} F \tag{A8}$$

421 which specifies the form of the Jacobian that satisfies (A2).

422 The only modification to (A6) from that appearing in Salmon and Talley (1989) are terms on the

423 boundary, implying that the classical Arakawa discretization applies to the interior gridpoints. On

424 the boundary, the usual discretization must be augmented by any discretization satisfying

$$\oint \nabla q \cdot \mathbf{n} dl = \oint q \nabla q \cdot \mathbf{n} dl = 0 \tag{A9}$$

425 The second order discretization

$$\left( \frac{\partial}{\partial x} q \right)_i = \frac{q_{i+1} - q_{i-1}}{2\Delta_l} \tag{A10}$$

426 meets this criterion provided the  $q$  in the second line integral is evaluated at point  $i$ . Evaluating  
 427  $F$  and taking the derivative in (A8) determines the required Jacobian stencil. For a point on a  
 30  
 428 north-south wall, the usual discretization must be modified to

$$J_{ib,j}(p, q) = J_{ib,j}(p, q)_{Arakawa} + p(\partial A)(q(i_b, j+1) - q(i_b, j-1)) \quad (\text{A11})$$

429 where  $ib, j$  are the zonal and meridional indices of a western boundary point. A straightforward  
 430 modification of the above applies to points on other boundaries.

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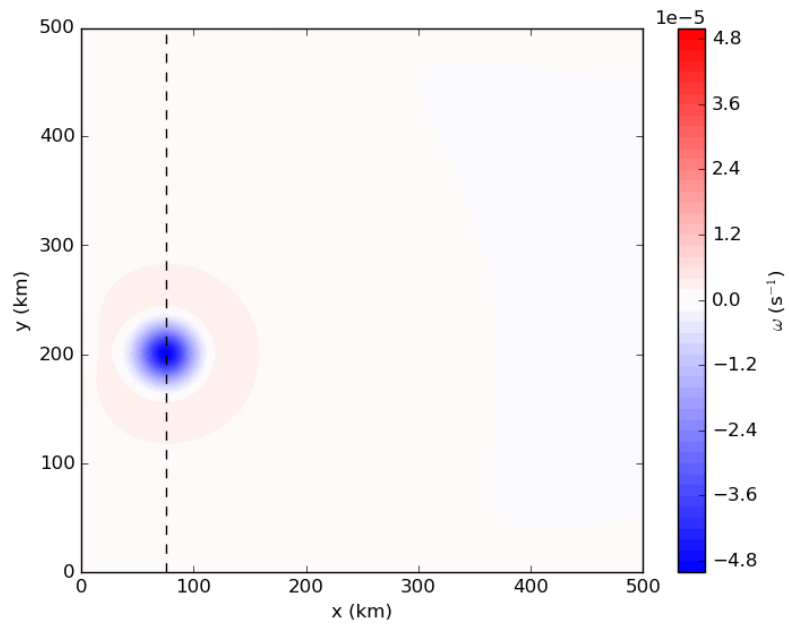


FIG. 1: Surface vorticity profile (same initial condition used in all three models).

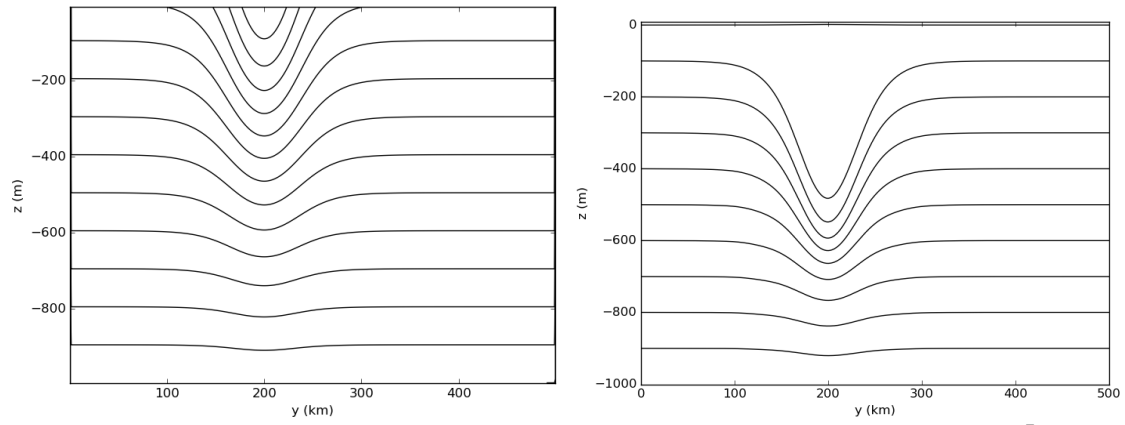


FIG. 2: Left: Vertical temperature profile along the dashed line in Fig. 1 for the MITgcm (contour interval: 0.5 K). Right: position of the isopycnals in GOLD along the same section.

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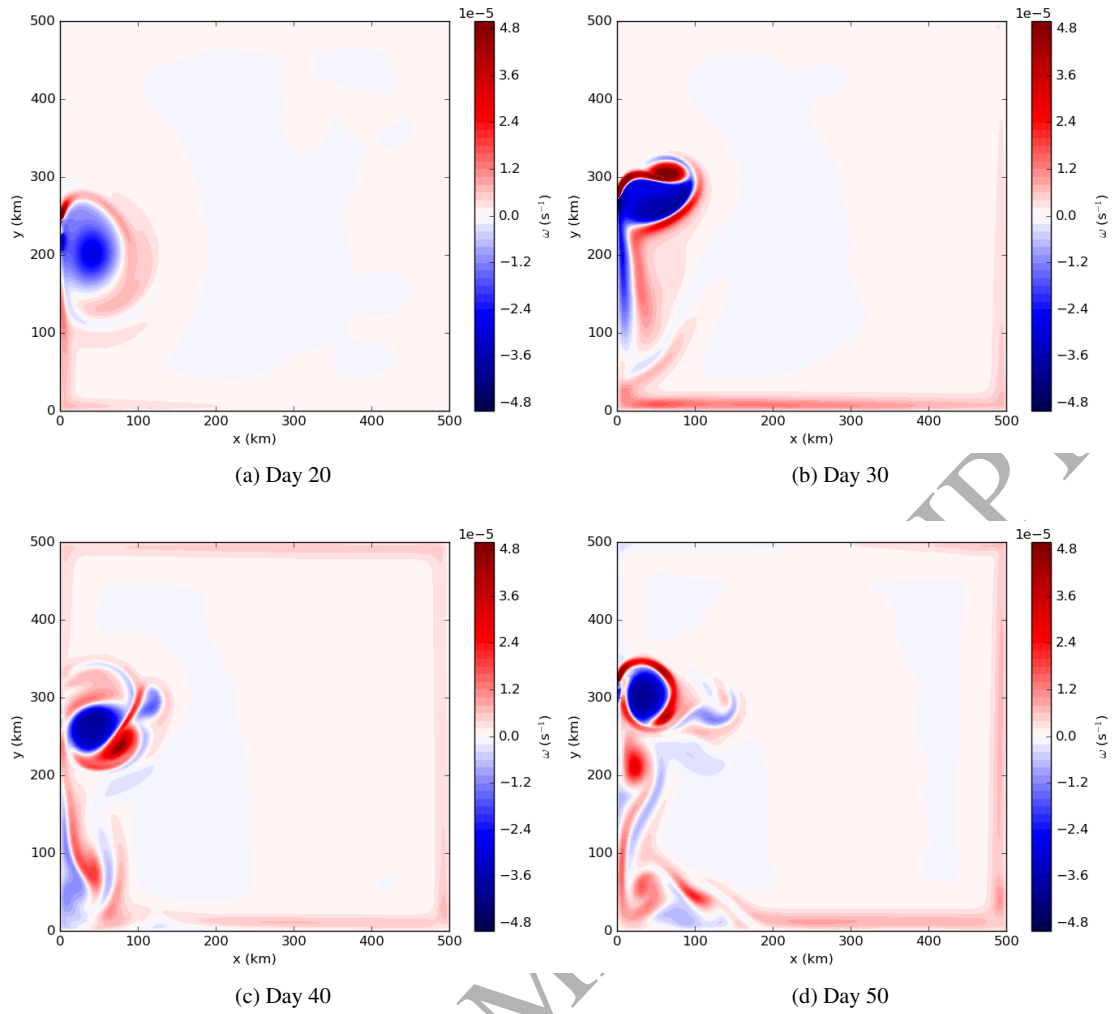


FIG. 3: Snapshots of the surface relative vorticity at days 20, 30, 40 and 50 (moving clockwise from the upper left) from GOLD.

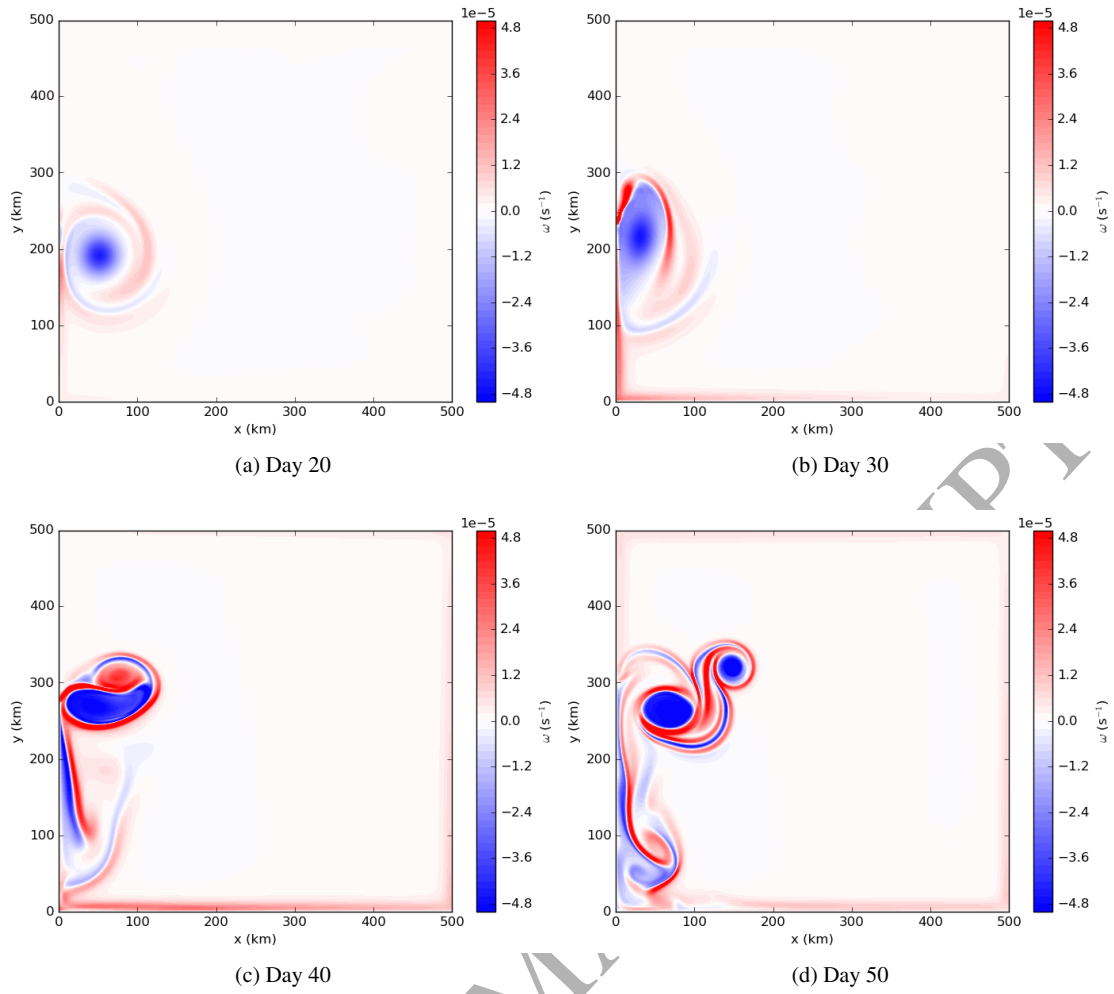


FIG. 4: Snapshots of the surface relative vorticity at days 20, 30, 40 and 50 for the MITgcm

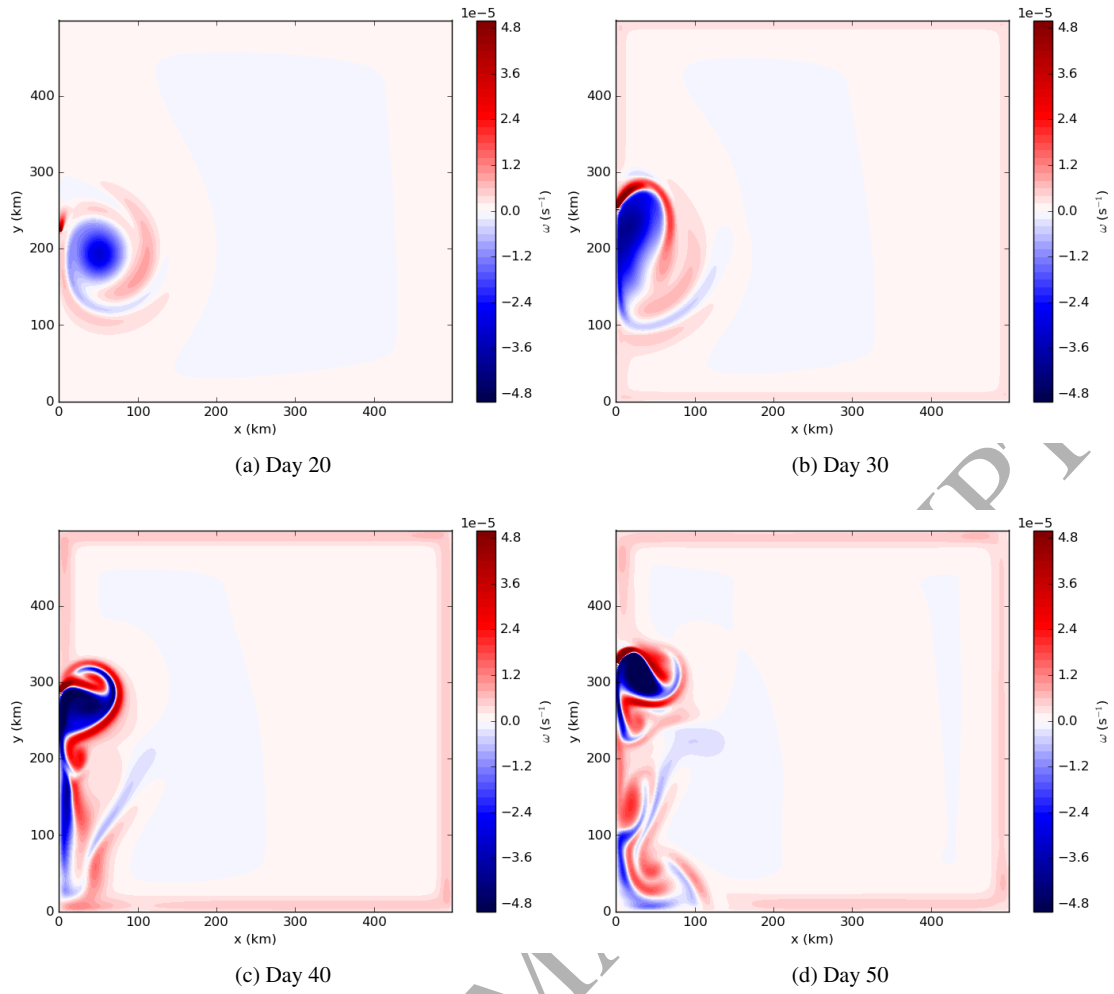


FIG. 5: Snapshots of the surface relative vorticity at days 20, 30, 40 and 50 for the Q-GCM

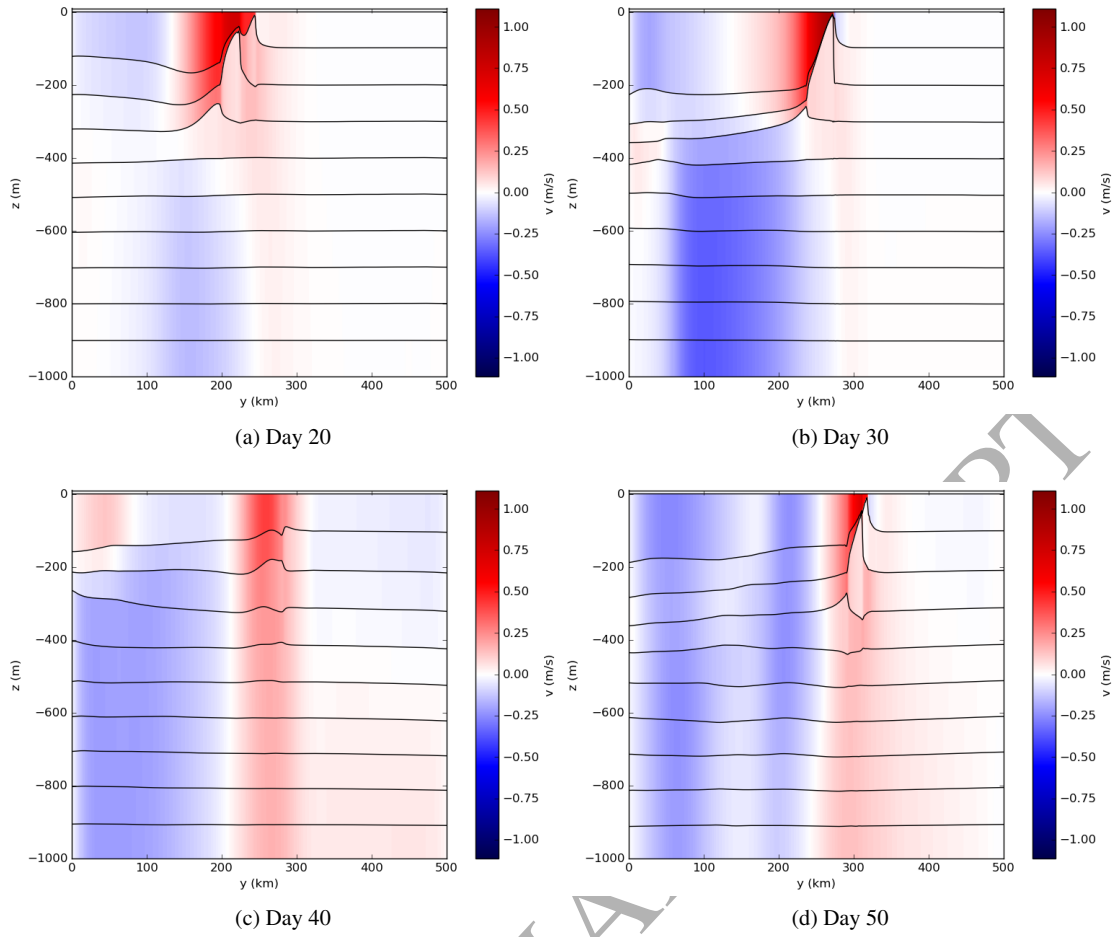


FIG. 6: Snapshots of the along wall velocity (color) and interface displacement (contours) days 20, 30, 40 and 50 for GOLD

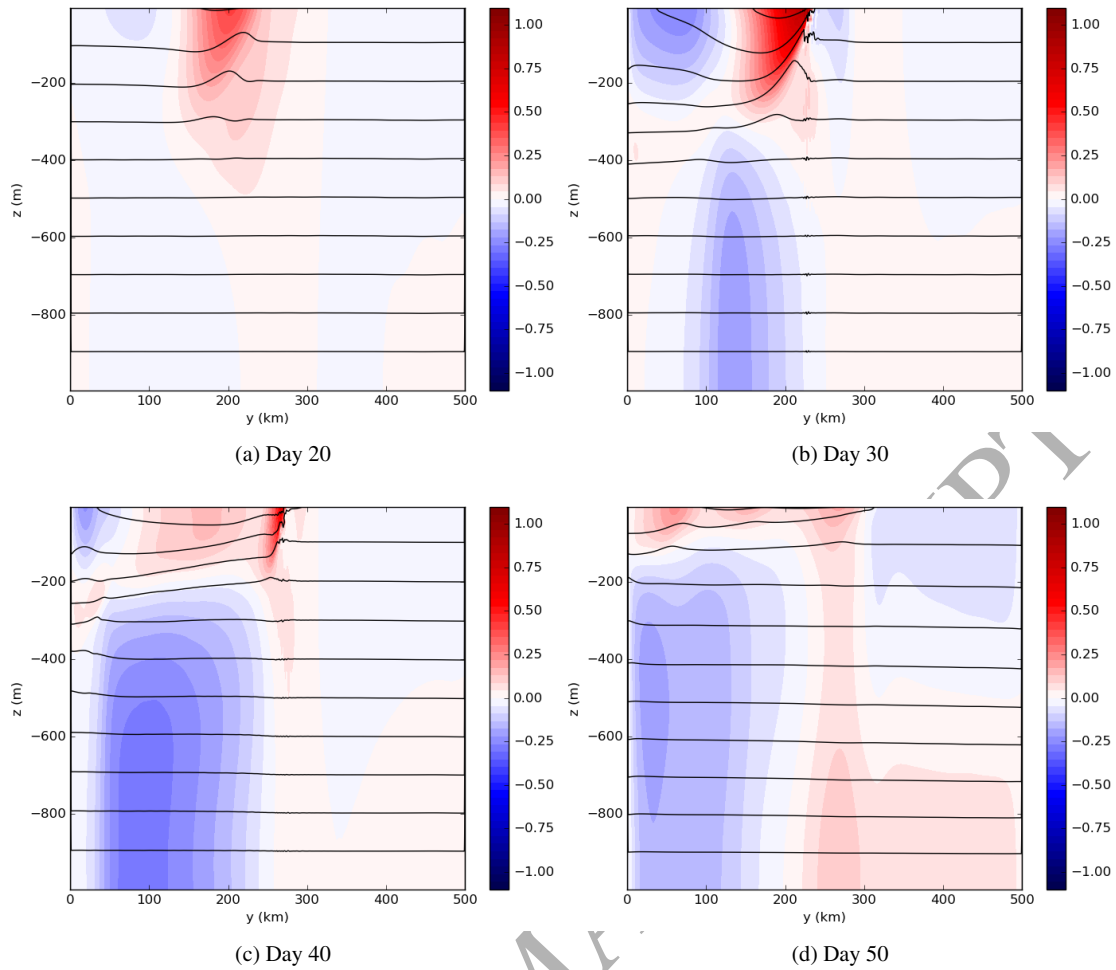


FIG. 7: Snapshots of the along wall velocity (color) and temperature (contours; contour interval = 0.5 K) days 20, 30, 40 and 50 for the MITgcm.

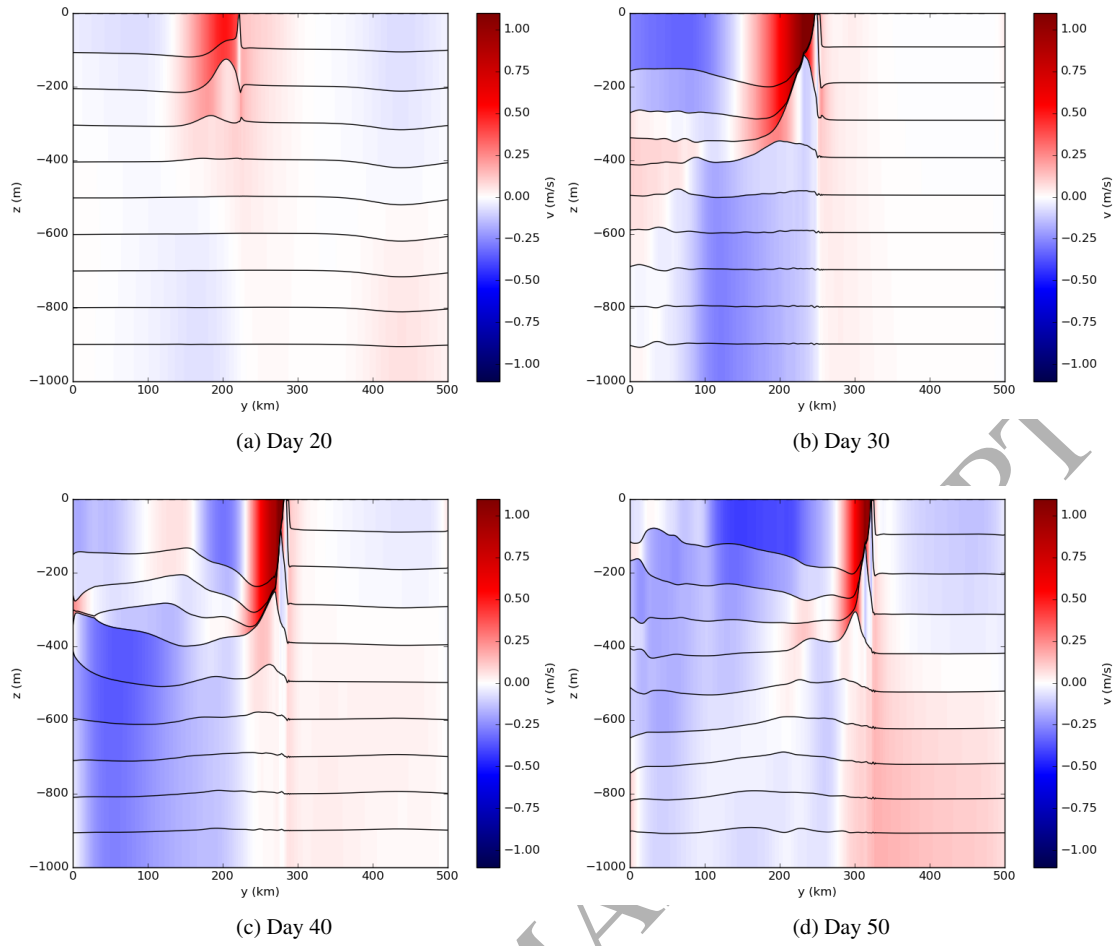


FIG. 8: Snapshots of the along wall velocity (color) and interface displacement (contours) days 20, 30, 40 and 50 for the Q-GCM coupled to the wall equation.

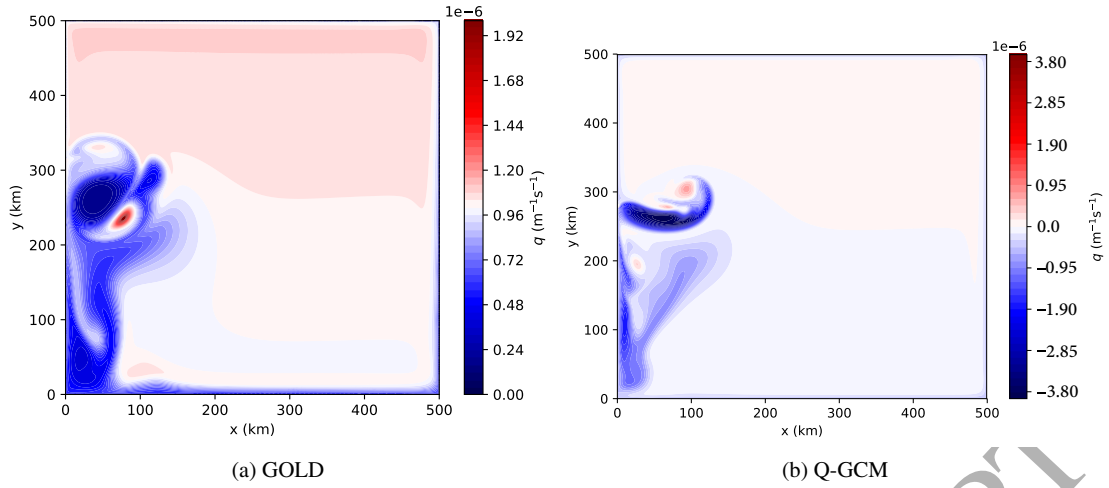


FIG. 9: Potential vorticity fields at Day 40 from GOLD and Q-GCM. Regions of positive potential vorticity coincide with regions of cyclonic vorticity; other regions of cyclonic vorticity are invisible in pv. This is consistent with our theory.

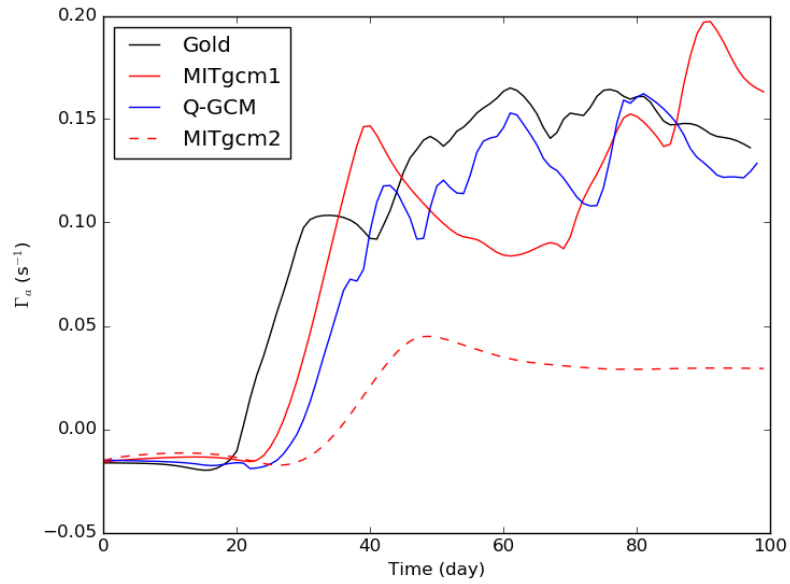


FIG. 10: Time series of the relative vorticity in the upper layer in the 3 configurations. We also added the curve for MITgcm with  $\nu = 50 \text{ m}^2 \text{ s}^{-1}$ .



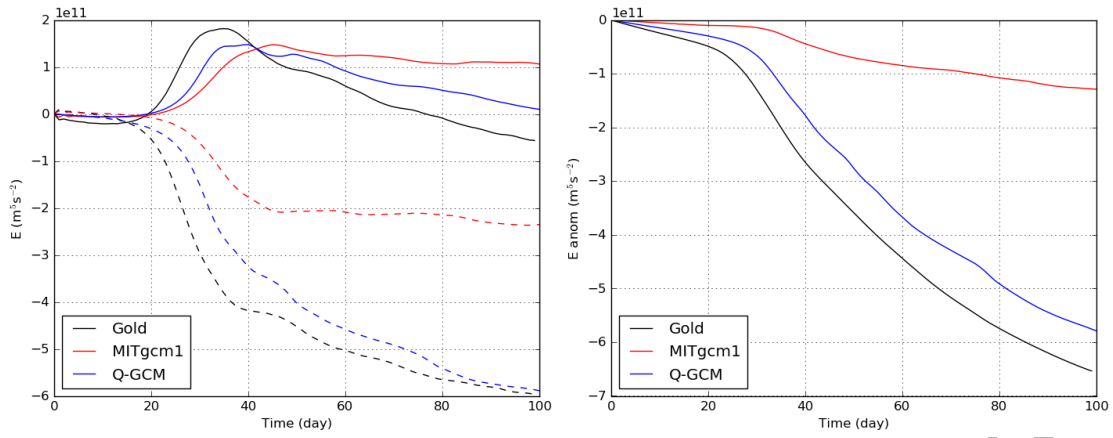


FIG. 11: (left) Time series of the kinetic (solid) and potential (dashed) energy anomalies in the three models. (right) Time series of the total energy from the three model runs.

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