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# Real Time Non-Invasive Hemodynamic Assessment of Ventricular Tachycardia

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**ABSTRACT** Hemodynamically unstable ventricular tachycardia (VT) is a critical cardiac arrhythmia associated with hemodynamic compromise that requires immediate cardioversion to prevent sudden cardiac death. Since unnecessary cardioverter defibrillators shocks damage the heart and increase the risk of mortality, the discrimination between unstable (i.e. requiring cardioversion) and stable (i.e. not requiring cardioversion) VT is of paramount importance. The aim of this study was to propose and assess non-invasive identification of hemodynamically unstable VT using photoplethysmography (PPG). Seventy-five ( $n = 75$ ) episodes of VT were recorded in 14 patients undergoing invasive electrophysiological studies for VT catheter ablation. Invasive continuous arterial blood pressure (ABP), PPG and electrocardiogram (ECG) were simultaneously recorded. VTs were classified as unstable if during the first 10 seconds from onset, the mean ABP ( $\bar{P}_{VT} < 60P_{VT}$ ) was  $\bar{P}_{VT} < 60P_{VT} < 60$  mmHg or if  $P_{VT}$  dropped more than 30% with respect to a 10 seconds baseline (i.e. ratio  $R_{ABP} < 0.70$ ). Five PPG morphological features were derived and compared to the heart rate from the ECG. PPG markers detected hemodynamically unstable VT with accuracy as high as 86% and were more accurate than the heart rate. The mean absolute slope was the best PPG parameter for classification of  $\bar{P}_{VT} < 60P_{VT} < 60P_{VT} < 60$  mmHg (AUC = 0.85, Sensitivity = 72%, Specificity = 86%) and  $R_{ABP} < 0.70$  ( $R_{ABP} < 0.70$ ) (AUC = 0.90, Sensitivity = 83%, Specificity = 89%) and it was automatically selected in the best two-variables logistic regression, for which AUC = 0.94. In conclusion, PPG analysis can accurately identify haemodynamically unstable VTs and has potential to enable optimization of VT therapy and reduce unnecessary and harmful cardioversion shocks.

**INDEX TERMS** Assistive technology, biomedical signal processing, cardiology.

## I. INTRODUCTION

Ventricular tachycardia (VT) is a critical arrhythmia that in some circumstances can become life threatening. The condition manifests itself through consecutive rapid contractions dissociated from normal sinus rhythm and it can dramatically reduce cardiac output. The degree of danger associated with VT depends on its impact on arterial blood pressure (ABP), i.e. on its haemodynamic stability. Hemodynamically unstable VT is associated with abrupt ABP loss that can prevent oxygen and nutrients from circulating, therefore threatening vital organs function. Contrary to hemodynamically

stable VT, which does not dramatically impact ABP, unstable VT requires immediate cardioversion to prevent sudden cardiac death.

Implantable cardioverter defibrillators (ICD) are capable of stopping life-threatening ventricular arrhythmias by delivering electrical shocks to the heart and are becoming mainstream (hundreds of thousands are implanted every year worldwide). Although potentially life-saving, defibrillator shocks damage the heart and increase the risk of death [1]–[4]. Therefore, reducing the number of unnecessary ICD shocks by specifically targeting unstable VT is a critical aspect for improving VT patients' care. In current practice, ICDs are programmed to deliver a shock when the heart rate increases above a pre-determined threshold,

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without taking into consideration ABP. Automatic identification of unstable VT remains however challenging, as no fixed relationship exists between heart rate and ABP during VT [5].

The photoplethysmogram (PPG) is a non-invasive optical signal measured in many wearable devices capable of providing real-time cardiac and haemodynamic information. We therefore hypothesised that PPG could be used to enable detection of hemodynamically unstable VT. The methodology presented in this study uses PPG features recorded before and at the onset of VT to classify its hemodynamic response. While previous studies have focused on improving alarm detection (including cardiac arrhythmia) in intensive care using PPG data [6] and others have classified ventricular arrhythmias based on electrocardiographic (ECG) features [7], non-invasive identification of unstable VT by means of PPG is novel. We envisage this study as a first step towards a new approach with the potential of improving clinical management of millions of patients relying on ICD therapy to stop life-threatening VTs.

## II. METHODS

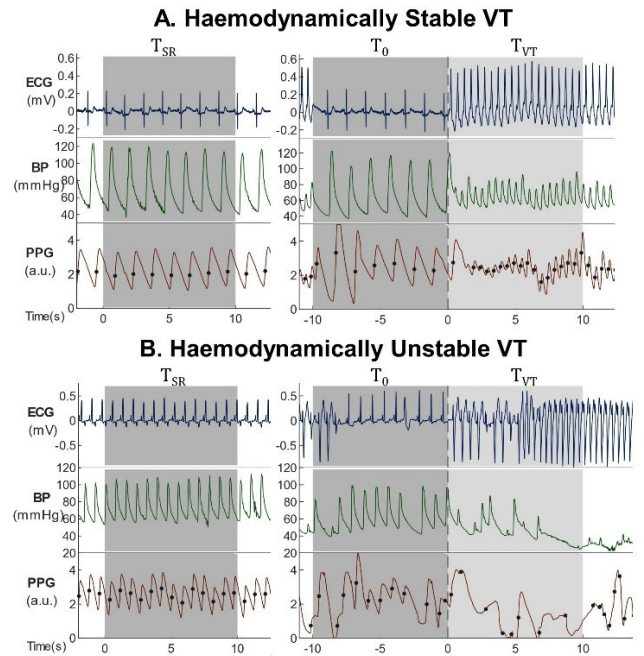
### A. DATA SETS AND PRE-PROCESSING

Twenty-two ( $n = 22$ ) patients undergoing catheter ablation of VT in the Catheterization Lab were prospectively recruited at the Barts Heart Centre, London, UK. ECG, invasive arterial blood pressure and PPG were simultaneously measured with sampling frequency of 240 Hz (Mac-Lab System, General Electric). Fourteen ( $n = 14$ ) patients, out of the 22, exhibited VT and were included in the study. Their background is presented in supplementary Table S.I. PPG was recorded from the middle finger of the left hand. Signals were exported bypassing the patient monitor auto-gain filters. ABP and PPG signals were filtered with a finite impulse response (FIR) low pass filter of 30 Hz cut-off frequency and order 120. A 100 Hz low pass filter was applied to the ECG waveform. Data were collected as part of a Barts Heart Centre ethically approved study of VT ablation and patients gave informed consent.

In some patients, ventricular pacing (cycle length equal to  $423 \pm 32$  ms, range 410-870 ms) was established to induce VT and 4 patients were studied while in slow incessant monomorphic stable ventricular tachycardia.

### B. DATA ANALYSIS

The onset of each VT was time-stamped ( $t_0$ ) and invasive ABP, PPG and ECG were evaluated in 3 windows (see Fig. 1): (A) From 10 s before to the onset of VT ( $T_0 : t_0 - 10s < t < t_0$ ); (B) From the onset of VT to 10 s after it ( $T_{VT} : t_0 \leq t < t_0 + 10s$ ); (3) Earliest 10 second interval preceding the VT onset,  $t_0$ , showing either normal sinus rhythm or baseline atrial pacing ( $T_{SR}$ ). This additional reference window was considered because in some cases  $T_0$  presented irregular rhythm due to ectopics or standard pacing maneuvers utilized to induce VT.



**FIGURE 1.** Recordings of ECG, invasive blood pressure (ABP) and non-invasive PPG during hemodynamically stable (A) and unstable (B) VTs, within 3 10-second windows: Sinus rhythm preceding VT ( $T_{SR}$ ), any cardiac rhythm immediately before VT onset ( $T_0$ ) and VT ( $T_{VT}$ ).

#### 1) ARTERIAL BLOOD PRESSURE AND DEFINITION OF UNSTABLE VT

Mean ABP was used to evaluate the hemodynamic response to VT. This is standard practice and more reliable than using measurements based on systolic blood pressure, since during fast VT it is not always possible to clearly distinguish blood pressure pulses. Hemodynamically unstable VTs were identified as those characterized by either (A) mean ABP during  $T_{VT}$  lower than 60 mmHg, i.e.  $\overline{P_{VT}} < 60$  mmHg, where  $\overline{P_{VT}} = \text{mean}_{t=T_{VT}}(x_{ABP}(t))$ , with  $x_{ABP}(t)$  representing continuous blood pressure, or by (B) a drop in mean ABP during VT higher than 30% from baseline mean ABP, i.e.  $R_{ABP}^{T_0} = \overline{P_{VT}} / \overline{P_{T_0}} < 0.70$  or  $R_{ABP}^{T_{SR}} = \overline{P_{VT}} / \overline{P_{T_{SR}}} < 0.7$ , with baseline taken at  $T_0$  and  $T_{SR}$ , respectively. These definitions are supported by previous studies and were adopted before data analysis [8], [9].

#### 2) HEART RATE FROM ECG

The heart rate was estimated from the time-frequency (TF) distribution of the ECG waveform. The signal was down-sampled to 20 Hz and the TF spectrum was calculated using the quadratic distribution described in [10], [11]. The heart rate during  $T_0$ ,  $T_{VT}$  and  $T_{SR}$  was measured as the temporal mean of the instantaneous frequencies,  $f_0(t)$ , identified as the highest spectral peak of the TF distribution. Only values above 40 bpm were considered as being valid heart rates.

#### 3) PPG PARAMETERS

Five PPG metrics based on the PPG signal,  $V(t)$ , were defined to indirectly assess hemodynamics during VT. All of them

were expressed as the ratio between the metric's value during  $T_{VT}$  and baseline values obtained either during  $T_0$  or  $T_{SR}$ .

1.  $R_A^{T_0}$  and  $R_A^{TSR}$ : Ratio between the mean pulse amplitude during VT and baseline, where the pulse amplitude was measured from foot to peak for each pulse within  $T_{VT}$ ,  $T_0$  and  $T_{SR}$ .
2.  $R_{MS}^{T_0}$  and  $R_{MS}^{TSR}$ : Ratio between the pulse maximum slope during VT and baseline. The pulse maximum slope was measured as the temporal mean of the maximum of the first derivative of each pulse:  $\overline{V'_M} = \frac{1}{N} \cdot \sum_n V'_M[n]$ , where  $n = 1, \dots, N$  is a heartbeat and  $V'_M[n]$  is the maximum of the first derivative measured during the pulse's upslope,  $V'_M = \max(dV(t)/dt)$ .
3.  $R_{MAS}^{T_0}$  and  $R_{MAS}^{TSR}$ : Ratio between the mean absolute slope during VT and baseline. The mean absolute slope was measured as the temporal mean of the absolute value of the first derivative of the PPG signal,  $|V'| = \text{mean}_T \left| \frac{dV(t)}{dt} \right|$ .
4.  $R_{PR}^{T_0}$  and  $R_{PR}^{TSR}$ : Ratio between the pulse rate during VT and baseline. The pulse rate was measured as the barycentre of the power spectrum of  $V(t)$  estimated using the Fourier transform of the PPG signal within the windows of interest  $T_{VT}$ ,  $T_0$  and  $T_{SR}$ .
5.  $R_{IP}^{T_0}$  and  $R_{IP}^{TSR}$ : Ratio between the average instantaneous power of  $V(t)$  during VT and baseline. The average instantaneous power was measured as  $\text{mean}_T \left( \int_{f_0(t)-B_L}^{f_0(t)+B_H} S(t, f) df \right)$ , where  $f_0(t)$  is the instantaneous frequency of the highest spectral peak,  $(B_L - B_H)$  are the boundaries of the time-varying spectral band where the instantaneous power is estimated and  $S(t, f)$  is the TF distribution described in [10], [12].  $B_L$  and  $B_H$  were set at  $\pm 10$  bpm within baseline windows  $T_0$  and  $T_{SR}$  and at  $-10$  to  $+70$  bpm within the VT window  $T_{VT}$ .

Of note,  $R_A$  and  $R_{MS}$  are the only metrics to require PPG peaks detection, which during some VTs can be challenging due to the loss of the pulsatile components in the PPG signal (see Fig. 1B).

#### 4) SENSITIVITY ANALYSIS

Sensitivity analyses were conducted to assess the impact of choosing different thresholds for the definition of unstable VTs (see Section II.B1) and varying the duration of windows  $T_{VT}$ ,  $T_0$  and  $T_{SR}$  from 5 to 15 seconds.

#### C. STATISTICAL ANALYSIS

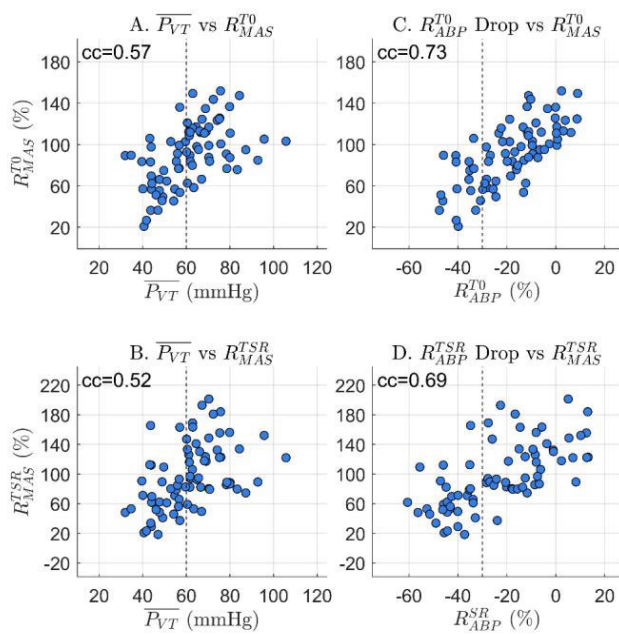
Distributions of data are presented as mean  $\pm$  standard deviation, unless otherwise specified. Correlation between ABP and PPG parameters was measured using the Spearman's correlation coefficient. Differences between PPG and ECG parameters during hemodynamically stable vs unstable VTs were assessed using the Wilcoxon rank-sum test using a threshold for statistical significance equal to  $0.05/N$ , where  $N = 23$  represents the number of pair-wise comparisons (see Table 1).

TABLE 1.

(A)	$\overline{P_{VT}} < 60$	$\overline{P_{VT}} > 60$	P	cc
$R_A^{T_0}$	0.55 $\pm$ 0.25	0.71 $\pm$ 0.15	<b>2.65E-04</b>	0.36
$R_{MS}^{T_0}$	0.53 $\pm$ 0.25	0.75 $\pm$ 0.15	<b>3.42E-06</b>	0.54
$R_{MAS}^{T_0}$	0.70 $\pm$ 0.26	1.06 $\pm$ 0.23	<b>2.36E-07</b>	0.57
$R_{PR}^{T_0}$	0.49 $\pm$ 0.35	0.80 $\pm$ 0.30	<b>1.34E-04</b>	0.42
$R_{IP}^{T_0}$	0.98 $\pm$ 0.06	1.02 $\pm$ 0.04	3.06E-03	0.30
$R_A^{TSR}$	0.49 $\pm$ 0.22	0.70 $\pm$ 0.13	<b>2.93E-06</b>	0.52
$R_{MS}^{TSR}$	0.51 $\pm$ 0.28	0.77 $\pm$ 0.16	<b>1.82E-06</b>	0.54
$R_{MAS}^{TSR}$	0.70 $\pm$ 0.36	1.18 $\pm$ 0.38	<b>9.04E-07</b>	0.52
$R_{PR}^{TSR}$	0.48 $\pm$ 0.41	0.95 $\pm$ 0.46	<b>1.62E-05</b>	0.48
$R_{IP}^{TSR}$	0.16 $\pm$ 0.16	0.39 $\pm$ 0.20	<b>7.26E-07</b>	0.58
$HR_{VT}$	155 $\pm$ 25	132 $\pm$ 24	<b>5.17E-04</b>	-0.45
(B1)	$R_{ABP}^{T_0} < 0.7$	$R_{ABP}^{T_0} > 0.7$	P	cc
$R_A^{T_0}$	0.49 $\pm$ 0.28	0.68 $\pm$ 0.17	<b>6.79E-04</b>	0.44
$R_{MS}^{T_0}$	0.43 $\pm$ 0.17	0.72 $\pm$ 0.19	<b>3.52E-06</b>	0.61
$R_{MAS}^{T_0}$	0.61 $\pm$ 0.25	0.99 $\pm$ 0.26	<b>8.17E-06</b>	0.73
$R_{PR}^{T_0}$	0.40 $\pm$ 0.33	0.75 $\pm$ 0.32	<b>3.18E-04</b>	0.55
$R_{IP}^{T_0}$	0.96 $\pm$ 0.07	1.01 $\pm$ 0.04	8.97E-03	0.39
$HR_{VT}$	166 $\pm$ 25	135 $\pm$ 23	<b>7.43E-05</b>	-0.6
(B2)	$R_{ABP}^{TSR} < 0.7$	$R_{ABP}^{TSR} > 0.7$	P	cc
$R_A^{TSR}$	0.49 $\pm$ 0.20	0.69 $\pm$ 0.16	<b>5.43E-06</b>	0.52
$R_{MS}^{TSR}$	0.50 $\pm$ 0.28	0.76 $\pm$ 0.17	<b>1.30E-06</b>	0.62
$R_{MAS}^{TSR}$	0.64 $\pm$ 0.31	1.19 $\pm$ 0.37	<b>8.47E-09</b>	0.69
$R_{PR}^{TSR}$	0.43 $\pm$ 0.37	0.97 $\pm$ 0.45	<b>7.10E-07</b>	0.6
$R_{IP}^{TSR}$	0.14 $\pm$ 0.13	0.39 $\pm$ 0.20	<b>5.50E-08</b>	0.64
$HR_{VT}$	159 $\pm$ 23	131 $\pm$ 23	<b>1.30E-05</b>	-0.54

Mean and standard deviation of PPG and ECG parameters in hemodynamically stable and unstable VTs, P-value of their differences and correlation coefficients, cc, with invasive blood pressure parameters ( $P_{VT}$  in A,  $R_{ABP}^{T_0}$  in B1 and  $R_{ABP}^{TSR}$  in B2).  $P < 2.17E-03$  (Bonferroni corrected threshold) are reported in bold.

Binary classification of stable and unstable VTs was assessed using receiver operating curves (ROC), from which the area under the curve (AUC), sensitivity and specificity were measured. For each parameter, the threshold providing best accuracy was defined as that associated with the ROC point closest to the upper left corner (Sensitivity = Specificity = 100%). Given that the number of events was relatively small ( $n = 75$ ), AUC, sensitivity and specificity were first estimated using all events as both training and test set. However, to assess possible overestimation due to overfitting, classification assessment was then repeated by randomly splitting all events into a training test composed of 80% of events, and an independent test set composed of the remaining 20%. The optimum threshold was estimated from the training set and used to assess sensitivity and specificity in the independent test set. This process was repeated 10 times and results are reported as mean  $\pm$  standard deviation.



**FIGURE 2.** Correlation between invasive blood pressure (ABP) features (mean ABP during VT,  $\overline{P_{VT}}$ , ABP reduction during VT with respect to baseline,  $R_{ABP}^{T_0}$  and  $R_{ABP}^{TSR}$ ) and PPG features (ratio of mean absolute slope during VT with respect to baseline,  $R_{MAS}^{T_0}$  and  $R_{MAS}^{TSR}$ ). Correlation coefficient (cc) is shown within each panel.

Least absolute shrinkage and selection operator (LASSO) models were used to identify the best pair of features for classification. Logistic regressions utilizing the selected pair of parameters were used for classification and assessed as described before, i.e. both using all data for training and test and then using 80% of data for training and 20% for testing.

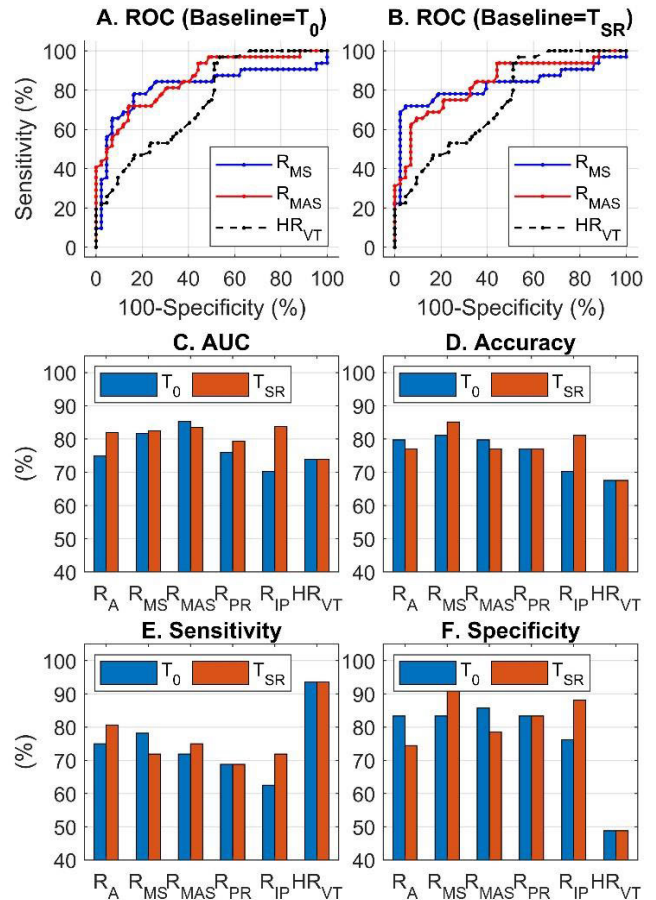
### III. RESULTS

Fourteen patients exhibited at least one VT episode and a total of 75 VTs were analysed. Table 1 reports the distribution of parameters within stable and unstable VT groups, the P-value of their differences and the correlation coefficient between PPG and ABP parameters. Boxplots providing a graphical representation of these results are shown in Supplementary Fig. S.1-2. Fig. 2 illustrates the relation between ABP changes and PPG mean absolute slope for all VT episodes. Table 2 reports results of the binary classification including AUC, optimum threshold, accuracy, sensitivity and specificity estimated within the entire data-set and using separate training and test sets.

#### A. IDENTIFICATION OF UNSTABLE VT

VT episodes were classified as hemodynamically stable or unstable based on two criteria: A) Mean ABP during VT lower than 60 mmHg ( $\overline{P_{VT}} < 60$  mmHg) and B) Drop of ABP larger than 30% with respect to baseline ( $R_{ABP}^{T_0} < 0.70$  or  $R_{ABP}^{TSR} < 0.70$  if baseline was taken at  $T_0$  or  $T_{SR}$ , respectively).

Thirty-two ( $n = 32$ , 42.7%) of VTs showed  $\overline{P_{VT}} < 60$  mmHg. The heart rate was higher during unstable



**FIGURE 3.** Classification of stable vs unstable VT based on mean blood pressure during the first 10 sec of VT. ROCs show classification results for the heart rate from the ECG ( $HR_{VT}$ ) and 2 of the best PPG features ( $R_{MS}$  and  $R_{MAS}$ ) using either  $T_0$  (A) or  $T_{SR}$  (B) as baseline. Panels C-F show the area under the curve (AUC), accuracy, sensitivity and specificity for all features measured using  $T_0$  (blue) or  $T_{SR}$  (red) as baseline.

than stable VTs ( $HR_{VT} = 155 \pm 25$  bpm vs  $132 \pm 24$  bpm,  $P = 5.2 \cdot 10^{-4}$ ). All PPG parameters except  $R_{IP}^{T_0}$  were significantly lower ( $P < 2.17E-03$ ) during unstable than stable VTs (see Table IIA). Among PPG parameters,  $R_{MAS}^{T_0}$  and  $R_{MAS}^{TSR}$  showed the highest correlation with  $\overline{P_{VT}}$ ,  $cc = 0.57$  and  $cc = 0.52$ , respectively (Fig. 2A-B).

Classification of unstable VTs ( $\overline{P_{VT}} < 60$  mmHg) using heart rate from the ECG was moderately accurate, with  $AUC = 0.74$ , high sensitivity (94%) but low specificity (49%). Classification was more accurate using PPG parameters, with  $R_{MS}^{T_0}$  and  $R_{MAS}^{T_0}$  providing the best results within parameters requiring and not-requiring PPG pulse detection, respectively. For these indices, AUC was  $>0.80$  and accuracy was  $>80\%$ , with specificity slightly higher than sensitivity. Results, including ROC curves, are summarized in Fig. 3.

Analysis performed using separate training and test data-sets showed similar results (Table 2 A).

Seventeen ( $n = 17$ , 23%) VTs showed  $R_{ABP}^{T_0} < 0.70$  and were considered hemodynamically unstable using this definition. As shown in Table IB, the heart rate correlated

TABLE 2. VT Classification using uni-variable models.

A. Mean ABP during VT < 60 mmHg													
REF	PRED	SIG	PD	AUC	THR	ACC	SENS	SPEC	AUC	THR	ACC	SENS	SPEC
$\overline{P_{VT}} < 60$	$R_A^{T0}$	PPG	Y	75	0.63	80	75	83	74±2.6	0.63±0.00	85±9	84±13	86±9.8
$\overline{P_{VT}} < 60$	$R_A^{TSR}$	PPG	Y	82	0.62	77	81	74	82±1.7	0.61±0.02	71±10	72±29	67±13
$\overline{P_{VT}} < 60$	$R_{MS}^{T0}$	PPG	Y	82	0.65	81	78	83	81±1.5	0.65±0.02	80±6	79±16	80±14
$\overline{P_{VT}} < 60$	$R_{MS}^{TSR}$	PPG	Y	83	0.58	85	72	95	82±1.8	0.63±0.04	76±11	68±27	76±13
$\overline{P_{VT}} < 60$	$R_{MAS}^{T0}$	PPG	N	85	0.84	80	72	86	85±2.1	0.84±0.00	80±9.4	76±14	84±11
$\overline{P_{VT}} < 60$	$R_{MAS}^{TSR}$	PPG	N	84	0.86	77	75	79	83±1.8	0.84±0.03	75±6.7	76±15	74±10
$\overline{P_{VT}} < 60$	$R_{PR}^{T0}$	PPG	N	76	0.52	77	69	83	76±2.2	0.56±0.07	76±8	76±10	76±14
$\overline{P_{VT}} < 60$	$R_{PR}^{TSR}$	PPG	N	79	0.53	77	69	83	80±1.8	0.53±0.02	71±8.5	68±19	74±6.8
$\overline{P_{VT}} < 60$	$R_{IP}^{T0}$	PPG	N	78	0.52	77	72	81	80±3.1	0.49±0.03	76±8	63±21	87±12
$\overline{P_{VT}} < 60$	$R_{IP}^{TSR}$	PPG	N	84	0.18	81	72	88	84±1.7	0.19±0.01	77±10	72±17	79±12
$\overline{P_{VT}} < 60$	$HR_{VT}$	ECG	-	74	128	68	94	49	74±2.7	133±10	61±8.1	72±28	51±18
B. Drop of ABP > 30%													
REF	PRED	SIG	PD	AUC	THR	ACC	SENS	SPEC	AUC	THR	ACC	SENS	SPEC
$R_{ABP}^{T0} < 0.7$	$R_A^{T0}$	PPG	Y	77	0.59	78	76	79	80±4.3	0.60±0.02	71±9.9	67±31	71±14
$R_{ABP}^{TSR} < 0.7$	$R_A^{TSR}$	PPG	Y	81	0.62	78	86	73	81±2.6	0.61±0.01	77±6.8	71±22	81±14
$R_{ABP}^{T0} < 0.7$	$R_{MS}^{T0}$	PPG	Y	87	0.57	82	82	82	87±1.9	0.58±0.02	77±7.4	80±29	75±11
$R_{ABP}^{TSR} < 0.7$	$R_{MS}^{TSR}$	PPG	Y	83	0.66	80	80	80	82±3.1	0.65±0.02	84±6.8	80±18	86±9.1
$R_{ABP}^{T0} < 0.7$	$R_{MAS}^{T0}$	PPG	N	86	0.84	77	82	75	86±2.1	0.84±0.00	76±9.5	70±24	77±11
$R_{ABP}^{TSR} < 0.7$	$R_{MAS}^{TSR}$	PPG	N	90	0.82	86	83	89	89±2.1	0.82±0.00	87±6.7	86±11	87±8.9
$R_{ABP}^{T0} < 0.7$	$R_{PR}^{T0}$	PPG	N	79	0.52	73	76	72	80±3.8	0.51±0.02	69±8.0	63±30	70±13
$R_{ABP}^{TSR} < 0.7$	$R_{PR}^{TSR}$	PPG	N	84	0.53	80	73	84	83±2.3	0.50±0.04	83±8.5	67±23	92±11
$R_{ABP}^{T0} < 0.7$	$R_{IP}^{T0}$	PPG	N	84	0.40	82	76	84	84±3.8	0.41±0.02	79±7.2	83±30	78±7
$R_{ABP}^{TSR} < 0.7$	$R_{IP}^{TSR}$	PPG	N	87	0.18	84	77	89	87±1.9	0.19±0.01	82±6.0	80±16	84±12
$R_{ABP}^{T0} < 0.7$	$HR_{VT}$	ECG	-	82	149	76	76	75	81±2.2	150±5.0	71±7.3	72±22	70±8.7
$R_{ABP}^{TSR} < 0.7$	$HR_{VT}$	ECG	-	80	149	77	67	84	80±1.8	148±1.7	71±9.3	63±10	78±15

Classification of hemodynamically unstable VTs based on its definition (REF) using the parameter (PRED); Results are obtained using all events for training and testing (left) or using 80% of events for training and 20% for testing (right, results reported as mean and standard deviation over 10 iterations). SIG: type of signal, either PPG or ECG; PD: Pulse detection required; AUC: Area under the ROC; THR: Threshold for best accuracy; ACC: Accuracy; SENS: Sensitivity; SPEC: Specificity.

only moderately to  $R_{ABP}^{T0}$  ( $cc = 0.6$ ) and it was significantly higher in VTs characterized by sudden and significant ABP drop ( $R_{ABP}^{T0} < 0.70$ ) than for the rest of VTs. All PPG parameters except  $R_{IP}^{T0}$  were significantly lower during VTs characterized by sudden and significant ABP drop than during the rest of VTs (Table 1B).  $R_{MAS}^{T0}$  showed the highest correlation coefficient with  $R_{ABP}^{T0}$  at  $cc = 0.73$  (Table 1B). Classification was more accurate using PPG parameters than heart rate from the ECG, with  $R_{MS}^{T0}$  and  $R_{MAS}^{T0}$  providing the best results within parameters requiring and not-requiring PPG pulse detection, respectively. For these indices,  $AUC \geq 0.82$  and accuracy was  $\geq 77\%$ , with similar specificity and sensitivity. Results, including ROC curves, are summarized in Supplementary Fig. S.3. Analysis performed using separate training and test data-sets or that used  $T_{SR}$  as baseline window showed similar results (Table 2B).

B. SENSITIVITY ANALYSES

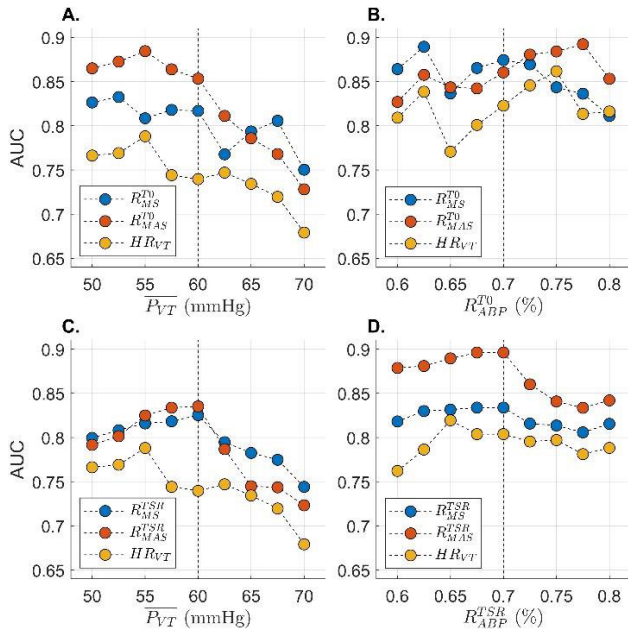
Sensitivity analyses were conducted to explore how the use of different parameters affected the accuracy of stable vs unstable VT classification.

1) IMPACT OF ARBITRARY THRESHOLDS FOR UNSTABLE VTs Data and statistical analysis were repeated for different thresholds, with unstable VTs identified as those for which  $\overline{P_{VT}} < X$ , with  $50 < X < 70$  mmHg or  $R_{ABP}^{T0}$  and  $R_{ABP}^{TSR} < X$ , with  $0.60 < X < 0.80$ . Prevalence of unstable VT varied between 27% and 72% in the first case and between 11% and 56% in the second case. Fig. 4 shows AUC of  $HR_{VT}$ ,  $R_{MAS}$  and  $R_{MS}$  as a function of the threshold used to identify unstable VTs based on mean ABP and ABP drop. AUC remained high for all configurations, and tended to slightly increase for thresholds that made unstable VT more severe

**TABLE 3.** VT Classification using lasso to identify the best pair of pre.

REF	PRED	AUC	ACC	SENS	SPEC	AUC	ACC	SENS	SPEC
$\overline{P_{VT}} < 60$	$R_{MAS}^{T0}; HR_{VT}$	87	84	84	84	86±2.0	83±7.2	83±15.9	86±8.4
$\overline{P_{VT}} < 60$	$R_{MAS}^{TSR}; R_A^{TSR}$	85	81	81	81	83±1.9	84±11.4	91±14.4	78±19.0
$R_{ABP}^{T0} < 0.7$	$R_{MAS}^{T0}; R_{MS}^{T0}$	89	83	82	83	88±2.3	82±8.3	84±21.7	82±11.6
$R_{ABP}^{TSR} < 0.7$	$R_{MAS}^{TSR}; HR_{VT}$	94	91	87	93	94±1.6	85±9.3	82±16.8	88±14.7

Results for the best 2-variables logistic regressions selected using the LASSO method. See Table II for details.



**FIGURE 4.** Classification using the heart rate from the ECG ( $HR_{VT}$ ) and 2 of the best PPG features ( $R_{MS}$  and  $R_{MAS}$ ) for different thresholds defining stable and unstable VTs based on invasive blood pressure. Panels show the area under the ROC (AUC) for unstable VTs defined by mean arterial blood pressure (ABP) lower than a threshold ranging from 50 to 70 mmHg, i.e.  $50 < \overline{P_{VT}} < 70$  mmHg (A and C), and for a reduction of ABP during VT with respect to baseline windows  $T_0$  (B) or  $T_{SR}$  (D) ranging from 60% to 80%, i.e.  $60\% < R_{ABP}^{T0} < 80\%$  and  $60\% < R_{ABP}^{TSR} < 80\%$ .

and less frequent (e.g.  $\overline{P_{VT}} < 55$  mmHg). Of note, AUC remained higher for PPG markers  $R_{MAS}$  and  $R_{MS}$  than for heart rate in all configurations.

## 2) IMPACT OF USING DIFFERENT WINDOW LENGTHS

Data and statistical analysis were repeated after modifying the duration of  $T_{VT}$ ,  $T_0$  and  $T_{SR}$  from 5 s to 15 s. The results (Supplementary Tables S.II-III) show that this did not significantly impacted on the accuracy of stable and unstable VTs classification.

## C. COMBINING PARAMETERS FOR MULTIPLE REGRESSIONS

The pairs of parameters providing the best classification of VTs showing  $\overline{P_{VT}} < 60$ ,  $R_{ABP}^{T0} < 0.7$  and  $R_{ABP}^{TSR} < 0.7$  are shown in Table 3. In all cases,  $R_{MAS}$  was retained as one of

the two best features. Classifications improved with respect to single-variable models, with AUC ranging from 0.85 for the detection of  $\overline{P_{VT}} < 60$  mmHg using  $(R_{MAS}^{TSR}; R_A^{TSR})$  to 0.94 for the detection of  $R_{ABP}^{TSR} < 0.7$  using  $(R_{MAS}^{TSR}; HR_{VT})$ . Results obtained using a separate test sets confirmed high sensitivity and specificity for all multi-variables logistic regressions (Table 3).

## IV. DISCUSSION

This study investigates for the first time the use of PPG markers to identify VTs characterized by hemodynamic compromise within 10 sec from its onset, a critical aspect for improving therapy in patients at risk of sudden cardiac death. The main findings are: (1) PPG markers can detect hemodynamically unstable VTs with accuracy as high as 86%; (2) Detection of unstable VTs was more accurate using PPG parameters than the heart rate measured from the ECG, independently of the specific ABP threshold or definition of unstable VTs. (3) The combination of PPG markers and heart rate improved accuracy, suggesting that PPG provides complementary information to the ECG. (4) Accurate pulse detection in the PPG is not necessary to accurately detect unstable VTs.

The hemodynamic response to VTs (i.e. stable vs unstable) was characterized both in terms of mean ABP and sudden changes in mean ABP. Results show that PPG parameters can detect both accurately. All PPG markers were expressed as a ratio between a given PPG feature measured during the first 10 sec of VT and during a baseline interval, which was defined either as the 10 sec preceding the VT onset independent of the heart rhythm ( $T_0$ ), or as the earliest 10 sec of sinus rhythm preceding VT ( $T_{SR}$ ). The rationale for establishing this second baseline window was that VT is sometimes preceded by runs of ectopic beats. Additionally, in this study, some VTs were induced by ventricular pacing that can potentially affect both ABP and PPG. Results obtained using these different baseline windows were similar, which suggests that any interval preceding VT can serve as baseline, even in presence of irregular rhythm.

The heart rate measured during VT, which represents the standard parameter utilized to programme ICDs and prevent sudden cardiac death, was found to only moderately correlate with mean ABP ( $cc = -0.45$ ) or sudden drop in mean ABP ( $cc = -0.60$ ). While this is not surprising (ABP critically depends on cardiac function/contractility), it confirms the

need for a better estimator of the hemodynamic response to VT. The PPG parameter  $R_{MAS}$  showed the highest correlation with mean ABP ( $cc = 0.57$ ) and sudden drop in mean ABP ( $cc = 0.73$ ) during VT, and one of the best accuracy in classifying unstable and stable VTs ( $AUC \leq 0.85$ ). Furthermore,  $R_{MAS}$  is easy to estimate as it does not require PPG pulse detection. This makes it one of the most promising parameters for further clinical validation.

Previous studies have proposed algorithms to reduce false alarms in critical care [6], [13], with some of them including ventricular tachycardia. Another study has demonstrated high accuracy in discriminating between VT and ventricular fibrillation and between ICD shocked and non-shocked rhythms using features based on Taylor-Fourier analysis of the ECG [7]. The present study differs in many aspects as it focused for the first time on the challenge of non-invasively discriminating haemodynamically unstable VTs from haemodynamically stable VTs, it uses simultaneous invasive blood pressure recordings instead of surrogate parameters (e.g. ICD shocks) as a reference, and it focused on PPG features. Electromechanical coupling analysis has been recently used with success [14] to discriminate ventricular fibrillation from sinus rhythm or artefacts using used two laser doppler flowmetry light probes, one at the heart and the other at the finger. Compared to PPG, this laser doppler is a complex and expensive technology that uses coherent light to measure perfusion, which limits the application to in-clinic use.

In this study, we have focused on PPG, because, in contrast with cardiac signals such as the ECG, it offers an insight into hemodynamic cardiovascular changes. It functions by illuminating arterially perfused tissue within light in the visible and infra-red spectrum and recording the reflected tissue light. As an estimator of blood pressure, PPG has been limited by calibration requirements, and has been shown to perform well only in some patients [15], [16]. Interestingly, PPG had already been shown potential to detect hypotensive events during haemodialysis and labour [17], [18], but it was never been utilized to classify the hemodynamic response to VT. We have recently shown that PPG features can be used to detect mechanical (or pulsus) alternans [19], [20]. Combined with the present results, this suggests that although PPG may not be accurate in measuring ABP, it can be used to detect fast and sudden changes in ABP though the analysis of its pulsatile components.

#### A. CLINICAL RELEVANCE AND FUTURE APPLICATIONS

PPG sensors are commonly utilized for measuring oxygen saturation and are ubiquitous in clinics. In recent years, they have been increasingly incorporated in wearable health tracking devices (e.g. smart watches) that can provide a platform for improved individualized treatment. We envisage that future wearable/implanted devices could be used in combination with ICDs to enable a precise assessment of the hemodynamic response to VT, thus withholding unnecessary shock therapy and extending patient life expectancy. Combining

ICD detected electrograms or surface ECG for rates below the standard VT zone rate cut-offs would also enable more accurate arrhythmia classification for determining therapy delivery in certain cases for slower VTs which can represent as significant challenge. Furthermore, PPG could be used to indirectly estimate respiratory rate [21]–[23], heart rate variability [24], mechanical alternans [19], [20] and other physiological markers to monitor cardiac risk and modulate ICD therapy (e.g. by preventively using anti-tachycardia pacing to prevent VTs). Cardiac risk assessment traditionally based on ECG parameters could be further benefit from the inclusion of ECG parameters. [25]–[28].

#### B. LIMITATIONS

The main limitation of the study was that data were recorded during electrophysiological studies. While this provides the unique opportunity to measure ABP, ECG and PPG during VT safely and in a controlled environment, the recording condition with the patients in supine position and the PPG measured at the finger with minimal movement differ from those in which the methodology is eventually intended to be used. Further study should address robustness against noise and movement artefacts. Furthermore, thresholds for obtaining the most accurate classification was performed by optimizing both sensitivity and specificity. While this is the standard approach, in a clinical scenario a high specificity at maximum sensitivity (no false negative) may be preferred. Finally, in this study the ECG was only used to derive the heart rate, because this is the standard parameter used to programme ICDs. Further studies may include ECG features derived with advanced methods [7].

#### V. CONCLUSION

This work has shown for the first time that PPG features can accurately classify hemodynamically stable and unstable VTs defined using simultaneous invasive recordings of arterial blood pressure. This may have potential clinical implications as reducing the number of unnecessary ICD shocks by specifically targeting unstable VT is a critical aspect of improving VT patients' care.

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