# Optimizing Time and Space MIMO Antenna System for Frequency Selective Fading Channels

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Abstract—Smart or adaptive antennas promise to provide significant increases in system capacity and performance in wireless communication systems. In this paper, we investigate the use of adaptive antennas at the base and mobile stations, operating jointly, to maximize the average signal-to-interference and noise ratio (SINR) of each packet in the system for frequency selective channels with prior knowledge of the channel at the transmitter. Our approach is based on deriving an analytic formula for the average packet SINR and using the Lagrange multiplier method to determine an optimum. We derive necessary conditions for an optimum solution and propose an analytical expression for the optimum. Our analytical expression is not guaranteed to be the global optimum but it does satisfy the derived necessary conditions and, in addition for frequency flat channels, our results reduce to expressions for optimal weights previously published. To demonstrate the potential of the proposed system, we provide Monte Carlo simulation results of the system bit-error rates and make comparisons with other adaptive antenna systems. These show that significant improvements in performance are possible in a wireless communications context.

*Index Terms*—Co-channel interference, flat and frequency selective fading channels, intersymbol interference, MIMO, smart antennas, wireless communication systems.

# I. INTRODUCTION

TUTURE WIRELESS COMMUNICATION systems are expected to support a wide range of services that will require high transmission rates of several megabits per second. Communicating at these high transmission rates over wireless channels with a limited spectrum implies that an increase in the capacity of current wireless systems will need to be achieved [1]–[4].

One possible approach to increase system capacity is through the use of smart or adaptive antennas. Several smart antenna systems have been proposed, and demonstrated at the base station (BS) of the wireless communication system, and these have shown that significant increases in capacity are possible [5]–[8]. Further increases in capacity may be possible by including smart antennas at the mobile station (MS) in both the down and uplinks as well. Although this may not be practical for current mobile

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stations, reductions in antenna sizes and also the use of notebook computers in wireless computing applications may make this feasible in the future [9]. Therefore, it is worthwhile investigating the use of smart antennas at the MSs and BSs operating jointly and determine whether the increased performance justifies the increased system complexity. We refer to this type of system as a smart base and smart mobile (SBM) antenna system.

Recently, systems similar to SBM have been considered by several authors and they have utilized space time coding in multiple-input multiple-output (MIMO) channels [10], [11] or joint transmitter receiver systems [12]-[19]. In [10], Foschini proposed the combined array processing and symbol cancellation approach for obtaining high capacity in MIMO antenna system while Raleigh and Cioffi [11] studied space-time water-filling for multipath fading, with prior knowledge of the channel at the transmitter. In [12]-[14], the capacity of the system is maximized under flat fading channel conditions without co-channel interference (CCI). In [15], the signal-to-noise ratio (SNR) is maximized by using a joint multiple transmission and reception filter system. However, an equalizer is required to mitigate the effect of intersymbol interference (ISI) and CCI is not considered. Results on joint transmitter and receiver optimization appeared in [16] and [17], and are based on a frequency domain analysis. In [18] and [19], smart antennas at the BS and MS which jointly maximize signal-to-interference and noise ratio (SINR) for flat Rayleigh fading channels in the presence of CCI are studied. In addition, [20] and [21] provide interesting results for joint optimization for the case of additive white Gaussian noise (AWGN) and where antenna arrays at the transmitter and receiver are utilized. However overall, the optimization problem (in the sense of maximizing the SINR) for frequency selective fading channels has not been considered.

In this paper and in contrast to the previous work, a solution to the broader problem of performance optimization for multipath frequency selective fading channels in the presence of interference is provided using a discrete time channel model. We consider smart antennas jointly at the BS and MS to suppress ISI together with CCI. The paper provides a useful extension of [12]–[20].

Our approach is based on deriving an analytic expression for the average SINR of each packet with the constraint of fixed transmitter power. The Lagrange multiplier method is then utilized for finding an optimal solution. Several solutions are found which satisfy the Lagrange conditions for a maximum and we select the optimum of these to form an analytic solution. Although this solution is not guaranteed to be the global optimum, it reduces to the global optimum for flat fading channels and performs better [in terms of average bit-error rate (BER)] than

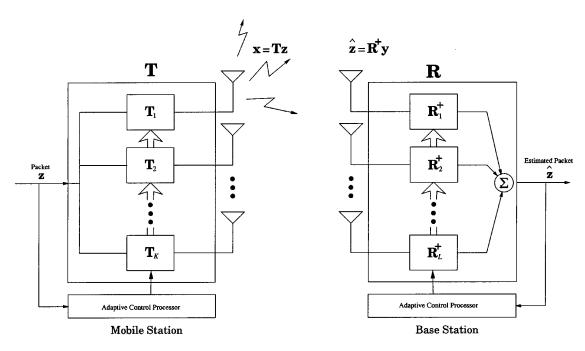


Fig. 1. System configuration demonstrating the uplink in which smart antennas are included at both BS and MS in the down and uplinks.

other techniques in numerical simulations for frequency selective fading channels. It is also shown that under the assumption of orthogonal transmit weights, the solution is the optimum in the sense of maximizing average SINR. Throughout, we utilize quaternary phase-shift keying (QPSK) modulation in an environment with ISI, AWGN, and CCI in a similar way to that described in [22].

This paper is organized as follows. In Section II, we introduce some necessary notation that is used throughout the paper. Section III derives analytical expressions for the optimal antenna weights for SBM in frequency selective and nonselective fading environments with CCI. Section IV presents simulation setup and results and we have some discussion in Section V concerning practical issues. Finally, we make some concluding remarks in Section VI.

## II. SYSTEM MODEL

The configuration of the SBM system is shown in Fig. 1 where K antennas are located at the MS and L antennas are located at the BS. A time division multiple access (TDMA)-based transmission system is assumed and data is transmitted in blocks of symbols of length N and the number of spatial subchannels (symbols or spatial dimensions) per sample is denoted by  $n_s$ . Therefore, the total number of symbols sent per packet is  $M \triangleq Nn_s$  and this is written in packet form as  $\mathbf{z} = [z_1 \ z_2 \ \cdots \ z_M]^T$  where the superscript T denotes the transpose operation. The input vector  $\mathbf{z}$  is assumed to have independent identically distributed components. The packet is multiplied by a  $N \times M$  transmission matrix

$$\mathbf{T}_{k} = \begin{bmatrix} t_{1,1}^{(k)} & t_{1,2}^{(k)} & \dots & t_{1,M}^{(k)} \\ t_{2,1}^{(k)} & t_{2,2}^{(k)} & & \vdots \\ \vdots & & \ddots & \vdots \\ t_{N,1}^{(k)} & \dots & & t_{N,M}^{(k)} \end{bmatrix}$$
(1)

to produce a packet  $\mathbf{x}_k = \mathbf{T}_k \mathbf{z}$  which is transmitted by the kth antenna.

At the BS, L antennas are used for reception and the channel between the  $\ell$ th BS antenna and kth MS antenna is assumed quasistationary and can be considered as time-invariant over a packet, so that it can be characterized by a Toeplitz matrix

$$\mathbf{H}_{\ell,k} = \begin{bmatrix} h_0^{(\ell,k)} & 0 & 0 & \dots & 0 \\ h_1^{(\ell,k)} & h_0^{(\ell,k)} & 0 & \dots & 0 \\ \vdots & \ddots & \ddots & \ddots & \vdots \\ h_{\nu}^{(\ell,k)} & & \ddots & h_0^{(\ell,k)} \\ 0 & \ddots & & \ddots & 0 \\ \vdots & & & \ddots & h_0^{(\ell,k)} \\ 0 & & & & h_1^{(\ell,k)} \\ \vdots & & & \ddots & \ddots & \vdots \\ 0 & & & & 0 & h_1^{(\ell,k)} \end{bmatrix}$$
(2)

where the received packet is given by  $\mathbf{y}_{\ell} = \sum_{k=1}^{K} \mathbf{H}_{\ell,k} \mathbf{x}_{k}$ . The maximum delay is assumed to last for  $\nu$  samples and the discrete-time channel gains are defined by an q-ray model and this is discussed in the simulations in Section IV.

Following Fig. 1, the received packet  $y_\ell$  is then weighted in space and time by a matrix  $R_\ell^\dagger$  where

$$\mathbf{R}_{\ell} = \begin{bmatrix} r_{1,1}^{(\ell)} & r_{1,2}^{(\ell)} & \dots & r_{1,M}^{(\ell)} \\ r_{2,1}^{(\ell)} & r_{2,2}^{(\ell)} & & \vdots \\ \vdots & & \ddots & \\ r_{N+\nu,1}^{(\ell)} & \dots & & r_{N+\nu,M}^{(\ell)} \end{bmatrix}$$
(3)

and the superscript  $\dagger$  denotes the conjugate transpose operation. The weighted packets are finally combined to produce an estimate  $\hat{\mathbf{z}}$  of the original packets. Writing the packet transmitted

from all K antennas as  $\mathbf{x} = [\mathbf{x}_1; \mathbf{x}_2; \dots; \mathbf{x}_K]^T$  and the received data by all L antennas as  $\mathbf{y} = [\mathbf{y}_1; \mathbf{y}_2; \dots; \mathbf{y}_L]^T$ , we can write the entire MIMO system as

$$y = Hx + n \tag{4}$$

where  $\mathbf{n} = [n_1 \ n_2 \ \dots \ n_{L(N+\nu)}]^T$  is the noise vector and is assumed to be AWGN with power  $\sigma_n^2$ . Likewise,  $\mathbf{H}$  is given by

$$\mathbf{H} = \begin{bmatrix} \mathbf{H}_{1,1} & \mathbf{H}_{1,2} & \dots & \mathbf{H}_{1,K} \\ \mathbf{H}_{2,1} & \mathbf{H}_{2,2} & \dots & \mathbf{H}_{2,K} \\ \vdots & & \ddots & \vdots \\ \mathbf{H}_{L,1} & \dots & & \mathbf{H}_{L,K} \end{bmatrix}$$
(5)

where  $\mathbf{H}_{\ell,k}$  is defined in (2). The overall system can, therefore, be written as

$$\hat{\mathbf{z}} = \mathbf{R}^{\dagger} \mathbf{H} \mathbf{T} \mathbf{z} + \mathbf{R}^{\dagger} \mathbf{n} \tag{6}$$

where  $\mathbf{R} \stackrel{\triangle}{=} [\mathbf{R}_1; \mathbf{R}_2; \dots; \mathbf{R}_L] \in C^{(N+\nu)L \times M}$  and  $\mathbf{T} \stackrel{\triangle}{=} [\mathbf{T}_1; \mathbf{T}_2; \dots; \mathbf{T}_K] \in C^{NK \times M}$ .

Interference is also considered and P interferers are assumed. For now, we consider the uplink only. However, the formulation for the downlink will be similar, but with generally different CCI. The interfering channel matrix from the pth interferer  $\tilde{\mathbf{H}}_p$  is defined similar to (5), and the transmitted signal vector from the pth interferer  $\tilde{\mathbf{x}}_p$  is also defined similar to  $\mathbf{x}$ . The signal vectors  $\{\tilde{\mathbf{x}}_p\}$  are assumed to be uncorrelated with themselves and  $\mathbf{z}$ . In addition, the receiver employs perfect timing and the interfering signals are time-aligned with the desired signal. As a result,  $\hat{\mathbf{z}}$  is then given by

$$\hat{\mathbf{z}} = \mathbf{R}^{\dagger} \left( \mathbf{H} \mathbf{T} \mathbf{z} + \sum_{p=1}^{P} \tilde{\mathbf{H}}_{p} \tilde{\mathbf{x}}_{p} + \mathbf{n} \right)$$

$$\equiv \mathbf{\Lambda} \mathbf{z} + \mathbf{R}^{\dagger} \left( \sum_{p=1}^{P} \tilde{\mathbf{H}}_{p} \tilde{\mathbf{x}}_{p} + \mathbf{n} \right)$$

$$\equiv \mathbf{\Lambda}_{\text{diag}} \mathbf{z} + \mathbf{\Lambda}_{\text{off}} \mathbf{z} + \mathbf{R}^{\dagger} \left( \sum_{p=1}^{P} \tilde{\mathbf{H}}_{p} \tilde{\mathbf{x}}_{p} + \mathbf{n} \right)$$
(7)

where  $\mathbf{R}^{\dagger}\mathbf{HT} \stackrel{\triangle}{=} \mathbf{\Lambda}$  and  $\lambda_{i,j}$  are elements of  $\mathbf{\Lambda}, \mathbf{\Lambda}_{\mathrm{diag}} = \mathrm{diag}(\lambda_{i,i})$ , and  $\mathbf{\Lambda}_{\mathrm{off}} = \mathbf{\Lambda} - \mathbf{\Lambda}_{\mathrm{diag}}$  which contains all the off diagonal elements. Hence, in (7), the first term represents the desired signal, the second term represents the ISI of the desired signal, and the third term is the CCI and noise.

### III. OPTIMAL SBM SOLUTION

Using the system model described in Section II, our objective is to find the mobile (transmit) and base (receive) matrices  $(\mathbf{T},\mathbf{R})$  that maximize the average SINR of the packet with the constraint of a fixed transmit power (the norm of each column vector of  $\mathbf{T}$  is  $\sqrt{P_T}$ ). We note that both  $\mathbf{T}$  and  $\mathbf{R}$  are arbitrary and do not necessarily have orthogonal columns (or equivalently, are not necessarily unitary when NK=M). By allowing solution weights with nonorthogonal columns, we allow the possibility of improved performance under a wider range of conditions than would otherwise occur with weights with orthogonal columns.

Our overall objective can then be written as

$$(\mathbf{T}, \mathbf{R})_{\text{opt}} = \arg \max_{\substack{\mathbf{T}, \mathbf{R} \\ ||\mathbf{t}_i|| = \sqrt{P_T} \ \forall i}} \{\text{SINR}\}$$
(8)

where  $\mathbf{t}_i \in C^{NK}$  is the *i*th column vector of  $\mathbf{T}$  and the average SINR of the packet is defined as

SINR 
$$\stackrel{\triangle}{=} \frac{1}{M} \sum_{i=1}^{M} \gamma_i$$

$$\equiv \frac{1}{M} \sum_{i=1}^{M} \left( \frac{|\lambda_{i,i}|^2 \sigma_z^2}{\sum_{\substack{j=1\\j \neq i}}^{M} |\lambda_{i,j}|^2 \sigma_z^2 + \mathbf{r}_i^{\dagger} \mathbf{\Phi} \mathbf{r}_i} \right) \tag{9}$$

where  $\gamma_i$  is the *i*th symbol SINR,  $\mathbf{r}_i$  is the *i*th column vector of  $\mathbf{R}, E[\mathbf{z}\mathbf{z}^{\dagger}] = \sigma_z^2\mathbf{I}$  and

$$\mathbf{\Phi} = E \left[ \left( \sum_{p=1}^{P} \tilde{\mathbf{H}}_{p} \tilde{\mathbf{x}}_{p} + \mathbf{n} \right) \left( \sum_{p=1}^{P} \tilde{\mathbf{H}}_{p} \tilde{\mathbf{x}}_{p} + \mathbf{n} \right)^{\dagger} \right]$$

$$= \sum_{p=1}^{P} \tilde{\mathbf{H}}_{p} E[\tilde{\mathbf{x}}_{p} \tilde{\mathbf{x}}_{p}^{\dagger}] \tilde{\mathbf{H}}_{p}^{\dagger} + \sigma_{n}^{2} \mathbf{I}.$$
(10)

To find the receive weight matrix that maximizes (9), we first rewrite the SINR expression as

SINR = 
$$\frac{1}{M} \sum_{i=1}^{M} \left\{ \frac{\mathbf{r}_{i}^{\dagger}(\mathbf{H}\mathbf{t}_{i})(\mathbf{H}\mathbf{t}_{i})^{\dagger}\mathbf{r}_{i}\sigma_{z}^{2}}{\mathbf{r}_{i}^{\dagger} \left[ \sum_{\substack{j=1\\j\neq i}}^{M} (\mathbf{H}\mathbf{t}_{j})(\mathbf{H}\mathbf{t}_{j})^{\dagger}\sigma_{z}^{2} + \mathbf{\Phi} \right] \mathbf{r}_{i}} \right\}$$

$$= \frac{\sigma_{z}^{2}}{M} \sum_{i=1}^{M} \frac{\mathbf{r}_{i}^{\dagger} (\mathbf{H}\mathbf{t}_{i}) (\mathbf{H}\mathbf{t}_{i})^{\dagger} \mathbf{r}_{i}}{\mathbf{r}_{i}^{\dagger} \mathbf{\Theta}_{i} \mathbf{r}_{i}}$$
(11)

where

$$\mathbf{\Theta}_{i} \stackrel{\triangle}{=} \sum_{\substack{j=1\\ i \neq i}}^{M} (\mathbf{H} \mathbf{t}_{j}) (\mathbf{H} \mathbf{t}_{j})^{\dagger} \sigma_{z}^{2} + \mathbf{\Phi}.$$
 (12)

It is known [18] that the  $\mathbf{r}_i$  that maximizes (11) is

$$\mathbf{r}_i = \mu_i \mathbf{\Theta}_i^{-1} \mathbf{H} \mathbf{t}_i \tag{13}$$

where  $\mu_i$  is arbitrary and does not affect the SINR. Hence, to simplify our equations, we set  $\mu_i = 1$  for all i. Substituting (13) into (11), the SINR can be expressed as

$$SINR = \frac{\sigma_z^2}{M} \sum_{i=1}^{M} \mathbf{t}_i^{\dagger} \mathbf{H}^{\dagger} \mathbf{\Theta}_i^{-1} \mathbf{H} \mathbf{t}_i.$$
 (14)

We now wish to maximize (14) subject to the power constraint  $||\mathbf{t}_i||^2 = P_T \ \forall i$ . To make the analysis more succinct, we write  $\mathbf{T} = \mathbf{U}\mathbf{A}$  where  $\mathbf{A} = [\mathbf{a}_1 \ \mathbf{a}_2 \ \dots \ \mathbf{a}_M]$  is an arbitrary  $NK \times M$  matrix and  $\mathbf{U}$  is the matrix that contains all the eigenvectors of  $\mathbf{H}^{\dagger}\mathbf{\Phi}^{-1}\mathbf{H}$  so that  $\mathbf{H}^{\dagger}\mathbf{\Phi}^{-1}\mathbf{H} = \mathbf{U}\mathbf{D}\mathbf{U}^{\dagger}$ , where  $\mathbf{D} = \mathrm{diag}(\lambda_1, \dots, \lambda_{NK})$ . Based on the power constraint, it can be shown easily that  $\mathbf{a}_i$  must satisfy

$$\|\mathbf{a}_i\|^2 = P_T \quad \forall i. \tag{15}$$

To find the weights which maximize (14), subject to the constraint (15), we use the Lagrange multiplier method. Specifically

$$\mathcal{L} = \frac{\sigma_z^2}{M} \sum_{i=1}^M \mathbf{t}_i^{\dagger} \mathbf{H}^{\dagger} \mathbf{\Theta}_i^{-1} \mathbf{H} \mathbf{t}_i - \sum_{i=1}^M \eta_i (\mathbf{a}_i^{\dagger} \mathbf{a}_i - P_T)$$
 (16)

where  $\eta_i$  represents the Lagrange multipliers. Now, consider the derivative of  $\mathcal{L}$  with respect to the real and imaginary parts of  $\mathbf{a}_k$  for any k. We write this in a compact notation as

$$\Delta_{\mathbf{a}_{k}} \mathcal{L} \stackrel{\triangle}{=} \frac{\partial \mathcal{L}}{\partial \operatorname{Real}\{\mathbf{a}_{k}\}} + j \frac{\partial \mathcal{L}}{\partial \operatorname{Imag}\{\mathbf{a}_{k}\}}$$
(17)

and as a consequence, we have

$$\Delta_{\mathbf{a}_{k}} \mathcal{L} = \frac{\sigma_{z}^{2}}{M} \Delta_{\mathbf{a}_{k}} (\mathbf{t}_{k}^{\dagger} \mathbf{H}^{\dagger} \mathbf{\Theta}_{k}^{-1} \mathbf{H} \mathbf{t}_{k}) 
+ \frac{\sigma_{z}^{2}}{M} \sum_{\substack{i=1\\i\neq k}}^{M} \Delta_{\mathbf{a}_{k}} (\mathbf{t}_{i}^{\dagger} \mathbf{H}^{\dagger} \mathbf{\Theta}_{i}^{-1} \mathbf{H} \mathbf{t}_{i}) - 2\eta_{k} \mathbf{a}_{k}. \quad (18)$$

The optimum  $\mathbf{t}_k$  must satisfy  $\Delta_{\mathbf{a}_k} \mathcal{L} = 0 \ \forall k$ . Since the expression involves the gradients of inverse matrices, this is a nontrivial exercise and we rewrite the expression by defining the following matrices

$$\mathbf{\Theta}_{i}^{(n)} = \sum_{\substack{k=1\\k\neq i}}^{n} \sigma_{z}^{2}(\mathbf{H}\mathbf{t}_{k})(\mathbf{H}\mathbf{t}_{k})^{\dagger} + \mathbf{\Phi} \quad \forall n \neq i$$
 (19)

with  $\Theta_i^{(0)} = \Phi$ . Then using (53) in the Appendix recursively, we can write

$$\mathbf{t}_{i}^{\dagger}\mathbf{H}^{\dagger}\boldsymbol{\Theta}_{i}^{-1}\mathbf{H}\mathbf{t}_{i}$$

$$=\mathbf{t}_{i}^{\dagger}\mathbf{H}^{\dagger}\boldsymbol{\Phi}^{-1}\mathbf{H}\mathbf{t}_{i} - \sum_{\substack{\ell=1\\\ell\neq i}}^{M} \frac{\left|\mathbf{t}_{i}^{\dagger}\mathbf{H}^{\dagger}\boldsymbol{\Theta}_{i}^{(\ell-1)^{-1}}\mathbf{H}\mathbf{t}_{\ell}\right|^{2}}{\mathbf{t}_{\ell}^{\dagger}\mathbf{H}^{\dagger}\boldsymbol{\Theta}_{i}^{(\ell-1)^{-1}}\mathbf{H}\mathbf{t}_{\ell} + 1/\sigma_{z}^{2}}.$$
(20)

As a result, (18) can be expressed as

$$\Delta_{\mathbf{a}_{k}} \mathcal{L} = \frac{\sigma_{z}^{2}}{M} \sum_{i=1}^{M} \left[ \Delta_{\mathbf{a}_{k}}(\mathbf{a}_{i}^{\dagger} \mathbf{D} \mathbf{a}_{i}) - \sum_{\substack{\ell=1\\\ell \neq i}}^{M} \Delta_{\mathbf{a}_{k}} \left( \frac{\left| \mathbf{t}_{i}^{\dagger} \mathbf{H}^{\dagger} \mathbf{\Theta}_{i}^{(\ell-1)^{-1}} \mathbf{H} \mathbf{t}_{\ell} \right|^{2}}{\mathbf{t}_{\ell}^{\dagger} \mathbf{H}^{\dagger} \mathbf{\Theta}_{i}^{(\ell-1)^{-1}} \mathbf{H} \mathbf{t}_{\ell} + 1/\sigma_{z}^{2}} \right) \right] - 2m \cdot \mathbf{a}_{\ell}.$$
(21)

After setting  $\Delta_{\mathbf{a}_k} \mathcal{L} = 0$ , we have the system of simultaneous nonlinear equations

$$\frac{2\sigma_z^2}{M} \mathbf{D} \mathbf{a}_k - 2\eta_k \mathbf{a}_k \\
= \frac{\sigma_z^2}{M} \sum_{i=1}^M \sum_{\substack{\ell=1\\\ell \neq i}}^M \mathbf{\Delta}_{\mathbf{a}_k} \left( \frac{\left| \mathbf{t}_i^{\dagger} \mathbf{H}^{\dagger} \mathbf{\Theta}_i^{(\ell-1)^{-1}} \mathbf{H} \mathbf{t}_{\ell} \right|^2}{\mathbf{t}_{\ell}^{\dagger} \mathbf{H}^{\dagger} \mathbf{\Theta}_i^{(\ell-1)^{-1}} \mathbf{H} \mathbf{t}_{\ell} + 1/\sigma_z^2} \right).$$

The above equations do not allow an analytic solution to be found. However, it can be shown (see the Appendix) that the terms under the summation are eliminated by setting

$$\mathbf{t}_{i}^{\dagger}\mathbf{H}^{\dagger}\mathbf{\Phi}^{-1}\mathbf{H}\mathbf{t}_{j} = \mathbf{a}_{i}^{\dagger}\mathbf{D}\mathbf{a}_{j} = 0 \quad \forall i \neq j$$
 (23)

then (22) becomes

$$\frac{\sigma_z^2}{M} \mathbf{D} \mathbf{a}_k = \eta_k \mathbf{a}_k \quad \forall k. \tag{24}$$

The imposed condition (23) is desirable and it will be shown later that under the assumption of unitary (or orthogonal) transmit weights, our solution is the global optimal in the sense of maximizing average SINR.

To solve (24), we first note that the diagonal matrix  $\mathbf{D}$  has nonzero eigenvalues of which none are repetitive (since in general  $\mathbf{H}^{\dagger}\mathbf{\Phi}^{-1}\mathbf{H}$  is random and unlikely to have repetitive eigenvalues). By also realizing that  $||\mathbf{a}_k||^2 = P_T$  from (15), the solution for  $\mathbf{a}_k \ \forall k$  is

$$a_{k,j} = \begin{cases} \sqrt{P_T} & \text{if } j = \ell \\ 0 & \text{if } j \neq \ell \end{cases}$$
 (25)

for a given  $\ell$ , and  $\eta_k = \sigma_z^2 \lambda_\ell / M$ .

As a result, the transmit weight matrix is

$$\mathbf{T} = \sqrt{P_T} \mathbf{F}_M \tag{26}$$

where  $\mathbf{F}_M$  is a matrix that contains the eigenvectors that correspond to M distinct eigenvalues of  $\mathbf{H}^{\dagger}\mathbf{\Phi}^{-1}\mathbf{H}$ . In addition, the corresponding receive weight matrix  $\mathbf{R}$  is

$$\mathbf{R} = \mathbf{\Phi}^{-1} \mathbf{H} \mathbf{T} \tag{27}$$

where we have used (23). Using these weights, the overall SINR is

$$SINR = \frac{P_T \sigma_z^2}{M} \sum_{i=1}^{M} \lambda_i$$
 (28)

and the overall maximum SINR is achieved by selecting the eigenvectors corresponding to the M largest eigenvalues as the transmit weight matrix in (26).

The expressions (26) and (27) provide analytical expressions for the joint antenna weights at BS and MS. The combined effect of transmit and receive antenna weights is to perform space-time equalization and CCI suppression jointly at the BS and MS. In order to utilize them, we must know the channel  $\mathbf{H}$  and also the interference  $\boldsymbol{\Phi}$ . The practicality of this and its computational load are discussed in Section V-A.

In addition, the SBM solution reduces to previously known solutions for the flat fading case, as shown in Section III-A, and performs better than other techniques in frequency selective fading channels as shown in Section IV. It should also be noted that the solution is intuitively satisfying since it effectively sets all the transmit weights to be orthogonal to each other. It is also noted that the transmitter/receiver pair causes the channel to decompose into independent subchannels. Note, however, that examples can be found where weights with nonorthogonal columns provide higher SINR results than our suboptimum orthogonal column solution. This can occur, for example, when

interference does not play a dominant role in maximizing the overall SINR, and high noise conditions prevail. In this situation, improved SINR performance occurs if the weights combine the signals together to improve noise performance but at the expense of allowing some additional interference. Such tradeoffs can only occur if the weights are allowed to have nonorthogonal columns and further work needs to be performed to find the optimum solution in this situation.

We conclude this section by pointing out that if we begin with the assumption that T has orthogonal columns, then by using the inequality (50) on (14), we obtain an upper bound

SINR 
$$\leq \frac{\sigma_z^2 P_T}{M} \sum_{i=1}^{M} \mathbf{t}_i^{\dagger} \mathbf{H}^{\dagger} \mathbf{\Phi}^{-1} \mathbf{H} \mathbf{t}_i$$
  

$$= \frac{\sigma_z^2 P_T}{M} \operatorname{trace}_M(\mathbf{T}^{\dagger} \mathbf{H}^{\dagger} \mathbf{\Phi}^{-1} \mathbf{H} \mathbf{T})$$
(29)

where  $\mathrm{trace}_{M}(\cdot)$  denotes the summation of the M largest eigenvalues of the input matrix. Since trace is invariant by orthogonal transformation, we have

$$SINR \le \frac{\sigma_z^2 P_T}{M} \operatorname{trace}_M(\mathbf{H}^{\dagger} \mathbf{\Phi}^{-1} \mathbf{H})$$
 (30)

and now the upper bound is the same as the SINR (28) obtained by the SBM solution. Therefore, under the assumption of transmit weights with orthogonal columns (or equivalently unitary transmit weights when NK=M), the SBM solution is optimal in the sense of maximizing SINR.

#### A. Flat Fading

It is interesting to determine the form of (26) and (27) for flat fading and compare with those in [12]–[19]. In a flat fading radio environment, the mobile radio channel has a constant gain and linear phase response over a bandwidth that is greater than the bandwidth of the transmitted signal and, therefore, ISI is negligible. Hence, only  $h_0^{(\ell,k)}$  in (2) is significant and the received signal can be written as (7), but with

$$\mathbf{H}_{\ell,k} = h_0^{(\ell,k)} \mathbf{I} \tag{31}$$

where the identity matrix  ${\bf I}$  has dimensions  $M\times M$ . Consequently, the matrix  ${\bf H}^\dagger {\bf \Phi}^{-1} {\bf H}$  can be expressed as

$$\mathbf{H}^{\dagger} \mathbf{\Phi}^{-1} \mathbf{H} = \begin{bmatrix} a_{1,1} \mathbf{I} & a_{1,2} \mathbf{I} & \dots & a_{1,L} \mathbf{I} \\ a_{1,2}^* \mathbf{I} & a_{2,2} \mathbf{I} & \dots & \\ \vdots & & \ddots & \\ a_{1,L}^* \mathbf{I} & \dots & & a_{L,L} \mathbf{I} \end{bmatrix}$$
(32)

where the elements  $a_{i,j}$  are the corresponding elements of  $\mathcal{H}^{\dagger} \Psi^{-1} \mathcal{H}$  in which

$$\mathcal{H} = \begin{bmatrix} h_0^{(1,1)} & h_0^{(1,2)} & \dots & h_0^{(1,K)} \\ h_0^{(2,1)} & h_0^{(2,2)} & \dots & \\ \vdots & & \ddots & \\ h_0^{(L,1)} & \dots & & h_0^{(L,K)} \end{bmatrix}$$
(33)

and similarly  $\Psi$  can be defined by

$$\Psi = \sum_{p=1}^{P} \tilde{\mathbf{H}}_{p} E[\tilde{\mathbf{x}}_{p} \tilde{\mathbf{x}}_{p}^{\dagger}] \tilde{\mathbf{H}}_{p}^{\dagger} + \sigma_{n}^{2} \mathbf{I}$$
 (34)

where  $\tilde{\mathbf{H}}_p$  and  $\tilde{\mathbf{x}}_p$  are defined similarly to (31).

It follows [23] that there are only L distinct eigenvalues of  $\mathbf{H}^{\dagger}\Phi^{-1}\mathbf{H}$ , each with multiplicity M and that these are the same as the eigenvalues of  $\mathcal{H}^{\dagger}\Psi^{-1}\mathcal{H}$ . Therefore, utilizing the results derived in (26) and (27), the weight matrices,  $\mathbf{T}$  and  $\mathbf{R}$ , which maximize the output SINR are given by  $\mathbf{T}_{\mathrm{opt}} = [\mathbf{t}_{\mathrm{opt}} \ \mathbf{t}_{\mathrm{opt}} \ \cdots]$ , and  $\mathbf{R}_{\mathrm{opt}} = [\mathbf{r}_{\mathrm{opt}} \ \mathbf{r}_{\mathrm{opt}} \ \ldots]$ , respectively, where

$$\mathbf{r}_{\text{opt}} = \mathbf{\Psi}^{-1} \mathcal{H} \mathbf{t}_{\text{opt}} \tag{35}$$

and

$$\mathbf{t}_{\mathrm{opt}} = \sqrt{P_T} \mathbf{e} \tag{36}$$

and e is the eigenvector that corresponds to the largest eigenvalue of  $\mathcal{H}^{\dagger}\Psi^{-1}\mathcal{H}.$ 

This solution is the same as the results in [12]–[19]. The corresponding maximum SINR can be found very easily to be  $\sigma_z^2 P_T \lambda_{\max}$  per symbol, where  $\lambda_{\max}$  is the largest eigenvalue or maximal eigenvalue of the matrix  $\mathcal{H}^{\dagger} \Psi^{-1} \mathcal{H}$ . Therefore, the maximum SINR we can achieve with the constraint  $\|\mathbf{t}_m\|^2 = P_T \ \forall m$  is when the weight vectors (35) and (36) are used throughout the packet.

For the special case of flat fading without interference,  $\Phi$  is simply the correlation matrix of the complex Gaussian noise. Hence, the optimum values of  $\mathbf{t}_{\mathrm{opt}}, \mathbf{r}_{\mathrm{opt}}$  and the corresponding maximum SINR are then, respectively, given by

$$\mathbf{t}_{\mathrm{opt}} = \sqrt{P_T} \cdot \text{Maximum eigenvector of } (\mathcal{H}^\dagger \mathcal{H})$$
 (37)

$$\mathbf{r}_{\text{opt}} = \frac{\mathcal{H}\mathbf{t}_{\text{opt}}}{\sigma_n^2} \tag{38}$$

$$SINR|_{max} = \left(\frac{\sigma_z}{\sigma_n}\right)^2 P_T \lambda_{max}.$$
 (39)

This can be considered as *an extension of maximum ratio combining* (MRC) with multiple antennas at BS and MS. In particular, the BS transmits according to the channel condition and the MS combines the received signals based on their SNRs. When there is only one transmit antenna, (38) and (39) reduce to the standard MRC formulas.

#### IV. SIMULATION RESULTS

The proposed SBM system is investigated for a TDMA/time division duplex (TDD) based wireless communication system by computer simulation. Two configurations are considered: 1) two antenna elements at both the BS and MS and 2) two antenna elements at BS and three antenna elements at MS, in which the packet size M=50 and  $n_s=1$ . The results are also compared with a conventional adaptive antenna system where two, three, or four antennas are used at the BS only, and a MIMO system using singular value decomposition (SVD) at the transmitter and minimum mean square error (MMSE) at the receiver. To refer to the different configurations, we use the notation K+L. For example, when we use two antennas at BS and three antennas at MS with SBM, we refer to it as 2+3 SBM. Alternatively,

when we use a conventional adaptive antenna system with two antennas at the BS, we refer to it as 2+1 conventional.

Average bit-error probability  $(P_e)$  is provided for various CCI [Signal-to-interference ratio (SIR)] and AWGN (SNR). The "average SNR per branch-to-branch" in the x-axis of the figures is defined as  $E[|\alpha|^2]E_b/N_o$  where  $E[|\alpha|^2]$  is the average channel power from a transmit antenna to a receive antenna,  $E_b$  is the average bit energy, and  $N_o$  is the noise spectral density. For each  $P_e$  simulation, data packets consisting of 50 data symbols are transmitted with more than 10 000 independent channels [22].

The simulation is performed in the context of a QPSK signaling scheme, the transmitted baseband signal is

$$s(t) = \sum_{n} z_n p(t - nT) \tag{40}$$

where  $\{z_n\}$  is the complex symbol sequence having the values of  $\pm 1 \pm j$  and p(t) is the pulse shaping function at the transmitter which gives a bandlimited transmitting signal. One popular example of p(t) is the root-raised cosine pulse shaping filter and here we take roll-off factor of 0.3. In practice, pulse shaping is performed at both the transmitter and receiver to provide matched filtering for SNR enhancement.

### A. Channel Model

The antenna elements transmit or receive information through a wireless communication channel which is here characterized by a multipath fading model. For a particular channel, the multipath model is represented by its channel impulse response using a *q*-ray model defined as [24], [25]

$$c_{\ell,k}(t) = \sum_{i=0}^{q-1} \beta_{\ell,k}^{i} \delta\left(t - \tau_{\ell,k}^{i}\right)$$
 (41)

where the subscripts  $\ell,k$  refer to the channel between the  $\ell$ th and kth antenna at the BS and MS, respectively and n is the total number of paths. Likewise,  $\beta_{\ell,k}^i$  and  $\tau_{k,\ell}^i$  are, respectively, the complex gain and time delay for the ith path of the diversity channel. In the simulation, the channel of each link contains ten random multipath components [q=10] will be defined later in (41)] and one interferer (P=1).

To determine  $\beta_{\ell,k}^i$ , we can use either ray tracing (deterministic model) [26] or statistical approaches. In this paper, a statistical approach is used to allow easier control of channel parameters such as delay spread. Assuming that paths with different delays are uncorrelated (i.e., uncorrelated scattering) and that the paths are uncorrelated for each antenna branch so as to provide perfect spatial diversity. As a result, path gains  $\beta_{\ell_1,k_1}^{i_1}$  and  $\beta_{\ell_2,k_2}^{i_2}$  are uncorrelated if  $\ell_1 \neq \ell_2$  or  $k_1 \neq k_2$  or  $i_1 \neq i_2$ . This will be realistic if antenna spacings at the MS and BS are, respectively, greater than 0.4 and 20–40 wavelengths. We can refer to [27] for the effect of correlation on the antennas. Additionally, the transmitted signals from other users causing CCI are also assumed to suffer from the delay spread of radio channels with uncorrelated path gains. We model  $\beta_{\ell,k}^i$  statistically by zero-mean, complex

Gaussian random variables, with their power following the exponential delay profile given by

$$E[|c_{\ell,k}(t)|^2] = \begin{cases} \frac{1}{D} \exp(-\frac{t}{D}), & \text{for } t \ge 0\\ 0, & \text{elsewhere.} \end{cases}$$
(42)

Hence,  $h_j^{(\ell,k)}$  in (2) is equal to  $(p \otimes c_{\ell,k} \otimes p)(t)|_{t=jT}$  where  $\otimes$  denotes the convolution operator between two continuous time signals. For simplicity, we consider only the paths with delays less than five normalized rms delay spread which is defined as  $D \stackrel{\triangle}{=} \tau_{\rm rms}/T$  where  $\tau_{\rm rms}$  and T are the rms delay spread and symbol period, respectively. In addition, we specifically assume the path delay as  $\tau_{\ell,k}^i = (5Di)/(M-1)$ .

#### B. Results

In Fig. 2, results are provided for a flat Rayleigh fading channel in the absence of interference for the configurations 2+1 conventional, 3+1 conventional, 4+1 Conventional, 2+2 SVD-MMSE, 2+3 SVD-MMSE, 2+2 SBM, and 2+3 SBM. A close observation of this figure indicates that there is over 100 times decrease in  $P_e$  when 2+2 SBM is employed compared to 2+1 conventional for SNR > 10 dB. This is an interesting result and reveals that significant advantages can be achieved by using smart antennas at both the BS and MS. In addition, SVD-MMSE has almost the same performance as that of SBM, which agrees with theoretical results.

It can also be argued that to obtain fair comparisons, the same number of antenna elements should be utilized in both configurations. Taking four antenna elements, this implies that we should compare 2+2 SBM and 3+1 conventional and referring to Fig. 2, this reveals that 2+2 SBM has about tenfold improvement in BER for SNR > 10 dB. This advantage in SBM comes about by realizing that an additional branch of diversity is available compared to the conventional system even if the total number of antennas used in both configurations is the same. Note also that more than tenfold improvement is possible for the 2+3 SBM system compared with 4+1 conventional system when SNR > 6 dB.

In Fig. 3, results are provided for a flat Rayleigh fading channel but with CCI at SIR = 15 dB. These results demonstrate that 2+2 SBM provides over 100 fold decrease in  $P_e$  as compared to 2+1 conventional when SNR > 11 dB. The results also illustrate that more than a tenfold reduction in  $P_e$  is possible for 2+2 SBM compared with 3+1 conventional for SNR > 10 dB. Note that the results for SVD-MMSE now become slightly worse compared to SBM, and the difference is supposed to get larger as SNR increases.

Results in Fig. 4 are provided for a flat Rayleigh fading channel with CCI at SIR = 0 dB. In this situation, note that the performance of 2+2 SBM becomes closer to the performance of 3+1 conventional smart antenna system while the performance of 2+3 SBM is close to that of a 4+1 conventional antenna system at the BS only. The reason for this is that the antenna weights are used for CCI suppression, so that the diversity gain is relatively low compared to the high SIR case. In addition, results demonstrate that the performance difference between SVD-MMSE and SBM becomes large, and the performance of 2+2 SVD-MMSE is even not as good as

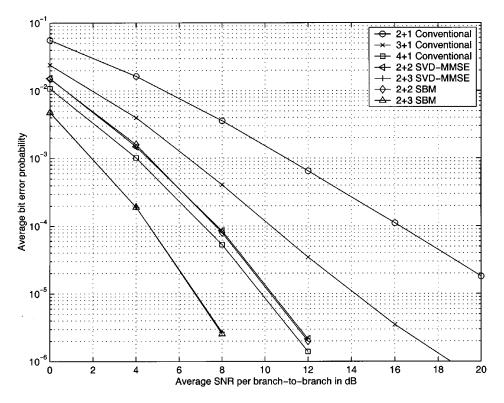


Fig. 2. Average error probability performance of SBM under conditions of no CCI and flat fading.

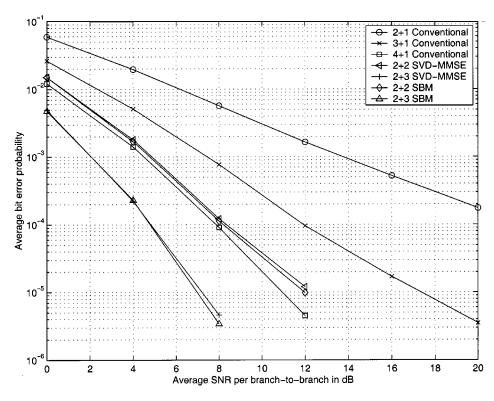


Fig. 3. Average error probability performance of SBM under conditions in flat fading channels with a single dominant CCI at SIR = 15 dB.

that of 3+1 conventional when SNR > 0 dB. Note also that 2+2 SBM and 3+1 conventional smart antenna system can have better performance compared with 2+3 SVD-MMSE, starting at SNR = 6 dB, and 8 dB, respectively.

In Figs. 5–7, results for frequency selective fading channels are presented. The frequency selective channels

are characterized by the normalized rms delay spread, D, which is an important and convenient measure of the degree of frequency selective fading. In particular, in digital transmission over multipath channels, the BER is highly dependent on D [28]. In our simulations, we will exclusively set D=0.5.

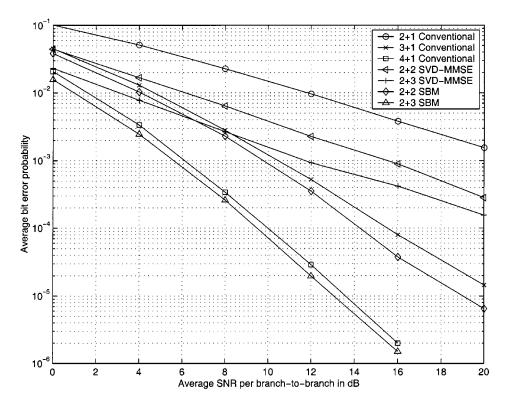


Fig. 4. Average error probability performance of SBM under conditions in flat fading channels with a single dominant CCI at SIR = 0 dB.

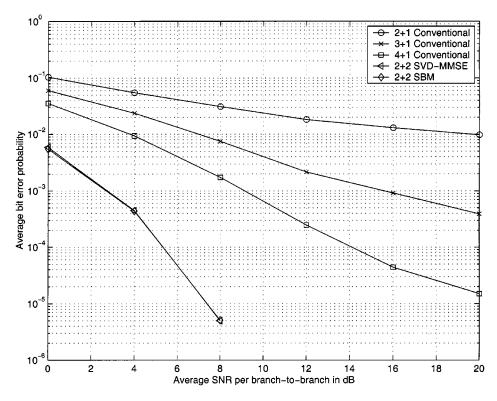


Fig. 5. Average error probability performance of SBM in frequency selective fading channels (D = 0.5) with no CCI.

In Fig. 5, results of BER are provided for D=0.5 with no CCI. Here it is revealed that 2+2 SBM and 2+2 SVD-MMSE have over 100 fold improved BER performance for SNR >6 dB when compared even to 4+1 conventional. This huge performance improvement can be explained by realizing that for SBM system, CCI suppression, and equalization can be performed

jointly while the conventional smart antenna systems are unable to equalize the signal effectively. Additionally, in the absence of CCI, SVD-MMSE has the same performance as SBM.

In Figs. 6 and 7, similar results are provided but with SIRs of 15 and 0 dB, respectively. The relative performance of SBM compared to conventional systems decreases,

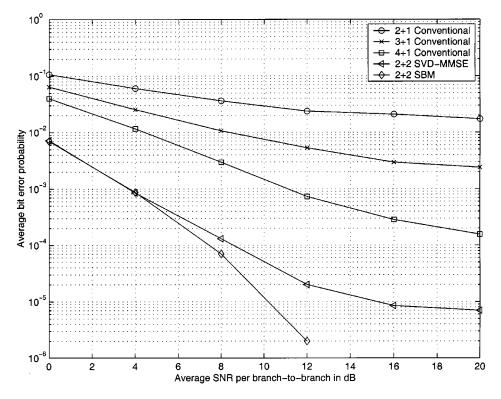


Fig. 6. Average error probability performance of SBM in frequency selective fading channels (D = 0.5) with a single dominant CCI at SIR = 15 dB.

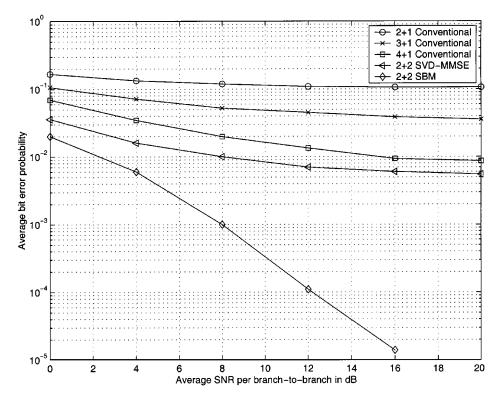


Fig. 7. Average error probability performance of SBM in frequency selective fading channels (D=0.5) with a single dominant CCI at SIR=0 dB.

but for SNR > 12 dB, over 100-fold decrease in BER is possible even with SIR = 0 dB. Results also demonstrate that SVD-MMSE becomes worse as SIR decreases, and huge difference compared to SBM can be noticed. However, SVD-MMSE has better performance compared to conventional smart antenna system as it could somewhat equalize

the ISI. However, results also demonstrate that, as SNR gets close to SIR, the slope of the performance of SVD-MMSE changes significantly and the performance converges. This can be explained by the fact that the ISI of the desired signal is not joint optimized. Hence, the receive weights need not only suppress the CCI but also the ISI.

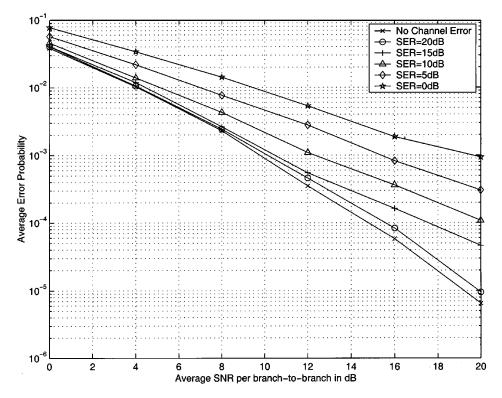


Fig. 8. Average error probability performance of 2+2 SBM in flat fading channels with CCI at SIR = 0 dB in the presence of channel estimation error.

Overall, these results imply that multiple antennas at MS and BS can have very good  $P_e$  performance, while reducing the required total number of antennas used, in frequency selective fading channels. Results also reveal that the performance of SBM in frequency selective fading channels is slightly better than that in flat fading and this is because path diversity is obtained by the inherent space—time equalization of SBM. Therefore, multipath could be a desired feature for high-speed wireless communications. In addition, SBM outperforms significantly SVD-MMSE in the presence of CCI. As such, the joint optimization of antenna weights at BS and MS is important.

#### V. DISCUSSION

The results in the previous section indicate that we can achieve useful improvements in performance compared with existing systems but there are additional considerations such as computational load, channel estimation, and channel errors, and we wish to briefly discuss them.

# A. Computational Load

The computational requirement for implementing the joint smart antennas can be large when K,L or N is large. The computation of (26) and (27) requires several matrix multiplications involving  $\mathbf{H}, \mathbf{\Phi}$ , and  $\mathbf{T}$ , each of sizes,  $(N+\nu)L \times NK, (N+\nu)L \times (N+\nu)L$ , and  $NK \times M$ , respectively. Additionally, the inverse of  $\mathbf{\Phi}$  and the eigenvectors of  $\mathbf{H}^{\dagger}\mathbf{\Phi}^{-1}\mathbf{H}$  are needed to be computed.

Several possibilities are available for complexity reduction. For instance, it is possible to group the packet into many subpackets and calculate the weights for the subpackets in order to

avoid computing matrix operations with high dimensions. Performance, however, would be degraded due to the loss of some path diversity. In addition, it is also possible to add in a cyclic prefix to the signals before transmission so that discrete Fourier transform (DFT) and inverse discrete Fourier transform (IDFT) matrices could be used for diagonalization, as in orthogonal frequency-division multiplexing (OFDM) systems.

## B. Channel Matrix Estimation

The calculation of the weights (26) and (27) requires that the channel be estimated. Using pilot tones [29], the channel response  $\{h_j^{(\ell,k)}\}$  can be measured and the matrix  $\mathbf{H}$  can be constructed by using (2) and (5). In TDD systems, pilot tones on the downlink can be used to estimate the uplink channel since the channels are reciprocal. For frequency division duplex (FDD) systems, feedback of the channel estimations would be necessary.

Estimating the correlation matrix and reference correlation vector can be found from

$$E[\mathbf{y}\mathbf{y}^{\dagger}] = \mathbf{H}E[\mathbf{x}\mathbf{x}^{\dagger}]\mathbf{H}^{\dagger} + \sum_{p=1}^{P} \tilde{\mathbf{H}}_{p}E[\tilde{\mathbf{x}}_{p}\tilde{\mathbf{x}}_{p}^{\dagger}]\tilde{\mathbf{H}}_{p}^{\dagger} + \sigma_{n}^{2}\mathbf{I} \quad (43)$$

and

$$\mathbf{S} = E[\mathbf{y}c_n^*] \tag{44}$$

by using a reference sequence reception period [30]. The correlation matrix of the undesired signal at the mobile can then be estimated from

$$\hat{\mathbf{\Phi}} = E[\mathbf{y}\mathbf{y}^{\dagger}] - \frac{\mathbf{S}\mathbf{S}^{\dagger}}{\sigma_{z}^{2}} \tag{45}$$

and fed back to the BS.

#### C. Sensitivity to Channel Matrix Errors

In general, channel estimation will contain some error depending on the channel quality as well as the ability of the channel estimation method used. In order to estimate the system performance of SBM in a more realistic way, the  $P_e$  performance of SBM in which the channel and feedback information are in error is investigated.

To study the sensitivity of our system to channel errors, we model the estimation error, e, as zero-mean complex AWGN with variance  $\sigma_e^2$ , so that

$$\begin{split} \hat{h}_0^{(\ell,k)} &= h_0^{(\ell,k)} + e_{\ell,k}, \\ & \text{for } k = 1, \dots, K \quad \text{and} \quad \ell = 1, \dots, L \quad \text{(46)} \\ \hat{\underline{\phi}}_{m,n} &= \underline{\phi}_{m,n} + e_{m,n}, \quad \text{for } m,n = 1, \dots, K \quad \quad \text{(47)} \end{split}$$

where  $\hat{h}_0^{(\ell,k)}$  and  $\hat{\underline{\phi}}_{m,n}$  are the estimates of  $h_0^{(\ell,k)}$  (elements of  $\underline{\mathbf{H}}$ ) and  $\underline{\phi}_{m,n}$  (elements of  $\underline{\boldsymbol{\Phi}}$ ), respectively. To characterize the errors, we define the term, signal-to-error ratio (SER), which is given by  $E[|h_0^{(\ell,k)}|^2]/\sigma_e^2$  or  $E[|\underline{\phi}_{m,n}|^2]/\sigma_e^2$ .

In Fig. 8, results are provided for flat fading channels in the presence of CCI with SIR = 0 dB for  $SER = 0, 5, 10, 15, 20, \infty$  dB. Note that when SER = 20 dB, nearly the same performance is obtained. However, as SER decreases, the degradation becomes larger. Results reveal that as long as SER is greater than 15 dB, the performance has only little degradation. Accordingly, in interference limited environments, accurate channel estimation becomes important.

### VI. CONCLUSION

The investigation presented here has demonstrated the use of smart antennas at the base and mobile stations for frequency selective and frequency flat fading channels in the presence of interference. Analytical expressions for the jointly optimized antenna weights have been obtained and these reduce to existing expressions for the flat fading situation. Simulation results reveal that reduction in average bit-error probability by at least one order of magnitude with flat and selective fading with CCI is possible by SBM compared to conventional systems. For example, when the normalized rms delay spread is 0.5 and SIR = 0 dB, 2+2 SBM for SNR greater than 12dB has BER over 100 fold less than a 4+1 conventional system. In addition, our system has also been compared with a SVD scheme with MMSE applied at the receiver. Results conclude that the joint optimization of antenna weights is extremely important and more than 100 fold decrease in  $P_e$  is possible when interference is present.

The implementation of the system, however, requires that multiple antennas and signaling overheads be incorporated into the MS. Additionally, a larger computational load is also imposed. Consequently, we suggest its suitability for high speed data communications for wireless computing applications in combination with recent advances in antenna design.

#### APPENDIX

Define a set of hermitian matrices  $\{\mathbf{A}_n\}_{n=0}^N$ . For  $n=1,\ldots,N$ , the matrices are defined by

$$\mathbf{A}_n \stackrel{\triangle}{=} \sum_{i=1}^n \mathbf{a}_i \mathbf{a}_i^{\dagger} + \mathbf{B} \tag{48}$$

and

$$\mathbf{A}_0 \stackrel{\triangle}{=} \mathbf{B} \tag{49}$$

where **B** is hermitian and positive definite, and  $\{a_i\}_{i=1}^N$  are column vectors. It follows that:

$$\mathbf{v}^{\dagger} \mathbf{A}_{N}^{-1} \mathbf{v} \le \mathbf{v}^{\dagger} \mathbf{B}^{-1} \mathbf{v} \tag{50}$$

with equality if and only if

$$\mathbf{v}^{\dagger}\mathbf{B}^{-1}\mathbf{a}_{N} = \mathbf{v}^{\dagger}\mathbf{B}^{-1}\mathbf{a}_{N-1} = \dots = \mathbf{v}^{\dagger}\mathbf{B}^{-1}\mathbf{a}_{1} = 0$$
 (51)

is satisfied.

*Proof:* From the definition, it can be seen that for n = 1, ..., N, we have the following recursive relation

$$\mathbf{A}_n = \mathbf{a}_n \mathbf{a}_n^{\dagger} + \mathbf{A}_{n-1}. \tag{52}$$

Using the mathematical theory [31] that for a matrix  $\mathbf{Q} = \mathbf{r}\mathbf{r}^{\dagger} + \mathbf{S}$  where  $\mathbf{Q}$  and  $\mathbf{S}$  are square matrices of the same size, and  $\mathbf{r}$  is a column vector,  $\mathbf{Q}^{-1}$  can be expressed as

$$\mathbf{Q}^{-1} = \mathbf{S}^{-1} - \frac{\mathbf{S}^{-1} \mathbf{r} \mathbf{r}^{\dagger} \mathbf{S}^{-1}}{\mathbf{r}^{\dagger} \mathbf{S}^{-1} \mathbf{r} + 1}.$$
 (53)

Letting  $\mathbf{Q} = \mathbf{A}_n$ , we get

$$\mathbf{A}_{n}^{-1} = \mathbf{A}_{n-1}^{-1} - \frac{\mathbf{A}_{n-1}^{-1} \mathbf{a}_{n} \mathbf{a}_{n}^{\dagger} \mathbf{A}_{n-1}^{-1}}{\mathbf{a}_{n}^{\dagger} \mathbf{A}_{n-1}^{-1} \mathbf{a}_{n} + 1}.$$
 (54)

Now, for any column vector  $\mathbf{v}$ , our objective is to find the upper bound of

$$\mathbf{v}^{\dagger} \mathbf{A}_{N}^{-1} \mathbf{v} = \mathbf{v}^{\dagger} \left( \sum_{i=1}^{N} \mathbf{a}_{i} \mathbf{a}_{i}^{\dagger} + \mathbf{B} \right)^{-1} \mathbf{v}$$
 (55)

and the condition provides equality. To find the upper bound, let us first consider the case for  $1 \le n \le N$ . This gives

$$\mathbf{v}^{\dagger} \mathbf{A}_{n}^{-1} \mathbf{v} = \mathbf{v}^{\dagger} \left[ \mathbf{A}_{n-1}^{-1} - \frac{\mathbf{A}_{n-1}^{-1} \mathbf{a}_{n} \mathbf{a}_{n}^{\dagger} \mathbf{A}_{n-1}^{-1}}{\mathbf{a}_{n}^{\dagger} \mathbf{A}_{n-1}^{-1} \mathbf{a}_{n} + 1} \right] \mathbf{v}$$

$$= \mathbf{v}^{\dagger} \mathbf{A}_{n-1}^{-1} \mathbf{v} - \frac{\left| \mathbf{v}^{\dagger} \mathbf{A}_{n-1}^{-1} \mathbf{a}_{n} + 1 \right|^{2}}{\mathbf{a}_{n}^{\dagger} \mathbf{A}_{n-1}^{-1} \mathbf{a}_{n} + 1}$$

$$\leq \mathbf{v}^{\dagger} \mathbf{A}_{n-1}^{-1} \mathbf{v}$$

$$(56)$$

where the equality holds when

$$\left|\mathbf{v}^{\dagger}\mathbf{A}_{n-1}^{-1}\mathbf{a}_{n}\right|=0. \tag{57}$$

Repeatedly using (56) and (57), we then have

$$\mathbf{v}^{\dagger} \mathbf{A}_{N}^{-1} \mathbf{v} \le \mathbf{v}^{\dagger} \mathbf{A}_{N-1}^{-1} \mathbf{v} \le \dots \le \mathbf{v}^{\dagger} \mathbf{A}_{0}^{-1} \mathbf{v} = \mathbf{v}^{\dagger} \mathbf{B}^{-1} \mathbf{v}.$$
(58)

The upper bound can be obtained when all the equalities hold. This is achieved when the following set of equations is satisfied:

$$\mathbf{v}^{\dagger} \mathbf{A}_{N-1}^{-1} \mathbf{a}_{N} = \mathbf{v}^{\dagger} \mathbf{A}_{N-2}^{-1} \mathbf{a}_{N-1} = \dots = \mathbf{v}^{\dagger} \mathbf{A}_{0}^{-1} \mathbf{a}_{1} = 0.$$
(59)

To simplify this condition, let us consider the general equation  $\mathbf{v}^{\dagger} \mathbf{A}_{n}^{-1} \mathbf{a}_{n+1} = 0$ ,

$$\mathbf{v}^{\dagger} \mathbf{A}_{n-1}^{-1} \mathbf{a}_{n+1} - \frac{\left(\mathbf{v}^{\dagger} \mathbf{A}_{n-1}^{-1} \mathbf{a}_{n}\right) \left(\mathbf{a}_{n}^{\dagger} \mathbf{A}_{n-1}^{-1} \mathbf{a}_{n+1}\right)}{\mathbf{a}_{n}^{\dagger} \mathbf{A}_{n-1}^{-1} \mathbf{a}_{n} + 1} = 0. \quad (60)$$

However, we know from (59) that  $\mathbf{v}^{\dagger} \mathbf{A}_{n-1}^{-1} \mathbf{a}_n = 0$ , as such

$$\mathbf{v}^{\dagger} \mathbf{A}_{n-1}^{-1} \mathbf{a}_{n+1} = 0. \tag{61}$$

Then, repeatedly doing the steps (60) and (61), we have

$$\mathbf{v}^{\dagger}\mathbf{B}^{-1}\mathbf{a}_{n+1} = 0. \tag{62}$$

Using the above results, we can rewrite the condition (59) as

$$\mathbf{v}^{\dagger} \mathbf{B}^{-1} \mathbf{a}_{N} = \mathbf{v}^{\dagger} \mathbf{B}^{-1} \mathbf{a}_{N-1} = \dots = \mathbf{v}^{\dagger} \mathbf{B}^{-1} \mathbf{a}_{1} = 0$$
 (63)

and this firms up the proof.

#### ACKNOWLEDGMENT

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#### REFERENCES

- K. B. Letaief, J. C.-I. Chuang, and R. D. Murch, "A high-speed transmission method for wireless personal communications," in *Wireless Personal Communications*. Norwell, MA: Kluwer, 1996, pp. 299–317.
- [2] C. G. Günther, J. E. Padgett, and T. Hattori, "Overview of wireless personal communications," *IEEE Commun. Mag.*, vol. 33, pp. 28–41, Jan. 1995
- [3] N. Seshadri, A. F. Naguib, V. Tarokh, and A. R. Calderbank, "Space-time coded modulation for high data rate wireless communications," in *Proc. IEEE Globecom*, Phoenix, AZ, Nov. 1997, pp. 102–109.
- [4] Y. Chen, K. B. Letaief, and J. C.-I. Chuang, "Soft-output equalization and TCM for wireless personal communication systems," *IEEE J. Select. Areas Commun.*, vol. 16, pp. 1679–1690, Dec. 1998.
- [5] J. H. Winters, "Signal acquisition and tracking with adaptive arrays in the digital mobile radio system IS-54 with flat fading," *IEEE Trans. Veh. Technol.*, vol. 42, pp. 377–384, Nov. 1993.
- [6] J. Fuhl and A. F. Molisch, "Capacity enhancement and BER in a combined SDMA/TDMA system," in *IEEE Vehicular Technology Conf.*, vol. 3, New York, Apr. 1996, pp. 1481–1485.
- [7] K. J. R. Liu, F. R. Farrokhi, and L. Tassiulas, "Transmit and receive diversity and equalization in wireless networks with fading channels," in *Proc. IEEE Globecom*, Phoenix, AZ, Nov. 1997, pp. 1193–1198.
- [8] R. Schmalenberger and J. J. Blanz, "Multi antenna C/I balancing in the downlink of digital cellular mobile radio systems," in Proc. IEEE Vehicular Technology Conf., Phoenix, AZ, May 4–7, 1997, pp. 607–611.
- [9] C. R. Rowell and R. D. Murch, "A capacitively loaded PIFA for compact mobile telephone handsets," *IEEE Trans. Antennas Propagat.*, vol. 45, pp. 837–842, May 1997.
- [10] G. J. Foschini, "Layered space-time architecture for wireless communication in a fading environment when using multiple antennas," *Bell Lab. Tech. J.*, vol. 1, no. 2, pp. 41–59, 1996.
- [11] G. G. Raleigh and J. M. Cioffi, "Spatio-temporal coding for wireless communications," in *Proc. IEEE Globecom*, London, U.K., Nov. 1996, pp. 1809–1814.
- [12] J. B. Andersen, "Intelligent antennas in a scattering environment—An overview," in *Proc. IEEE Globecom*, vol. 6, Sydney, Australia, Nov. 1998, pp. 3199–3203.

- [13] —, "Array gain and capacity for known random channels with multiple element arrays at both ends," *IEEE J. Select. Areas Commun.*, vol. 18, pp. 2172–2178, Nov. 2000.
- [14] ——, "Intelligent antennas in personal communications," presented at the IEEE Int. Conf. Personal Wireless Communications, Jaipur, India, Feb. 1999.
- [15] R. Kohno, "Spatial and temporal communication theory using software antennas for wireless communications," in *Int. Symp. Personal, Indoor, Mobile Radio Communication*, Helsinki, Finland, Sept. 1–4, 1997, pp. 293–321.
- [16] J. Salz, "Digital transmission over cross-coupled linear channels," ATT Tech. J., vol. 64, pp. 1147–1159, July 1985.
- [17] J. Yang and S. Roy, "On joint transmitter and receiver optimization for multiple-input-multiple-output (MIMO) transmission systems," *IEEE Trans. Commun.*, vol. 42, pp. 3221–3231, Dec. 1994.
- [18] K.-K. Wong, K. B. Letaief, and R. D. Murch, "Investigating the performance of smart antenna systems at the mobile and base stations in the down and uplinks," *Proc. IEEE Vehicular Technology Conf.*, vol. 2, pp. 880–884, May 17–21, 1998.
- [19] K.-K. Wong, R. S.-K. Cheng, K. B. Letaief, and R. D. Murch, "Adaptive antennas at the mobile and base stations in an OFDM/TDMA system," *IEEE Trans. Commun.*, vol. 49, pp. 1–8, Jan. 2001.
- [20] J. H. Winters, "On the capacity of radio communication systems with diversity in a Rayleigh fading environment," *IEEE J. Select. Areas Commun.*, vol. SAC-5, pp. 871–878, June 1987.
- [21] J. H. Winters, J. Salz, and R. D. Gitlin, "The impact of antenna diversity on the capacity of wireless communication systems," *IEEE Trans. Commun.*, vol. 42, pp. 1740–1751, Feb. 1994.
- [22] J. C.-L. Ng, K. B. Letaief, and R. D. Murch, "Trade-offs between diversity combining and equalization for wireless LANs," in *Proc. IEEE Vehicular Technology Conf.*, Phoenix, AZ, May 4–7, 1997, pp. 875–879.
- [23] G. H. Golub and C. F. Van Loan, Matrix Computations. Baltimore, MD: The Johns Hopkins Univ. Press, 1996.
- [24] L. F. Chang and J. C.-I. Chuang, "Diversity selection using coding in a portable radio communications channel with frequency-selective fading," *IEEE J. Select. Areas Commun.*, vol. 7, pp. 89–97, Jan. 1989.
- [25] K. B. Letaief, K. Muhammad, and J. S. Sadowsky, "Fast simulation of DS/CDMA with and without coding in multi-path fading channels," *IEEE J. Select. Areas Commun.*, vol. 15, pp. 626–639, May 1997.
- [26] T. A. Russell, C. W. Bostian, and T. S. Rappaport, "A deterministic approach to predicting microwave diffraction by buildings for microcellular systems," *IEEE Trans. Antennas Propagat.*, vol. 41, pp. 1640–1649, Dec. 1993.
- [27] J. Salz and J. H. Winters, "Effect of fading correlation on adaptive arrays in digital mobile radio," *IEEE Trans. Veh. Technol.*, vol. 43, pp. 1049–1057, Nov. 1994.
- [28] J. C.-I. Chuang, "The effects of time delay spread on portable radio communications channels with digital modulation," *IEEE J. Select. Areas Commun.*, vol. JSAC-5, pp. 879–889, June 1987.
- [29] J. K. Cavers, "An analysis of pilot assisted modulation for Rayleigh fading channels," *IEEE Trans. Veh. Technol.*, vol. 40, pp. 686–693, Nov. 1991
- [30] K. Yokohata, Y. Ogawa, and K. Itoh, "Spatial-domain path-diversity using an adaptive array for mobile communications," in *Proc. IEEE Int.* Conf. Universal Personal Communications, Nov. 1995, pp. 600–604.
- [31] R. T. Compton Jr., Adaptive Antennas: Concept and Performance. Englewood Cliffs, NJ: Prentice-Hall, 1988.



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