

A novel and anti-agglomerating Ni@yolk-ZrO₂ structure with sub-10nm Ni core for high performance steam reforming of methane

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Abstract

Steam reforming of methane is a versatile technology for hydrogen production in oil refinery and fuel cell applications. Using natural gas is a promising method to produce rich-hydrogen gas. Ni@yolk-ZrO₂ catalyst is used to study steam reforming of methane under various GHSVs, steam-to-carbon (S/C) ratio, and its recyclability. The catalyst was characterized using a combination of XRD, TEM, AAS, TPR, TPH, TGA, BET, XPS, and Raman techniques. The catalyst is evaluated on time stream and identify its anti-agglomeration property and coking mechanism. From the characterization of TEM and XPS establish the information of Ni particles mobility in the catalyst, which active metal particle size was controlled under the yolk-shell structure framework. Furthermore, the results from TGA, TPH, and Raman analysis of the used Ni@yolk-ZrO₂ catalyst showed the characteristic of inhibiting formation of highly ordered carbon structure.

1. Introduction

The steam reforming of methane is a well established industrial process for the production of hydrogen and synthetic gas.^{1, 2} Ni-based catalysts are commonly used in industrial reforming reactions due to their low cost and high activity. However, these catalysts

deactivate fast due to sintering⁵ and coke deposition⁷. Therefore, excess steam ($S/C > 3$) is introduced in the feedstock to prevent coke deposition. The excess steam favours water gas shift reaction that produces higher amount of hydrogen gas. However, steam at high temperature can be corrosive and invasive towards the catalysts. It also leads to deactivation of the catalyst due to oxidation of Ni species.⁸ Therefore, in order to prevent sintering and coke deposition while maintaining the catalyst integrity were the biggest challenges in the steam reforming process.

Several studies discuss enhancing the stability of Ni-based catalyst for the reforming reaction. Promoters such as alkaline earth (MgO or CaO) are often used to lower the coke formation and provide higher stability against sintering.⁹ However, the addition of these promoters obstructs the reduction of NiO leading to less active metals involved in the reactions. It has been observed that promotion with K or Ca increases the formation of NiAl_2O_4 phase, whereby Ni was substituted in the inert spinel structure and became inactive.¹⁰ It was reported that adding tolerable alkaline metal oxide suppressed the coke deposition in the reforming reaction. Hence, it is crucial that the modification of Ni-based catalysts do not compromise the activity.

It is evident that the reducible support (e.g. CeO_2) provides better stability and coke resistance in comparison with non-reducible supports.^{11,12} As they have the direct advantage of oxygen storage capacity that significantly reduces the coke formation on the catalyst surface.¹³ Ceria and ceria-doped supports are well known for their reversible exchange of lattice oxygen during reaction.¹⁴ However, CeO_2 support is vulnerable to sintering and loses its oxygen storage capacity (OSC) at high temperatures (e.g. above 500°C).¹⁵ Also, CeO_2 could fully cover the active metal during the redox reactions due to their amorphous feature which leads to deactivation.¹⁶

The activity of the catalyst often depends on the size and extent of metal dispersion.^{17,18} Small particles increase metal dispersion and also provide more active site (steps/kinks) on the surface.¹⁹ The energy barrier for methane dissociation is much lower at step sites. Therefore, the rate of reaction increases with smaller particles as they consisted of highly concentrated active phase of step sites.²⁰ Besides, small particles below a critical size have also been reported to be more resistant to coke formation.²¹ The highly dispersed active metal particles also tend to minimize surface energy by strongly interact with the support and reduce sintering occurrence. Hence, Ni with good particle size homogeneity and metal support interaction are essential for a highly stable catalyst.

The preparation method often influences the structure and morphology of the catalyst. Recently, a method of embedding the active metal nanoparticles in inorganic cavities shows promising application in preventing sintering of active metal.²² Among these materials, highly defined nanostructure of core-shell and yolk-shell structure have demonstrated excellent properties in various applications, for example, Au-Ni@SiO₂ for hydrolytic dehydrogenation of ammonia borane,²³ metal@TiO₂ yolk-shell nanostructures for photocatalytic dye degradation²⁴ and Au@ZrO₂ for CO oxidation.²⁵ Of particular interest is Au@ZrO₂ yolk-shell nanostructure. This is because it has great potential to be developed for highly stable and ease of gaseous exchange in catalytic applications. In addition, the structure is easy to be modified such as its porosity through modification of the shell to further improve its catalytic performance.²⁶ In this paper, we report a Ni@yolk-ZrO₂ catalyst synthesized via double template emulsion method which shows substantial long term high activity and successfully performed for multiple cycles without deterioration under operation mode of steam reforming of methane at S/C molar ratio of 2.5.

2. Experimental

2.1 Synthesis and characterization

Synthesis of Ni colloids and Ni@SiO₂. The synthesis of Ni@SiO₂ colloids was carried out by reverse micelle approach. Typically, 3ml of aqueous 0.25M NiCl₂ and 11.5ml of Brij L4 (Sigma-Aldrich) were mixed with 40ml of n-octane in a 250ml 3-neck round bottom flask at 30°C under N₂ atmosphere protection. The mixture was stirred for 10 min. 1ml of 3.172M ice-cooled NaBH₄ solution was drop quickly into the flask. Immediately, a clear solution would turn into pitch black and bubbles were generated. After 5 minutes of N₂ purge, the inlet and outlet were sealed. Subsequently the solution was stirred for 12 hours to form stable Ni colloids. The SiO₂ coating achieved by subsequently adding 50ml of n-octane, 2.4ml Brij L4, 1.2ml ammonia (26%-28%), 2ml of TEOS into the solution and kept stirring for 3 hours. After 3 hours, additional 2ml of TEOS was added and stirred for another 5 hours. The Ni@SiO₂ colloids was obtained after centrifuge and washed with acetone and ethanol, then re-dispersed into 40ml of ethanol.

Synthesis of Ni@SiO₂@ZrO₂. 35ml of dispersed Ni@SiO₂ colloids in ethanol was used for the subsequent synthesis by mixing with 0.6ml Brij L4, 0.6ml H₂O in 220ml of ethanol and stirred for 30 minutes. Then, 2ml of Zr(OBu)₄ was added and vigorously stirred for 8hours at 30°C. The colloids were washed with ethanol twice and re-dispersed into 40ml deionized water with 0.001M NaBH₄ and aged for 3 days. The powder was collected and dried under 105°C for 3 hours and calcined at 750°C (2°C/min) for 3 hours.

Synthesis of Ni@yolk-ZrO₂. The calcined powder was dispersed into 40ml of 3M NaOH solution for 48 hours under stirring. The colloids were washed with deionized water several times. After drying at 105°C for 3 hours, the powder was calcined at 550°C. Subsequently, the obtained powder was reduced under H₂ atmosphere at 650°C for 3 hours.

Synthesis of Ni/ZrO₂. 1g of commercially made ZrO₂ powder (TOSOH) was impregnated with 50ml of 0.017M NiCl and stirred under room temperature. After 6 hours, the obtained sol

was dried at 100 °C for 3 hours and subsequently calcined at 750 °C for 3 hours, followed by reduction under H₂ atmosphere at 650°C for 3 hours.

X-ray diffraction patterns were recorded using Bruker D8 Advance with Cu-K α radiation ($\lambda = 1.5418 \text{ \AA}$) in the 2θ range of 10°-90°. Transmission electron microscopy (TEM), model JEM 2100 was used to study the morphology and microstructure of the catalyst. The TEM specimens were prepared by dropping a trace amount of the sample dispersed in ethanol on a carbon coated copper grid (300 mesh). The BET surface area measurement was carried out using a Micrometrics ASAP 2020M apparatus at 77 K. Prior to the measurement, the sample was degassed at 300°C for 5 h under vacuum. Temperature-programmed reduction (FINESORB3010E, Zhejiang Fintec Co.) was performed to determine the nickel species and its reducibility for each catalyst. Typically, catalyst was filled into a U-shape quartz tube and held by quartz wool. Prior to reduction, the sample was treated with pure Ar for 30 min at 300°C to remove any impurities. The temperature was then cooled down to room temperature. 10%H₂/Ar (25mlmin⁻¹) was introduced, and the temperature was increased from room temperature to 800°C with a heating rate of 5°Cmin⁻¹. A temperature programmed hydrogenation was used to identify the carbon species of the used catalyst. Typically, used catalyst (30mg) was loaded into a U-shape quartz tube and held by a quartz wool. Prior to hydrogenation, the sample was treated under pure Ar for 3 h at 100°C and cooled down to room temperature. Then, a mixture of 10%H₂/Ar (25mlmin⁻¹) was introduced into the sample. After 2 hours, the temperature was increased to 900°C with a heating rate of 5°Cmin⁻¹. X-ray photoelectron spectroscopy (XPS) spectra were recorded on a Shimadzu Axis Ultradld spectroscope (Japan) using the monochromatized Al K α radiation resource at room temperature and under a vacuum of 10⁻⁷ Pa (10⁻⁹ Torr). The starting angel of the photoelectron was set at 90°. The spectrum was calibrated with a C 1s spectrum of 248.8 eV. Raman spectra were collected using a Renishaw inVia Reflex ($\lambda=532\text{nm}$) and a CCD detector. The spectrum acquisition consisted of 10 accumulations for 30 s. The spectra were

recorded at ambient temperature. Thermogravimetric analysis (TGA) was conducted using Perkin-Elmer Pyris Diamond TGA equipment. The used catalysts were preheated under a flow of nitrogen (100mlmin^{-1}) for 30 min. Then the samples were heated in air (100mlmin^{-1}) by raising the temperature from room temperature to 1000°C at a rate of 10Cmin^{-1} .

2.2 Catalytic evaluation

Steam reforming of methane was studied in a fixed bed quartz reactor (12mm ID) under atmospheric pressure. The reactor was equipped with a pre-heater, a syringe pump, a cold condenser and a gas flow meter. 100mg of catalyst diluted with filled quartz sand of 2cm length was used. The quartz reactor loaded with catalyst was heated in an electric furnace and the temperature of the bed was controlled by a K-type thermocouple positioned at the center of the catalyst bed. Prior to the test, the catalyst was reduced *in situ* 650°C with 10% H_2/Ar mixture (50mlmin^{-1}) for 3 h. A reaction mixture of H_2O and CH_4 (Steam to carbon molar ratio of 2.5:1) without dilution was fed using a gas hourly space velocity (GHSV) of $50,400\text{mlg}_{\text{cat}}^{-1}\text{h}^{-1}$. The effluent gases were analyzed by an on-line gas chromatography (INESA Scientific Instrument Co.Ltd, GC-122) equipped with a packed column (TDX-01) and a TCD detector. A cold trap was placed before the TCD to remove moisture in the gas products. The peak area normalization method was used for quantitative analysis of effluent gaseous²⁷,²⁸. The CH_4 conversion and CO selectivity were calculated using equations (1) and (2) as follows:

$$X_{\text{CH}_4}(\%) = \frac{[\text{CO}] + [\text{CO}_2]}{[\text{CO}] + [\text{CO}_2] + [\text{CH}_4]} \times 100 \quad (1)$$

$$\text{CO selectivity}(\%) = \frac{[\text{CO}]}{[\text{CO}] + [\text{CO}_2]} \times 100 \quad (2)$$

3. Results and discussion

3.1 Structural studies

XRD patterns of the catalyst are shown in Fig.2. The Ni@yolk-ZrO catalyst shows a low crystallinity of Ni metal compared to impregnated Ni/ZrO₂ catalyst. The catalysts showed the characteristic peaks of tetragonal ZrO₂ and Ni metal. The peaks observed at $2\theta = 44.5^\circ$, 51.8° , and 76.4° can be assigned to the (111), (200), (220) planes of Ni metal, respectively. The average crystallite size of Ni was determined by the peak broadening of the (111) reflection in the XRD patterns, using the Scherrer formula, and was found to be 3.6nm and 213.6nm respectively, for the Ni@yolk-ZrO₂ and impregnated Ni/ZrO₂ catalysts. Furthermore, Ni@yolk-ZrO₂ has a relatively broaden peak of tetragonal phase ZrO₂ at 30.5° (111) as compared to impregnated Ni/ZrO₂ and their crystallite size are 1.4nm and 42.4nm, respectively. This shows that Ni particles were highly disperse in the nano-framework of tetragonal phase ZrO₂.

The TEM micrographs of Ni@yolk-ZrO₂ catalyst before and after steam reforming test are shown in Fig. 3 and Fig. 5. Before reforming test, the Ni particles are uniformly distributed over the ZrO₂ hollow shell and no apparent aggregation of particles was observed. The average particle size of Ni is about 8.9nm. After 48 h on steam reforming of methane, the particle size increased to circa. 9.6nm. The crystallite size of Ni and the average Ni particle size from TEM observation was 8.9nm. Fig.4 shows the XPS Ni 2p peak of freshly reduced Ni@yolk-ZrO₂ with detectable Ni particles over the catalyst surface, in contrast, the used-catalyst showed almost the non-existence of Ni particles over the catalyst surface. From the XPS depth analysis,^{29, 30} Ni particles have been detected partly in the matrix of ZrO₂ hollow shell before testing and inside the hollow shell after steam reforming of methane testing. In addition, the Ni mass concentration is diminished after the reforming testing of Ni@yolk-ZrO₂ catalyst while the impregnated Ni/ZrO₂ remained the same. This

result indicated Ni particles have been moving toward inside the ZrO₂ hollow shell during catalytic testing.

The BET isotherm graph (Fig. 6) showed Ni@yolk-ZrO₂ has Type-IV isotherm characteristic and hysteresis loop of category H3. It has high amount micropore ($P/P_0 < 0.1$) as compared to impregnated Ni/ZrO₂. It also has the characteristic of multilayer adsorption before the onset of capillary condensation. The slope of the multilayer adsorption suggesting slit-shaped pore might present between the nano-size ZrO₂ grains in the shell which would allow gaseous exchange to occur during reactions. XRD patterns of Ni@yolk-ZrO₂ showed broadening peaks of tetragonal phase of ZrO₂, implicating the occurrence of multilayer adsorption of the shell is indeed promoting the high degree of reactants and products exchange. Besides, the capillary condensation is the void space between the Ni core and ZrO₂ shell with 18nm pore. The void space would allow active Ni particle to move freely around but was inhibited to move outside the shell attributed to the presence of the slit-shaped framework of the ZrO₂ shell. Such characteristic is advantageous to significantly reduce active Ni particles from agglomerating with each other and limiting their particle growth.

3.2 Catalytic evaluation

The catalytic steam reforming of methane of yolk-shell and impregnated catalysts were studied at GHSV of 50,400 ml/g_{cat}⁻¹h⁻¹ and S/C=2.5 at 750°C, and the results are shown in Fig. 7a. The methane conversion on Ni@yolk-ZrO₂ catalyst increases with time on steam reforming. Initially reaction time, and then the methane conversion kept at 90% with time on stream. In comparison with impregnated Ni/ZrO₂, the methane conversion is low and increases slowly with time on stream and reached a plateau of 30%. For Ni@yolk-ZrO₂ catalyst, activity maintained with time on stream that may be contributed to the homogeneously distributed active Ni particles. In addition, the TPR testing (Fig. 8) shows that

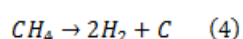
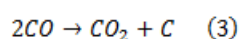
less free NiO species formed in the Ni@yolk-ZrO₂ catalyst as compared to impregnated Ni/ZrO₂ which may stabilize the Ni particle size and influence the catalytic activity.

Analysing the effect of the reaction temperature on the catalytic performance of Ni@yolk-ZrO₂, a temperature of 750°C was kept to study the effect of GHSVs. The purpose of this study is to optimize the possibility of reactants that could be process into synthesis gas. Moreover, steam reforming is an energy consuming process and it is necessary to reduce the process cost. Hence, the methane content in the feed was changed, and the results are depicted in Fig. 7b. As the GHSVs increased, the methane conversion decreased for all S/C conditions. The catalyst performance maintained up to 85% or above of methane conversion (for S/C = 1.5 and S/C = 2), when S/C = 1, the methane conversion was maintained up to 70% or above. Also, it can be observed that the H₂/CO ratio for all conditions is particularly low at GHSV of 20,000 ml_{g_{cat}}⁻¹h⁻¹ and a higher content of CO was produced at this operating condition.

The same catalyst was subjected to recyclability test of steam reforming of methane under S/C = 2.5. The catalyst was tested for 4hours, oxidizes in air at 500°C for 1 hour, reduced at the same temperature for 1 hour, and repeated these cycles for 5 times. The catalyst exhibited a methane conversion of 90% which is almost constant along 5 reaction cycles (Fig. 9a). Also, the catalyst was tested on stream and remained active and continuously producing synthetic gas for 150 hours (Fig. 9b). It is remarkable that the catalyst performance of the Ni@yolk-ZrO₂ exhibiting superior catalytic effect in steam reforming of methane.

3.3 Coking mechanism

Coke formation during steam reforming of methane causes the deactivation of catalysts. The most possible reactions³¹ leading to the carbon formation in steam reforming of methane were:



Equation (3) and (4) were the Boudouard reaction and methane decomposition which were preliminary formation of carbon nanotubes and graphites.³² Therefore, it is essential to determine the carbon species formed in the Ni@yolk-ZrO₂ catalyst as compared to impregnated Ni/ZrO₂. Fig. 10a represents the TGA of both tested catalyst. It is noticed that Ni@yolk-ZrO₂ has higher weight loss than Ni/ZrO₂ with carbon deposition rate of 1.15 mg_{cat}⁻¹h⁻¹ after 48 hours. This might be due to methane dissociation³³ is higher for smaller Ni particles size of Ni@yolk-ZrO₂ than Ni/ZrO₂; hence a higher weight loss would occur on the Ni@yolk-ZrO₂ catalyst. In order to understand the carbon species formed in the catalysts, it was subjected to TPH after steam reforming of methane. As identified in Fig. 10b that the surface carbon species on Ni@yolk-ZrO₂ is weak than Ni/ZrO₂ and the first peaks of carbon species are at 260°C and 293°C respectively. The first peak might be amorphous carbon (α -carbon) on the nickel sites. Second and third peaks would be whisker carbon (β -carbon) or graphitic carbon (γ -carbon) exists in the catalyst. It can be seen that Ni/ZrO₂ has a broad shoulder peak at 360°C and a small peak at 835°C. The impregnated Ni/ZrO₂ catalyst has higher order carbon species formed during the steam reforming of methane as compared to Ni@yolk-ZrO₂ with only α and β carbon. The main carbon deposited in Ni@yolk-ZrO₂ was amorphous carbon due to high density of kinks existing in small Ni particles size and this

amorphous carbon was readily to be reacted with steam. Furthermore, both of the catalyst were carried out under $S/C = 1$ with the same GHSV of $50400 \text{ ml}_{\text{g}_{\text{cat}}^{-1}\text{h}^{-1}}$ for 12 h in order to understand the carbon species formation in Ni@yolk-ZrO₂. From Fig. 11, the weight loss is significantly higher with 5% carbon ($3.29 \text{ mg}_{\text{C}}\text{g}_{\text{cat}}^{-1}\text{h}^{-1}$) was deposited. However, from the TPH analysis, the first peak diminished and second peak was intensified. As for the third peak which occurred at 650°C indicating a higher ordered carbon has formed, but the temperature lies lower than impregnated Ni/ZrO₂ catalyst. This phenomenon suggesting yolk-shell structure inhibiting the formation of highly ordered carbon in Ni@yolk-ZrO₂ catalyst. Further validation of Raman (Fig. 12) of the tested catalysts ($S/C = 2.5$ and $S/C = 1$) showed the presence of the spectra of D band and G band of carbon has the relative intensity ratio I_D/I_G of 0.94 and 0.96. It demonstrates the ZrO₂ shell has inhibited the continuous growth of whisker carbon or graphitic carbon from Ni particle. It can be concluded that Ni@yolk-ZrO₂ exhibiting the capability of inhibiting the formation of higher ordered carbon during steam reforming of methane.

Conclusions

Ni@yolk-ZrO₂ nanoparticles with sub-10nm Ni cores were synthesized via a double template method and evaluated for steam reforming of methane. The effect of introducing ZrO₂ shell for steam reforming of methane was discussed for the first time. It was found that the active Ni particles agglomerating behaviour was controlled by the ZrO₂ shell and showed high activity on steam reforming of methane at 750°C. XPS analysis showed Ni particles were confined in the ZrO₂ shell. The ZrO₂ shell has not only prevented the mobility of the Ni particles but also limited their growth. Raman and TPH analysis have provided the evident that ZrO₂ shell hindered the severe sintering of active Ni particles and continuously providing high catalytic activity in steam reforming of methane. In addition, the yolk-shell structure has the capability to inhibit the formation of highly ordered carbon deposit on the catalyst

surface attributed to ZrO₂ shell isolating highly dispersed active Ni particles. After 150 hours of reaction, Ni@yolk-ZrO₂ nanoparticles preserved their structures and remained active. It is remarkable to develop and comprehend such properties of the catalyst which is possible to be extended to other active metals and high temperature reactions.

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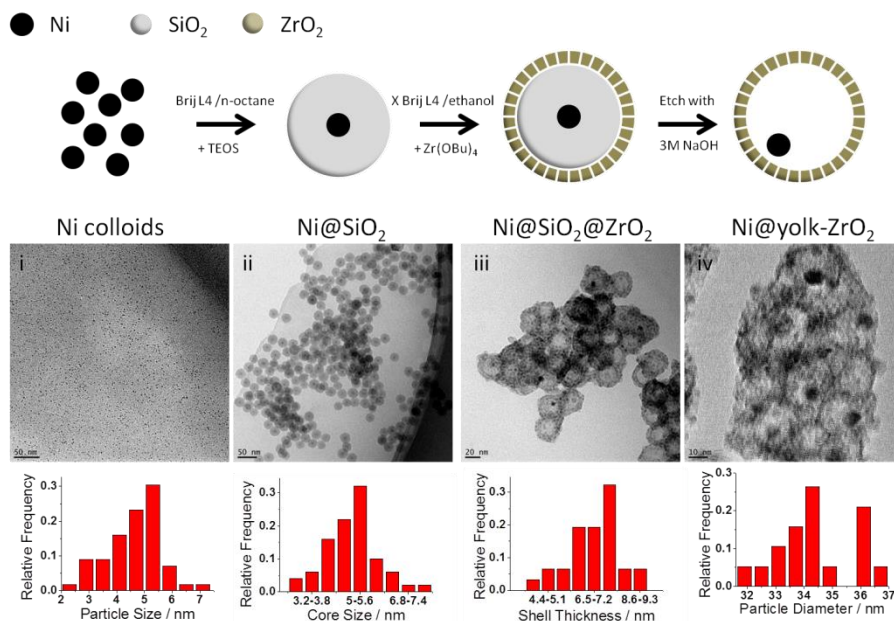


Fig 1. A schematic diagram of the synthetic route of Ni@yolk-ZrO₂ catalyst, and the associated TEM of the structures and core size distributions.

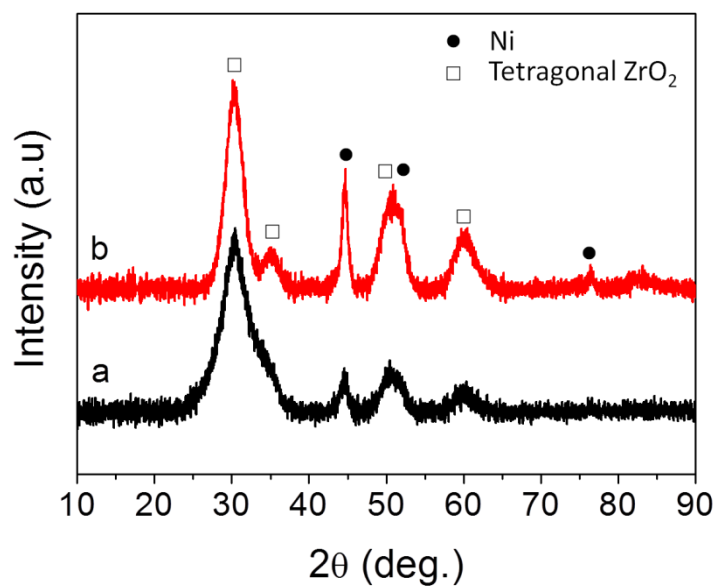


Fig 2. XRD of Ni@yolk-ZrO₂ (a) and impregnated Ni/ZrO₂ (b), both reduced at 650 °C for 3 hours.

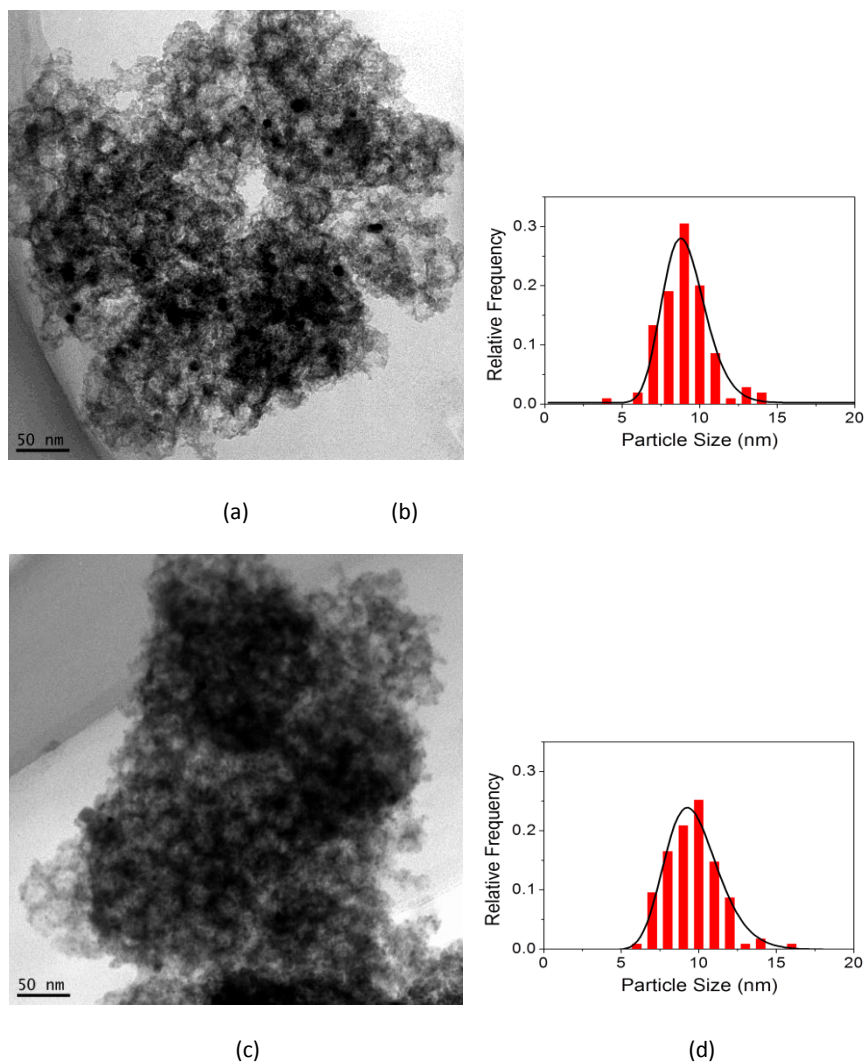


Fig 3. TEM images of Ni@yolk-ZrO₂ before (a) and after 48 h (c) steam reforming test and their Ni core particle size distribution (b) and (d) respectively.

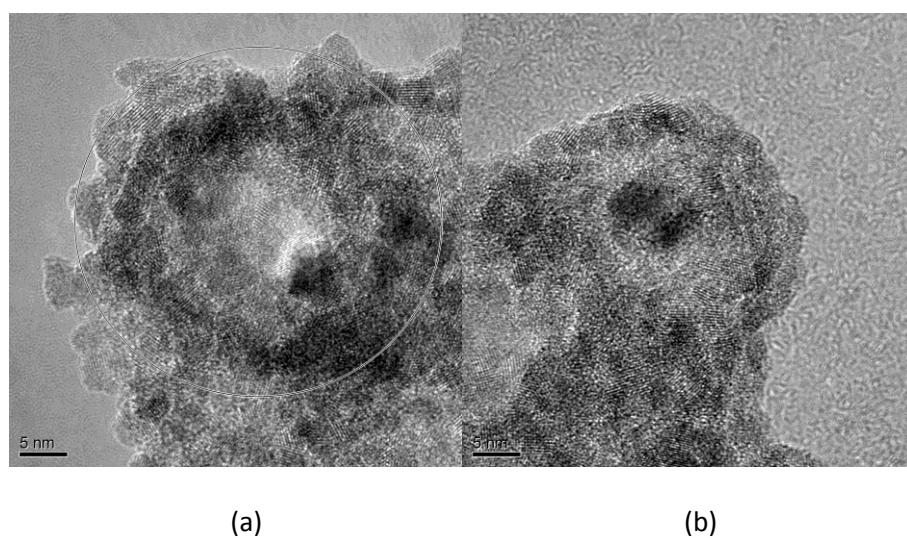


Fig 5. HRTEM images of Ni@yolk-ZrO₂ before (a) and after 48 h (b) steam reforming test.

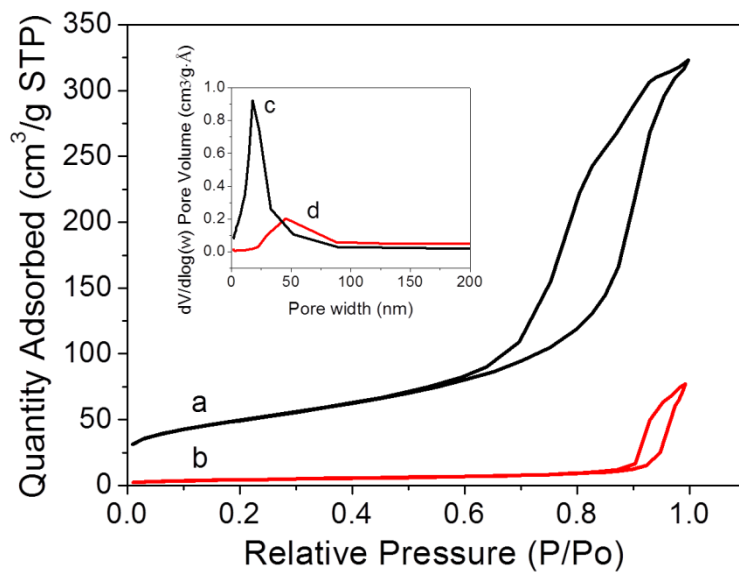
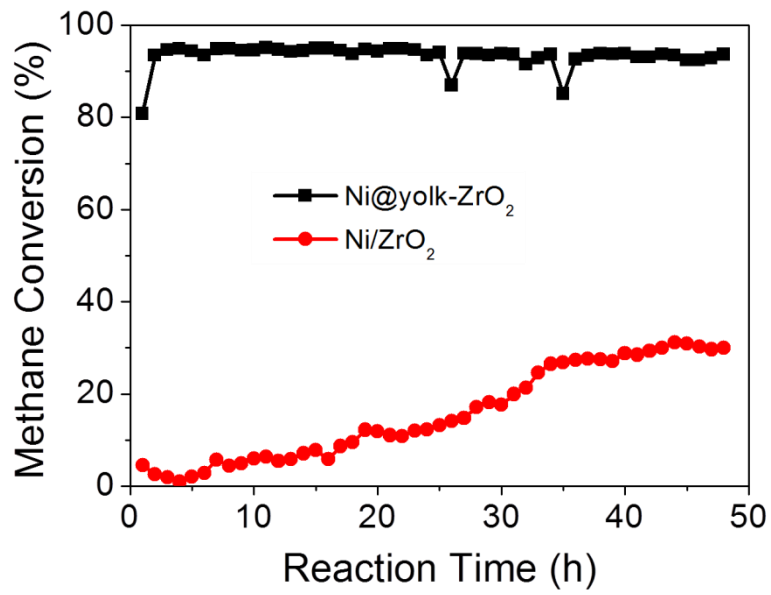
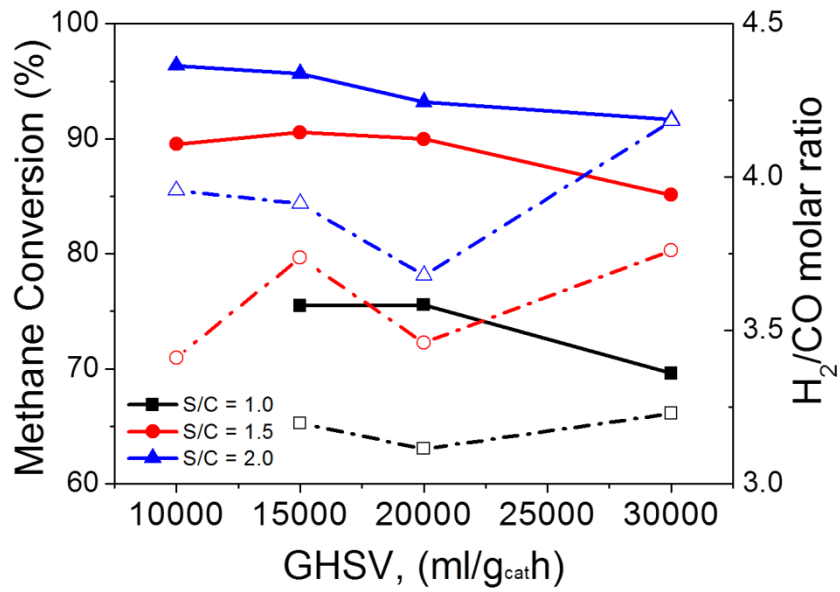


Fig 6. BET isotherm of Ni@yolk-ZrO₂ (a) and Ni/ZrO₂ (b). Inset: Pore size distribution of Ni@yolk-ZrO₂ (c) and Ni/ZrO₂ (d)



(a)



(b)

Fig 7. Catalytic steam reforming of methane on Ni@yolk-ZrO₂ and Ni/ZrO₂ catalyst (a).
 Catalytic performance and H₂/CO ratio under various GHSVs and S/C ratio on Ni@yolk-ZrO₂ catalyst (b).

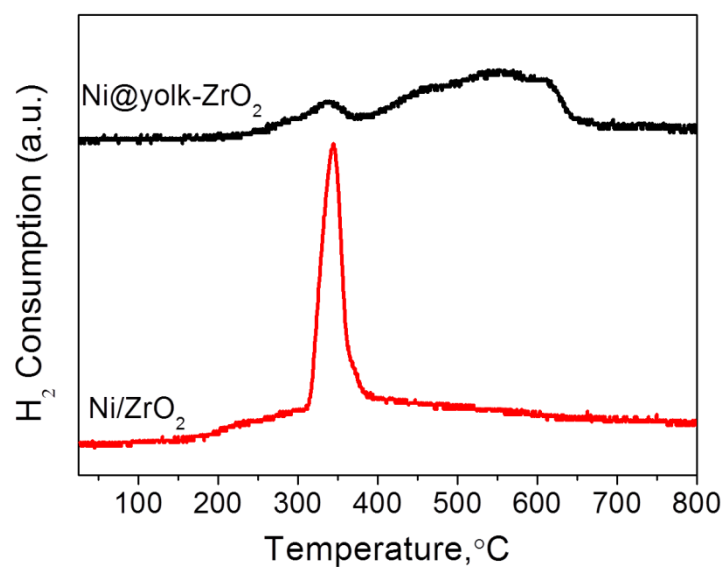
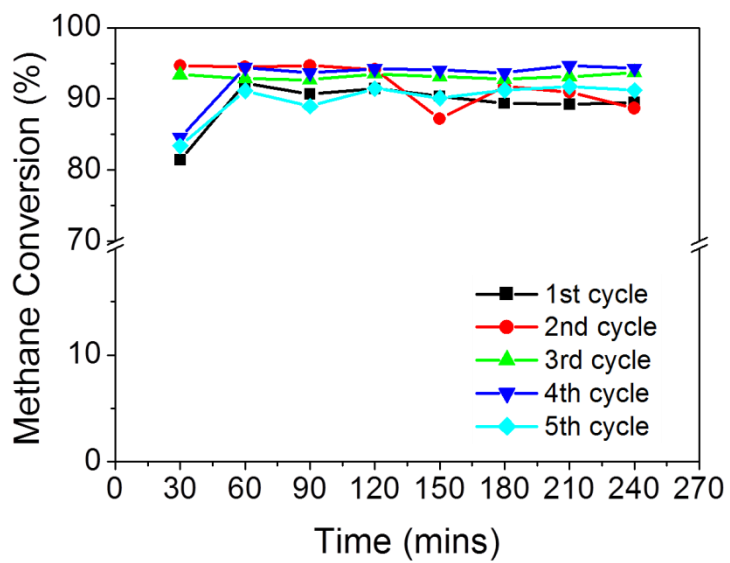
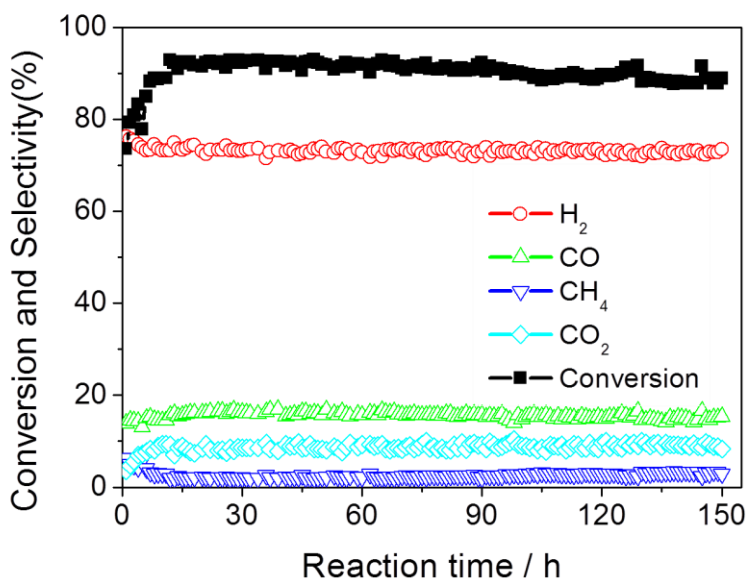


Fig 8. Temperature-programmed reduction of the catalysts.

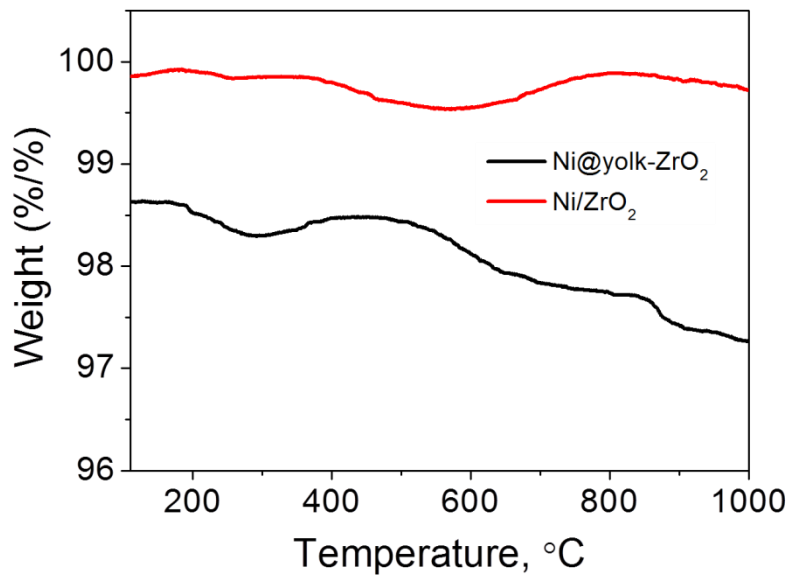


(a)

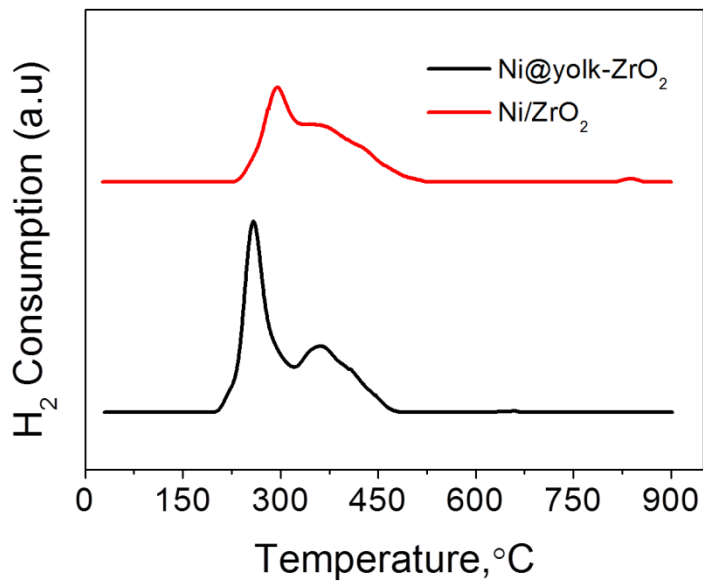


(b)

Fig 9. Reusability of Ni@yolk-ZrO₂ on steam reforming of methane (a) and 150 hours durability test on Ni@yolk-ZrO₂ catalyst (b).

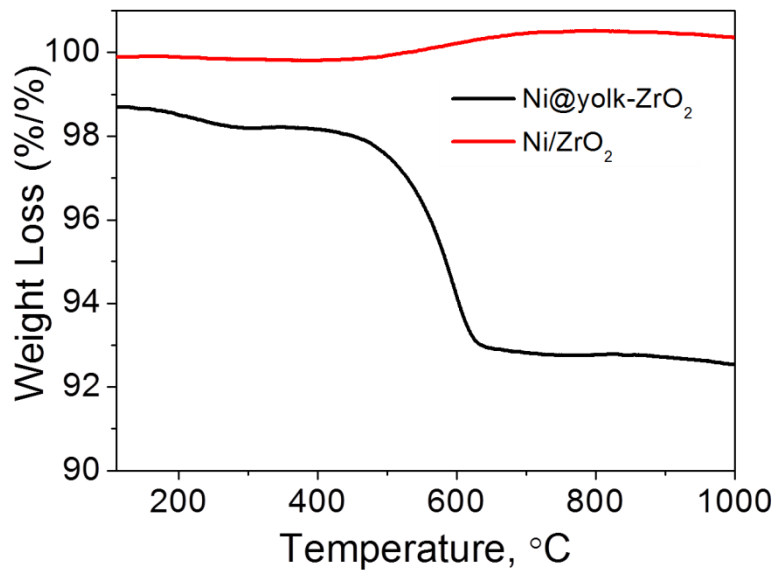


(a)

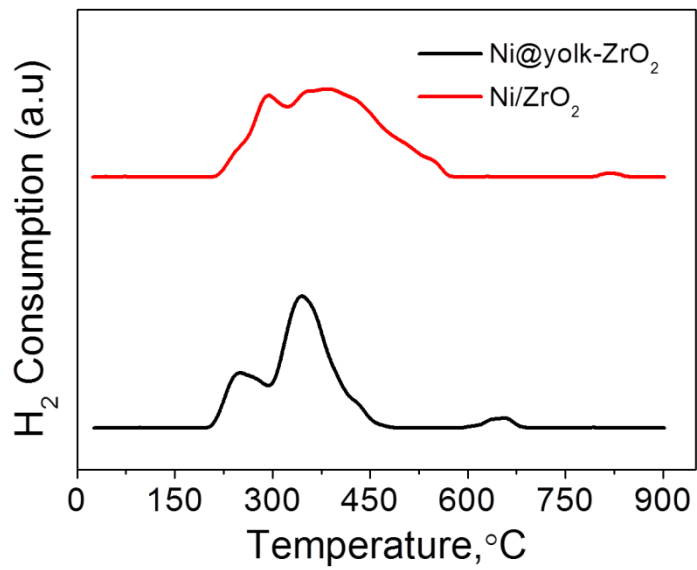


(b)

Fig 10. TGA analysis (a) and TPH analysis (b) of used catalysts under condition S/C = 2.5.



(a)



(b)

Fig 11. TGA analysis (a) and TPH analysis (b) of used catalysts under condition S/C = 1.

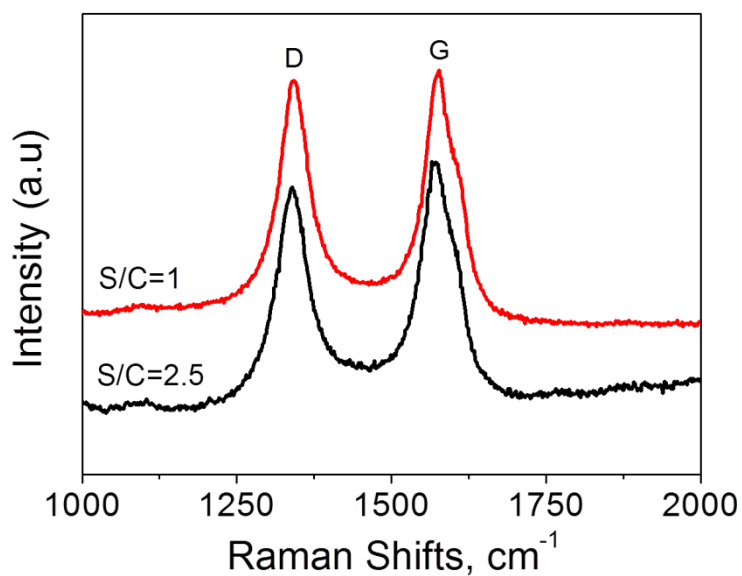


Fig 12. Raman spectra of used Ni@yolk-ZrO₂ catalyst

Table 1. XPS analysis of the relative mass concentration of Ni@yolk-ZrO₂ and impregnated Ni/ZrO₂ catalysts before and after steam reforming test

Catalysts	Ni 2p (%)	O 1s (%)	Zr 3d (%)	Si 2p (%)
Ni@yolk-ZrO ₂ -before	2.78	36.3	45.5	15.41
Ni@yolk-ZrO ₂ -after	0	31.13	40.02	22.69
Ni/ZrO ₂ -before	7.88	21.57	70.54	-
Ni/ZrO ₂ -after	7.49	36.13	56.38	-

Table 2. Selected results of core shell or yolk-shell structured catalysts in reforming of methane

Catalyst	Ni wt%	GHSV	Conditions	Temperature (°C)	X _{CH₄}
Ni@yolk-ZrO ₂	5.08	50400	SRM (S/C=2.5)	750	93.0
Ni@SiO ₂ yolk-shell ³	89	100000	SRM (S/C=4)	700	90.0
10 wt% Ni/MgAl ₂ O ₄ ⁴	10	54000	SRM (S/C=2)	750	97.2
NiO-350@meso-SiO ₂	54.8	72000	POM	750	93.0
Ni-Yolk@Ni@SiO ₂ ⁶	18.6	36000	DRM	800	90.0